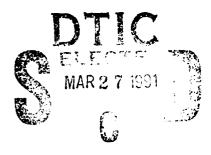
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# Flap-Lag Stability Data for a Small-Scale Isolated Hingeless Rotor in Forward Flight

Michael J. McNulty



**April 1989** 



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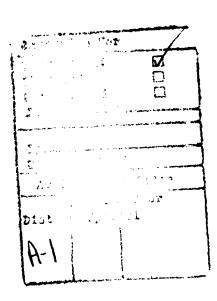
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# Flap-Lag Stability Data for a Small-Scale Isolated Hingeless Rotor in Forward Flight

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**April 1989** 





National Aeronautics and Space Administration

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#### **SUMMARY**

An isolated, hingeless rotor with discrete flap and lead-lag flexures and relatively rigid blades was tested in the Aeroflightdynamics Directorate's 7- by 10-Foot Wind Tunnel. The purpose of the test was to determine experimentally the lead-lag stability of a structurally simple rotor configuration in forward flight. The model tested had no cyclic pitch control, and was therefore operated untrimmed at several collective pitch angles, at shaft angles from  $0^{\circ}$  to  $-20^{\circ}$ , and at advance ratios as high as 0.55. Two inplane natural frequencies, 0.61/rev and 0.72/rev, were tested for configurations both with and without structural flaplag coupling. Concomitant hover testing of the model was also conducted. Representative plots of the frequency and damping data are presented to show general trends, and complete tabular data and model properties information are included for use in detailed correlation studies. The most prominent feature of the forward flight data is an abrupt increase in damping with advance ratio at certain high-speed, high shaft-angle conditions, with high flapping loads. The hover data are consistent with previous experimental and theoretical results for hingeless rotors without kinematic couplings. Overall, the data quality is very good and the data are expected to be useful in the development and validation of rotor aeroelastic stability analyses.

## **NOMENCLATURE**

B.S. blade station,	from	center	of	rotation, in	
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cd airfoil drag coefficient

c<sub>l</sub> airfoil lift coefficient

α airfoil angle-of-attack, to chord line, rad

α, rotor shaft angle, negative for forward tilt, deg

 $\mu$  advance ratio

 $\sigma$  damping exponent, 1/sec

 $\theta_0$  blade collective pitch angle, to chord line, deg

 $\omega$  natural frequency, Hz

 $\Omega$  rotor speed, rpm

### INTRODUCTION

The general problem of predicting rotorcraft aeromechanical and aeroelastic stability encompasses an array of analytical challenges. Structural dynamic complications include significant geometric nonlinearities, geometric stiffness, coupling between the rotor and the

nonrotating system, configurations with redundant load paths, and the widespread use of composite and elastomeric materials. Aerodynamic complications include rotor wake effects, nonlinear airfoil effects, transonic flows, and rotor-body aerodynamic interactions; all of which are, for the stability question, unsteady phenomena, and all of which may exist both in hover and forward flight. An additional complication whose importance promises to increase in the future is the effect of active controls. Developing an analysis which will accurately deal with all of these effects for an arbitrary rotorcraft configuration at any operating condition is a formidable task.

Specialized investigations of simple configurations and restricted flight conditions can emphasize the effects of one complicating factor and minimize the effects of others. For such cases, systematically comparing the results of various analyses with appropriate experimental data sets can give insights into the fundamental dynamic behavior of rotorcraft, as well as expose the specific strengths and weaknesses of the analyses. A number of such investigations have been conducted, and cases for which experimental data are available include: an isolated (i.e., the hub is fixed rigidly in space) torsionally soft elastic blade both in a vacuum (ref. 1), and in hover (ref. 2); an isolated hingeless rotor with rigid blades, flap- and lead-lag degrees of freedom, and various aeroelastic couplings in hover (refs. 3 and 4); a coupled hingeless rotor-body with rigid blades and discrete flap and lead-lag flexures, both under simulated vacuum conditions and in hover (ref. 5); and a simple isolated bearingless rotor in hover (ref. 6).

None of the investigations above deals with the effects of forward flight; the present work was intended to examine this area. Theoretical work has indicated that forward flight can have large effects on blade flap-lag stability (refs. 7 and 8), but a lack of experimental data has hampered the validation and refinement of those results. Coupled rotor-body stability data in forward flight are available (ref. 9), but isolated rotor flap-lag stability data are lacking. Although rotor-body testing more closely represents actual rotorcraft in flight, isolated rotor studies are probably even more valuable for examining the effects of forward flight because there are no body coupling effects present to obscure the results. Rotor-body coupling is a relatively tractable problem which can be dealt with separately. The primary objective of the research reported here was to obtain a set of isolated rotor flap-lag stability data in forward flight for correlation with existing and future analyses. Whereas all of the isolated rotor tests referred to above used two-bladed rotors, for this experiment a three-bladed rotor was chosen, in part so that the role of dynamic inflow (ref. 10) in isolated rotor flap-lag stability could be assessed.

This report presents an extensive set of experimental aeroelastic stability data and supporting documentation for the specialized case of an isolated rotor in forward flight. The model tested was a three-bladed, soft-inplane, hingeless rotor with discrete flap and lead-lag flexures and relatively rigid blades. The model structural configuration and control system were kept as simple as possible to more effectively isolate the effects of forward flight aerodynamics on lead-lag damping. The test was conducted in the Aeroflightdynamics Directorate's 7- by 10-Foot Low Speed Wind Tunnel at Ames Research Center. Two nominally identical rotor models were tested, Rotor I and Rotor II. Rotor I was tested extensively in hover, and

then tested in forward flight up to very high flapping conditions at a single rotor speed and a single collective pitch angle. When the flexures of Rotor I exceeded their fatigue life, a second set of flap and lead-lag flexures was installed with the blades on the hub, which gave Rotor II. Although Rotors I and II were identical in design, due to manufacturing differences the flap and lead-lag flexures of Rotor II gave slightly different fundamental frequencies than did Rotor I. Rotor II was tested in forward flight at two rotor speeds, and three collective pitch angles, both with and without structural flap-lag coupling, but it was restricted to less extreme flapping conditions than Rotor I. Only limited hover testing was conducted with Rotor II. Although the differences between Rotor I and Rotor II data are quite small for otherwise identical conditions, the rotor used is specified for each datum presented. Some of the data presented here have previously been published and compared to analytical predictions of lead-lag damping based on both linear (ref. 11) and nonlinear (ref. 12) quasi-steady aerodynamic theories.

This data report describes the model, instrumentation, test procedures, and data analysis techniques used for the experiment; presents representative plots of the data obtained; and includes complete tabulations of the data for use in future correlations with analyses.

# **EXPERIMENT DESCRIPTION**

# Model Description

A photograph of the rotor hub and blades installed on the model is shown in figure 1. Considerable analytical research has been conducted using the simplifying representation of a hingeless rotor as a set of rigid blades with offset, coincident, spring-restrained flap and lead-lag linges, (ref. 7); the model tested was designed to closely approach this simple analytical idealization. To accomplish this the model used lead-lag and flap flexures, shown in an exploded-view drawing in figure 2. Two stiff "side beams" attached the outboard end of the single element lead-lag flexure to the inboard end of the double-element flap flexure so that the lead-lag and flap flexural we's were both centered at 11% of the rotor radius. The flap flexure was very stiff in the lead-lag direction and the lead-lag flexure was very stiff in the flap direction. Both flexures were designed to be as stiff as possible in torsion so as to minimize elastic pitch motion inheard of the blade root. The measured torsional stiffness of the flexure assembly was 215 in-lbs/radian, which gave a nonrotating fundamental blade-torsion frequency of 149 Hz. This value is equal to 9/rev at the highest rotor speed tested.

The model had no cyclic pitch control, and the collective pitch angle was set manually prior to operation. This resulted in trim conditions with unrestricted cyclic flapping, and which satisfied no particular force and moment requirements. Rotor flapping flexure strain allowables determined the limits of the shaft angle versus advance ratio test envelope at a given collective pitch. While these are not normal rotorcraft operating conditions, they do

represent well defined and challenging conditions for analytical validation and development exercises. Eliminating the swashplate and pitch bearings minimizes control slop and friction damping, which allows higher quality model-scale dynamic data to be obtained than would be possible otherwise.

The model incorporated means for varying the amount of structural coupling between the flap and lead-lag motions of the blade, an important factor in hingeless rotor aeroelastic stability (ref. 3). This was accomplished by setting the collective pitch either by rotating the blade relative to the blade socket, giving essentially no flap-lag structural coupling, or by rotating the entire flexure assembly and the blade along with it, relative to the hub adaptor, giving full flap-lag structural coupling. These two possible pitch-change locations are identified in figure 2. The flexure-blade assemblies were mounted to the hub so that, when the flap and lead-lag angles were zero, the line along the blade quarter-chord was normal to the rotor shaft and passed through its center.

Figure 3 shows the details of the blade planform and cross section. The blades were composed of stiff Kevlar spars with tantalum leading edge weights for chordwise mass balance, balsa wood cores, fiberglass reinforcement at the trailing edges, and fiberglass overwraps for torsional stiffness. The blades were untwisted and untapered, with the root cutout at 18.6% and the NACA 23012 airfoil section beginning at 24.8% of the radius and continuing to the tip. The elastic axis, pitch axis, and axis of section mass centers were all located at the quarter chord. The blades were much stiffer than the flexures in both the flap and lead-lag directions so that rigid-body blade motions about the flexures would accurately represent the rotor's fundamental flap and lead-lag modes. With the blade root socket clamped to a backstop, the first flap and lead-lag frequencies of the blades alone were measured as 9.5 and 33 Hz, respectively, and the second flap frequency was 59 Hz. The first torsion frequency of the blade without flexures was estimated to be greater than 200 Hz.

Previous model-rotor testing experience has shown that even relatively small differences in properties from one blade to another can result in very poor data quality in isolated blade stability tests of rotors with three or more blades. This problem was dealt with by very carefully matching the blade inertias and flexure stiffness to each other. Before being instrumented, the flexures for each rotor were honed by hand so that they all had the same flap and the same lead-lag frequencies when each was mounted with the same blade. Then, after the flexures were instrumented, a small variable tip mass in each blade, located on the quarter chord, (see fig. 3) was adjusted so that each flexure-blade assembly had the same lead-lag frequency as the others. The result was that with the model installed in the wind tunnel the maximum nonrotating frequency difference between blades was approximately 0.5%. Reference 13 examines the effects of blade-to-blade dissimilarities.

The principal geometric properties of the rotor and mass and stiffness properties suitable for use in rigid blade analyses are given in table 1. The values given are all measured, except for the torsional inertia and the flap and lead-lag inertia. The torsional inertia was computed from the measured torsional frequency and the measured stiffness. The flap and lead-lag inertia was calculated from the blade and flexure mass distribution. The given mass

properties include only the mass outboard of the center of the flapping flexure; no lead-lag flexure or side beam mass is included. The nonrotating frequency values in table 1 are the most reliable measurements of the set; it is therefore suggested that analysts adjust the flap and lead-lag flexure stiffnesses as needed to yield the given frequencies. The flap and lead-lag frequency differences between Rotor I to Rotor II are caused by variations in the manufacturing process. These frequency differences could be due to variations in the flexure web thicknesses of less than 0.001 inches. The change in nonrotating flap damping from Rotor I to Rotor II results from a change in the way the instrumentation leads were routed off the flexures. In general, the nonrotating damping measurements were quite variable, ranging from -0.070 to -0.120 for the lead-lag mode, dependent primarily on the amplitude of the excitation; the values given are averages for excitation levels typical of those used when the rotor was operating.

An exploded view of the flexure and blade assembly has been included as figure 2. Figures 4 through 6 show the details of the lead-lag flexures, the side beams, and the flap flexures, respectively. These drawings and material properties from reference 14 were used to calculate the running mass per unit length, torsional inertia per unit length, flap bending stiffness, lead-lag bending stiffness, and torsional stiffness for each of these components. The results are given in tables 2 through 4. The given torsional stiffness values include the effects of warping restraint at both ends of the thin webs of the flap and lead-lag flexures. The radial distributions of these properties for the blade, including the root socket, were taken from reference 15 and are included here as table 5.

Because actual lift and drag data for the NACA 23012 airfoil is unavailable at the low Reynolds numbers appropriate for a small-scale, low tip-speed test, steady-bending-moment data from a test with the same blades used in the present test has been used to estimate the airfoil characteristics (Bousman, William G., The Effects of Structural Flap-Lag and Pitch-Lag Coupling on Soft Inplane Hingeless Rotor Stability in Hover, NASA Technical Paper, to be published). The results are

$$c_d = 0.0079 + 1.7\alpha^2$$
  
 $c_l = 9.15 + 5.73\alpha$ 

These results apply for positive angler-of-attack below stall, and may be useful for correlations with the hover results of the present test. The forward flight conditions of the present test, however, often involve large negative angles-of-attack over significant portions of the rotor disk, and so the expressions above are less useful. Instead, published airfoil data for higher Reynolds numbers might be used, perhaps corrected for low Reynolds number effects.

A photograph of the model installed in the Aeroflightdynamics Directorate's 7- by 10-Foot Wind Tunnel is shown in figure 7. Side- and front-view diagrams of the installation are shown in figure 8. The rotor stand included a gimbal which allowed the upper stand, enclosed by the fuselage fairing, to roll relative to the lower stand. This roll motion results in lateral translation of the rotor hub which excites the blades' lead-lag motion. A push rod and an arm extending from the side of the upper stand connected it to a 50-lb electromechanical shaker, located next to the base of the lower stand, which could drive the gimbal roll motion. The gimbal motion could be locked out by a hydraulic brake. The stand and shaker were mounted on a base plate located under the tunnel floor. The base plate was attached to the wind tunnel structure by a hinge at the front and an electric actuator at the rear which could pitch the entire assembly forward, thereby controlling the rotor shaft angle. Shaft angles from 0° to -20° could be obtained. At a given collective pitch angle, rotor speed, and advance ratio, varying the shaft angle was the only means available to control the rotor loads. With the shaft vertical, the rotor plane was 38 inches above the wind tunnel floor.

The rotor stand was designed to be as stiff as possible so that the rotor dynamic data would be representative of isolated rotor results. The lowest natural frequency of the stand, with the brake locking out the roll gimbal, was found to be about 25 Hz. This is nearly four times greater than the rotor lead-lag regressing mode frequency at 1000 rpm, but is slightly less than the lead-lag progressing mode frequency at that rotor speed.

## Instrumentation

For each blade, the flap and lead-lag bending moments at the flexure center were measured with strain gage bridges. Each flap flexure was also instrumented with a torsion moment bridge at the outboard end of the web. For Rotor II additional flap and chord bridges were installed at the inboard and outboard extremes of the webs of one flexure set so that the bending moment distributions could be monitored. These signals were routed from the rotor hub through a slip ring to the nonrotating system. A Hall-effect 1/rev sensor was used to determine the rotor speed and establish a blade azimuth reference. A 60/rev signal was also used to give the rotor operator a continuously updated rotor speed measurement. The wind tunnel dynamic pressure and the rotor shaft angle were also measured with standard instruments. Accelerometers were also installed in both the fixed and rotating systems to help resolve any uncertainties that might arise regarding rotor-body coupling.

The signals from the strain gages, accelerometers, 1/rev sensor, and, for Rotor II, the dynamic pressure and shaft angle transducers were low-pass filtered to 50 Hz for anti-aliasing, amplified, and then digitized by a computer controlled data aquisition system. For Rotor I data, the shaft angle and dynamic pressure were simply recorded manually. The strain gage signals were also displayed on oscilloscopes so that rotor loads could be continuously monitored.

### Test Procedures

The pitch of each blade was set with the aid of a small bubble level before each run. Small adjustments to the pitch of each blade were then made until the rotor tracked at the

operating rotor speed in hover. In general, the track did not depend on the rotor speed, but it did deteriorate with increasing advance ratio. After the rotor was established at operating speed, the wind tunnel was started and the dynamic pressure increased to give the desired advance ratio. The rotor shaft angle was adjusted as needed to control the rotor loads during the process. With the rotor and wind tunnel stabilized at the test condition, the hydraulic gimbal brake was released and the shaker used to drive the upper stand in roll at the appropriate fixed system rotor lead-lag frequency, progressing or regressing as desired. When sufficient excitation was evident on the oscilloscope displays of the lead-lag bending gages, the shaker was stopped, the brake engaged to lock up the upper stand, and the data aquisition system triggered to record the ensuing transient. At least two separate records were taken at each test condition so that the repeatability of the measurements could be assessed. A total of over 2000 damping measurements were made.

# Data Analysis

Each record consisted of 5.12 seconds of data, digitized at a sample rate of 100 Hz. The multiblade coordinate transform was then used to transform the recorded individual blade signals to the nonrotating system, using azimuth information from the 1/rev signal. The resulting multiblade sine or cosine lead-lag coordinate time history was then analyzed with spectral and moving-block techniques (ref. 16) to determine the frequency and damping of the progressing or regressing lead-lag mode. The details of the implementation of these analyses are described in reference 17. While the analyses could have been performed on any of the individual lead-lag signals, the use of the transformed signals generally resulted in a higher signal-to-noise ratio, and it clearly separated the rotor regressing and progressing modes from each other. The importance of this separation will be discussed below.

#### RESULTS

The set of lead-lag regressing mode frequency and damping data obtained in forward flight is the primary result of this investigation. Data were also obtained in hover.

### Hover

The collective pitches and rotor speeds that define the hover test points are shown in figures 9(a) and (b), for the configurations with and without structural flap-lag coupling, respectively. Complete tabulations of the regressing lead-lag mode stability data in hover are given in table 6 for the configuration without structural coupling and in table 7 for the configuration with structural coupling. The identifying number of the rotor tested, collective pitch, rotor speed, shaft angle, and an identifying data point number are given along with the measured regressing-mode frequency and damping. Each table is sorted by increasing

collective pitch and rotor speed, decreasing shaft angle, and increasing rotor number. At zero collective pitch the two rotor configurations are identical, so some data points are included in both tables 6 and 7.

The fixed system lead-lag frequencies and damping values at zero collective pitch are plotted as a function of rotor speed in figure 10. The 2/rev frequency separation between the progressing and regressing modes is as expected for isolated rotor data. The small difference in nonrotating frequency between Rotor I and Rotor II is the cause of the consistent spread in the regressing mode frequency data, but for each rotor the actual data scatter is practically zero. For a truly isolated rotor, any differences in damping between the progressing and regressing mode results can be caused only by blade-to-blade coupling through the rotor wake. The small damping differences seen in figure 10 between the progressing and regressing mode damping values at the lower rotor speeds may be due to wake effects, but the differences seen at the higher rotor speeds are clearly too great for this explanation. These damping differences at high rotor speeds indicate that the rotor lead-lag progressing mode was coupling with the stand. This is not surprising since the progressing mode frequency at 1000 rpm approximately equals the frequency of the lowest stand mode. For rotor speeds above approximately 600 rpm, the progressing mode data are not representative of an isolated rotor.

The most important conclusion from figure 10 is that the regressing mode data show no signs of contamination by rotor-body coupling at any rotor speed. This shows the advantages of using a rotor with three or more blades for isolated rotor dynamics tests. Distinct progressing and regressing modes do not exist for rotors with less than three blades, and, due to the periodic coefficients of the governing differential equations, a single blade mode with the frequency  $\omega$  in the rotating system will appear in the nonrotating system at the two frequencies  $\Omega + \omega$  and  $\Omega - \omega$  simultaneously. Any blade motions therefore will couple with the stand at both these frequencies, and any proximity of the high frequency manifestation of the blade mode (at  $\Omega + \omega$ ) to a stand natural frequency will equally contaminate the low frequency manifestation (at  $\Omega - \omega$ ). For the present stand and blades, at rotor speeds above 600 rpm any two-bladed rotor data would have been contaminated regardless of whether the excitation was at  $\Omega + \omega$  or  $\Omega - \omega$ . Bousman, in the paper mentioned earlier, suggests that, for a two-bladed rotor to represent the isolated rotor case, the lowest stand natural frequency should be several times  $(\Omega + \omega)$ . With three or more identical blades, distinct progressing and regressing rotor modes exist and so any coupling of the progressing mode with the rotor stand does not affect the regressing mode; therefore the necessary condition for a model to correctly represent an isolated rotor is that the the lowest stand frequency be several times greater than the regressing mode frequency. The present model fulfills this requirement.

Even with three blades, the impulsive locking of the roll degree of freedom following the shake: input excites the progressing mode to some degree, even when the model is excited in roll at exactly the regressing mode frequency. The pure regressing mode data can then be extracted only by making use of multiblade coordinates. In practice the single blade signals were usually found to give acceptable results when the excitation level was high relative to

the response to the locking impulse and to the background noise. The multiblade coordinate results were, however, consistently better, based on the appearance of the time histories and the moving-block functions, and were less sensitive to the details of the excitation. The only disadvantage associated with using the multiblade coordinates is the requirement that each blade be instrumented.

Only the regressing lead-lag mode data will be considered further. Figure 11 shows the regressing mode damping as a function of rotor speed for collective pitches of 0°, 4°, 6°, and 8° for the configuration without structural coupling. Figure 11(a) shows that at zero collective pitch the Rotor II damping is lower than that of Rotor I, but the diherences are small except at the lower rotor speeds. Those differences may be related to the lower nonrotating flap damping in Rotor II. The damping is generally seen to increase with increasing rotor speed, except for the decrease between 350 and 400 rpm. This decrease grows with increasing collective pitch, and is associated with the coalescence of the flap and lead-lag frequencies (ref. 3).

The regressing mode frequency measured without structural coupling is shown to be essentially independent of the collective pitch angle in figure 12. The regressing mode frequency results obtained with full structural coupling (not shown here) are essentially identical.

The regressing mode damping as a function of the collective pitch is shown in figures 13 and 14 for the configurations without and with structural coupling. For each configuration data are given for both 750 and 1000 rpm; these are the rotor speeds at which the forward flight data were taken. The dimensionless rotating lead-lag frequencies at these rotor speeds are 0.72 and 0.61, respectively. The increase in damping with collective pitch is as expected for soft-inplane hingeless rotors, without kinematic couplings, away from the flap-lag frequency coalescence.

The hover testing was conducted in a relatively small test section with the rotor only 0.6 diameters above the floor. Even for this small separation, there are several factors that indicate that the influence of ground effect and recirculation on the damping data is minor. Most convincing are the model tests with ground planes reported in reference 2. These tests showed that the ground planes had little influence on lead-lag damping, even for very small separations between the rotor and the ground planes. The second factor is evident from a comparison of the Rotor I and the Rotor II hover results to each other. The Rotor I hover testing was conducted with the wind tunnel test-section doors open and the windows removed to reduce recirculation, while the Rotor II hover testing was conducted with the doors closed and the windows installed. The recirculation present is certainly very different for these two situations, although neither closely represents a free air hover test. If recirculation were a major factor, then the data from the two rotors would be expected to show differences that increase significantly with increasing blade pitch. Figure 13, however, shows such differences to be small.

In general, the hover data quality, as judged by the small scatter in the results and the appearance of the time histories and moving-block functions, is very good. Figure 15 shows sample time histories of the cosine lead-lag coordinate and the resulting moving-block

functions at the regressing mode frequency for the hover cases at 1000 rpm, with collective pitches of 0°, 4°, and 8°. The ideal moving-block function is a straight line, whose slope is equal to the damping exponent, with small oscillations at twice the analysis frequency superimposed (ref. 17). The 0° and 4° cases (figs. 15(a) and (b)), show nearly ideal results, while the 8° case (fig. 15(c)) shows a somewhat degraded but still very good moving-block function. These results are typical of the hover data. The degradation of the moving-block function at higher collective pitches is the result of a decreased signal-to-noise ratio, due both to increased noise from recirculation, and a lower average signal, due to the higher damping of these cases. The degradation manifests itself in the damping data as increasing scatter with increasing collective pitch.

# Forward Flight

Forward flight testing was conducted at rotor speeds of both 750 rpm and 1000 rpm, for the configurations both with and without structural coupling, at collective pitch angles of 0°, 3°, and 6°. The conditions tested without structural coupling are summarized in figures 16 and 17. Figures 18 and 19 summarize the conditions tested with structural coupling. At each advance ratio, the high negative-shaft-angle limits were set by large negative coning loads, while the low shaft angle limits were set by high cyclic flapping loads. The data available for  $\theta_0 = 6^{\circ}$  are quite limited due to the high cyclic flapping loads, and therefore the effects of structural coupling in forward flight were not thoroughly explored by this test. Only the results for the configuration without coupling will be discussed herein, but the results obtained both with and without coupling are included in tabular form. Tables 8 and 9 present the data for the configuration without structural coupling at 750 and 1000 rpm respectively, sorted by collective pitch, advance ratio, and shaft angle. Tables 10 and 11 are the corresponding tables for the configuration with structural coupling.

Figures 20 through 25 show the regressing lead-lag mode damping as a function of the advance ratio for the 750 rpm rotor speed, for rotor shaft angles of 0°, -4°, -8°, -12°, -16°, and -20°, respectively. Figures 26 through 31 show the corresponding results at 1000 rpm. Each figure shows all of the data available at each collective pitch tested. The data for Rotor I are limited to the 1000-rpm, zero-collective cases, but includes advance ratio-shaft angle combinations that resulted in higher flapping conditions than Rotor II encountered. Overall the data scatter is small, and in all cases where data from both rotors are available, they agree very well with each other.

Significant changes in the damping at the high advance ratios are seen in figures 28 through 31 at zero collective pitch. The abrupt damping increases begin at lower advance ratios for more forward shaft angles, and are seen only at the high flap load conditions which only Rotor I encountered. In particular the increases appear related to high negative coning conditions, however, no flapping angle or thrust measurements are available for correlation. At these conditions large negative angles-of-attack are encountered over large regions of the rotor disk. The data at the higher collective pitch angles were limited to lower load levels, and do not show similar increases within the test envelope.

The effects of changing rotor shaft angle at fixed advance ratios are shown in figure 32. Results are shown for advance ratios of 0.05, 0.15, 0.25, 0.35, 0.45, and 0.55. Data from both rotors are included without distinction. The large damping increases with forward shaft tilt are again seen at the zero-collective pitch, high speed conditions. The higher advance ratio cases show the increase to begin at less extreme shaft angles.

No special problems were encountered using the moving-block analysis on the forward flight data, and in most cases very good results were obtained. As in hover, the more highly damped conditions tended to show more scatter in the results than did the less stable conditions. Wind tunnel turbulence was an additional noise source, but this was offset to some extent by the reduced recirculation. The addition of 1/rev and 2/rev lead-lag loads due to forward flight also restricted the excitation levels allowable within the lead-lag flexure load limits, but this was not a major factor. Sample transient time histories of the multiblade cosine coordinate of the lead-lag motion in forward flight and the resulting moving-block functions at the regressing mode frequency are shown in figure 33 for  $\alpha_s = 0^{\circ}$ , and in figure 34 for  $\alpha_s = -10^\circ$ . Both figures are for  $\theta_0 = 0^\circ$  and advance ratios of 0.15, 0.35, and 0.55. All the moving-block results of figure 33, and those of figure 34(a) and 34(b) are very good. These are all relatively low-damping, low-flapping conditions, and the effects of forward flight alone are not troublesome. The  $\mu = 0.55$ ,  $\alpha_s = -10^{\circ}$  case of figure 34(c), however, shows a somewhat degraded moving-block function. This is a high flapping load case and was one of the most highly damped cases found in forward flight, so the degradation is not surprising. The moving-block function for this case is probably the worst encountered during the entire test, and it is still quite acceptable.

## SUMMARY OF RESULTS

An isolated hingeless rotor with discrete flap and lead-lag flexures, relatively rigid blades, and high torsional stiffness was tested in the Aeroflightdynamics Directorate's 7- by 10-Foot Wind Tunnel. The objective of the test was to obtain a database of isolated rotor flap-lag stability in forward flight for correlation with current and future rotorcraft stability analyses. The model was tested at advance ratios up to 0.55, for three values of collective pitch, and for shaft angles from  $0^{\circ}$  to  $-20^{\circ}$ . Two inplane natural frequencies, 0.61/rev and 0.72/rev, were tested for configurations with and without structural flap-lag coupling. Specific findings include

- 1. The use of a simple model with no swashplate or pitch bearings eliminated control system slop and reduced friction damping to a minimum, and this, together with careful blade-to-blade matching, was largely responsible for the high quality of the test data. The use of a three-bladed rotor, rather than a two-bladed rotor, also greatly eased the problem of unwanted rotor-test stand coupling.
- 2. The test procedures and data analyis techniques, which were originally developed for hover, worked very well in forward flight. The use of multiblade coordinate data for the

damping measurements generally gave better results than did analysis of single blade signals. No problems peculiar to rotor stability testing in forward flight were encountered during the test.

- 3. The hover data obtained are consistent with previous experimental and theoretical results for hingeless rotors without kinematic couplings.
- 4. The most prominent feature of the forward flight data is an abrupt increase in damping with advance ratio at high speed, high shaft-angle conditions, and zero collective pitch. This behavior begins at lower advance ratios for more forward shaft angles, and seems related to high negative coning.

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TABLE 1.-ROTOR PROPERTIES

Property	Rotor I	Rotor II
Number of blades	3	3
Airfoil section	NACA 23012	NACA 23012
Hover tip Mach number at 1000 rpm	0.25	0.25
Hover tip Reynolds number at 1000 rpm	240,000	240,000
Rotor radius, in.	31.92	31.92
Blade chord, in.	1.65	1.65
Radial location of the center of the flexures, in.	3.55	3.55
Radial location of the blade center of mass, in.	11.1	11.1
Mass outboard of the flexure center, slugs	0.0130	0.0130
Flap and lead-lag inertia about flexure center, slug-in <sup>2</sup>	1.80	1.80
Torsional inertia, slug-in <sup>2</sup>	0.00294	0.00294
Flexure assembly flap stiffness, in-lb/radian	66.0	66.0
Flexure assembly lead-lag stiffness, in-lb/radian	281	281
Flexure assembly torsional stiffness, in-lb/radian	215	228
Nonrotating flap frequency, Hz	3.09	3.21
Nonrotating lead-lag frequency, Hz	6.98	7.24
Nonrotating torsion frequency, Hz	149	a
Nonrotating flap damping, 1/sec	-0.15	-0.09
Nonrotating lead-lag damping, 1/sec	-0.09	-0.09

<sup>&</sup>lt;sup>a</sup> Not measured.

TABLE 2.-LEAD-LAG FLEXURE PROPERTIES

Blade	Mass,	Torsional	Flapping	Lead-lag	Torsional
station,	slug/in	inertia,	stiffness,	stiffness,	stiffness,
in.		slug-in <sup>2</sup> /in	lb-in <sup>2</sup>	lb-in²	lb-in <sup>2</sup>
2.431	0.013 118	0.003 127	5 087 300	5 087 300	4 000 000
2.581	.013 118	.003 127	5 087 300	5 087 300	4 000 000
2.581	.003 568	.000 593	1 845 300	84 202	25 700
2.601	.002 492	.000 405	1 288 600	28 670	25 700
2.621	.002 202	.000 <b>356</b>	1 138 500	19 773	<b>25</b> 700
2.641	.002 117	.000 342	1 094 700	17 578	<b>25</b> 700
2.730	.002 117	.000 342	1 094 700	17 578	25 700
2.762	.001 799	.000 340	1 091 000	14 938	<b>25</b> 700
2.840	.000 765	.000 175	563 600	6 350	<b>25</b> 700
2.918	.000 584	.000 146	471 900	4 850	<b>25</b> 700
2.996	.000 765	.000 175	<b>563</b> 600	6 350	25 700
3.074	.001 700	.000 340	1 091 000	14 938	25 700
3.105	.002 117	.000 342	1 094 700	17 578	25 700
3.255	.002 117	.000 342	1 094 700	17 578	<b>25</b> 700
3.255	.002 117	.000 342	1 094 700	17 578	1 272
3.280	.000 903	.000 144	467 000	1 366	1 272
3.304	.000 550	.000 088	284 600	309	1 272
3.329	.000 448	.000 071	231 400	166	1 272
3.777	.000 448	.000 071	231 400	166	1 272
3.802	.000 550	.000 088	284 600	309	1 272
3.826	.000 903	.000 144	467 000	1 366	1 272
3.851	.002 117	.000 342	1 094 700	17 578	1 272
3.851	.002 117	.000 342	1 094 700	17 578	25 700
3.901	.002 117	.000 342	1 094 700	17 578	25 700
3.901	.002 566	.000 386	1 222 000	<b>32 26</b> 0	25 700
4.051	.002 566	.000 386	1 222 000	<b>32 26</b> 0	25 700
4.051	.002 117	.000 342	1 094 700	17 578	25 700
4.101	.002 117	.000 342	1 094 700	17 578	25 700

TABLE 3.-SIDE BEAM ASSEMBLY PROPERTIES

Blade station, in.	Mass, slug/in	Torsional inertia, slug-in <sup>2</sup> /in	Flapping stiffness, lb-in <sup>2</sup>	Lead-lag stiffness, lb-in <sup>2</sup>	Torsional stiffness, lb-in <sup>2</sup>
2.633	0.001 650	0.000 237	465 200	296 400	8 277
2.683	.001 650	.000 237	465 200	296 400	8 277
2.683	.001 905	.000 286	537 000	<b>383</b> 000	8 277
2.833	.001 905	.000 286	537 000	383 000	8 277
2.833	.001 650	.000 237	<b>465 2</b> 00	296 400	8 277
2.883	.001 650	.000 237	465 200	296 400	8 277
2.883	.001 274	.000 171	<b>359</b> 000	191 350	8 277
2.983	.001 274	.000 171	<b>359</b> 000	191 350	8 277
3.061	.000 601	.000 104	244 300	90 300	8 277
3.139	.000 497	.000 092	221 400	74 670	8 277
3.217	.000 601	.000 104	244 300	90 300	8 277
3.295	.001 274	.000 171	<b>359</b> 000	<b>191 350</b>	8 277
3.439	.001 274	.000 171	<b>359</b> 000	191 <b>3</b> 50	8 277
3.517	.000 601	.000 104	244 300	90 300	8 277
3.595	.000 497	.000 092	221 400	74 670	8 277
3.673	.000 601	.000 104	244 300	90 300	8 277
3.751	.001 274	.000 171	359 000	191 350	8 277
3.851	.001 274	.000 171	<b>359</b> 000	191 350	8 277
3.851	.001 915	.000 236	539 900	221 300	8 277
3.901	.001 915	.000 236	539 900	221 300	8 277
3.901	.001 661	.000 212	468 100	213 050	8 277
4.051	.001 661	.000 212	468 100	213 050	8 277
4.051	.001 915	.000 236	<b>539 9</b> 00	<b>221 3</b> 00	8 277
4.101	.001 915	.000 236	539 900	221 300	8 277

TABLE 4.-FLAP FLEXURE PROPERTIES

Blade station, in.	Mass, slug/in	Torsional inertia, slug-in <sup>2</sup> /in	Flapping stiffness, lb-in <sup>2</sup>	Lead-lag stiffness, lb-in <sup>2</sup>	Torsional stiffness, lb-in <sup>2</sup>
2.633 2.683 2.683 2.833 2.833 2.883 2.883 2.905 2.927 2.949 4.157	0.008 584 .008 584 .008 135 .008 135 .008 584 .001 382 .000 558 .000 340 .000 276 .000 276	0.003 526 .003 526 .003 439 .003 526 .003 526 .003 526 .000 450 .000 181 .000 110 .000 089 .000 089	2 445 000 2 445 000 2 317 000 2 317 000 2 445 000 2 445 000 10 200 671 151 81.6 81.6	9 026 000 9 026 000 8 871 000 8 871 000 9 026 000 9 026 000 1 452 900 586 600 357 100 290 600	591 000 591 000 591 000 591 000 591 000 591 000 342 342 342 342 342
4.179 4.201 4.223 4.223 4.243 4.273 4.303 4.423	.000 340 .000 558 .001 382 .007 515 .007 515 .008 054 .011 406	.000 110 .000 181 .000 450 .002 775 .002 775 .002 870 .003 394 .003 394	151 671 10 200 1 889 000 1 889 000 2 042 000 3 399 600 3 399 600	357 100 586 600 1 452 900 7 139 800 7 139 800 7 295 000 7 641 000 7 641 000	342 342 342 3 548 000 3 548 000 3 669 000 4 339 000 4 339 000

TABLE 5.-BLADE AND ROOT SOCKET PROPERTIES

Blade station, in.	Mass, slug/in	Torsional inertia, slug-in²/in	Flapping stiffness, lb-in <sup>2</sup>	Lead-lag stiffness, lb-in <sup>2</sup>	Torsional stiffness, lb-in <sup>2</sup>
4.423	0.006 894	0.001 708	1 770 000	3 660 000	2 180 000
4.484	.006 832	.001 708	1 770 000	<b>3</b> 660 000	2 180 000
4.484	.007 174	.001 708	1 770 000	<b>3</b> 660 000	2 180 000
4.613	.007 174	.001 708	1 770 000	<b>3</b> 660 000	2 180 000
4.613	.001 643	.000 077	124 000	124 000	95 900
5.078	.001 584	.000 076	124 000	124 000	95 900
5.260	.005 932	.001 224	124 000	124 000	95 900
5.410	.005 932	.001 224	124 000	124 000	95 900
5.410	.000 755	.000 023	45 900	45 900	23 800
5.469	.000 904	.000 027	<b>53</b> 800	<b>53</b> 800	28 800
5.469	.003 696	.000 457	<b>53</b> 800	<b>53</b> 800	28 800
5.529	.003 665	.000 481	99 100	99 100	61 600
5.529	.004 814	.000 916	99 100	99 100	61 600
5.659	.004 969	.000 922	101 000	101 000	59 600
5.659	.001 388	.000 053	101 000	101 000	59 600
5.764	.001 460	.000 052	102 000	102 000	56 800
5.764	.001 031	.000 021	<b>52</b> 600	<b>52 6</b> 00	18 700
5.924	.000 237	.000 022	2 280	61 700	1 200
7.924	.000 235	.000 027	2 280	61 700	1 200
31.92	.000 235	.000 027	2 280	61 700	1 200

CONFIGURATION WITHOUT STRUCTURAL FLAP-LAG COUPLING

Domping. 1/sec	-6.153	-0.154	-6.682	79.9	9	4 5 5	983	-0.092	<b>-0</b> .160	<b>-9</b> .162	-6.175	<b>-6.166</b>	97.9	<b>-6.117</b>	4.14	-0.189	<b>-6.175</b>	<b>-9</b> .221	9.189	e 173	\	2 4	3 E	189	-0.197	-0.179	4.17	<b>-6</b> .179	<b>-9.136</b>	2 - G	6.203	97.9	9	<b>6</b> .176	-0.201	<b>6</b> .171	<b>6.179</b>	<b>-6.159</b>	<b>-6</b> .155	‡ - 9		-0.157	<b>-6</b> .153
Frequency.	6.201	6.174	6.443	6.43	7.0.0	0.50 771 A	5.57	5.654	€.699	4.588	3.830	3.822	3.842	4.059	4.088	3.068	3.070	2.709	2.705	2.709	2.769	2.407	2.400	2.334	2.330	•	2.318	2.340	2.512	2.512	2.121	7 - 1 - 2	1 624	1.607	1.193	1.170	0.912	9.914	0.918	1.166	1.156	9.441	0.463
Shaft angle, deg	9.00	<b>9</b> 0.	<b>6</b> .9	6.6	90.0	9 6	9 6		99.	99.0	<b>9</b> 0.00	<b>9</b> 6.	99.9	10.0	<b>.6</b> .	<b>9</b> 6.	<b>9</b> 0.	9.00	90.0	<b>9</b>	9.00 0.00	9 6 9 6	9 6		9 6	90.	99.0	<b>9</b> 0.0	4.6	6.61	<b>9</b> 6	90.0	9 6	90.00		99.9	99.	99.	98.9	40.0	<b>.</b> 9	<b>9</b> 8.	<b>9</b> .00
Rotor speed,	49.57	50.98	50.82	59.82	166.00	24.75 24.75	07.001 04.101	189.36	149.41	150.59	200.04	200.39	199.34	200.84	200.84	250.66	250.43	275.16	275.27	274.92	274.80	296.27	280.04	300 47	301.05	300.23	301.17	299.88	300.05	300.86	315.00	313.23	310.03 48 48	350.39	378.69	380.04	400.31	399.38	399,61	400.29	400.99	•	500.98
Collective pitch, deg	9.	<b>0</b> .0	<b>.</b>	9.0	9.0	<b>D G</b>	•		0.0	0.0	<b>6</b> .0	<b>9</b> .0	0.0	<b>.</b>	<b>•</b> .•	• •	•.	<b>9</b> .	<b>.</b>	<b>6</b>	<b>9</b> .0		D 6	•	9 9	9.	<b>9</b> .0	<b>9</b> .	<b>0</b> .0	9.0	<b>.</b>	9.0	<b>D</b> 6	9		9	9.	9.0	9	0.0	<b>.</b>	9.	<b>.</b>
Data point number	82239001	82242041	83222012	83222013	62239663	82242044	8122201	83222015	82239005	82242046	82239007	82242048	82260009	, 83222016	83222017	82239669	82242050	82259056	82259062	82259063	82259064	82228	82259869	82249811	82242008	82242052	82246001	82260011	83222018	83222019	82259060	7/050779	02228073	82242015	82246063	82246011	82242012	82242056	82260013	83222620	83222021	82242060	82260015
Rotor	H	<b>-</b>	II	Ξ.	٠.	<b>}</b>	<b>-</b>		, <b></b>	-	-	-	-	11	I	-	-	<b>-</b>	<b>-</b>	<b></b> .	٠,	·	t	•	•	<b>—</b>	-	<b>-</b> -	11	I.	⊶.	<b>→</b> •	<b>-</b> -	٠,	•	• •			-	11	=	<b>-</b>	<b></b>

Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Shaft angle, deg	Frequency,	Damping. 1/sec
-	82260032	9.0	500.74	-21.00	0.475	<b>69.169</b>
-	82242018	<b>9</b> .	549.96	99.90	1.115	<b>-6</b> .151
-	82242062	9.0	549.96	99.00	1.123	9.148
_	82246005	9.9	565.66	9.00	1.326	7.9
	82246009	9.0	564.84	9.00	1.314	<b>6.143</b>
-	82242020	9.	600.59	9.00	1.775	-0.142
-	82242064	9.0	599.06	9.00	1.762	-0.147
-	82246007	60.60	600.35	90.00	1.756	-B. 158
-	82260017	0.0	600.00	9.00	1.77.1	-
II	83222024	<b>9</b> .0	599.28	<b>-6</b> .01	1.524	-a.135
11	83222025	<b>9</b> .0	600.21	<b>-9</b> .02	1.532	<b>-0</b> .128
=======================================	83222030	<b>9</b> .0	601.02	0.03	1.545	_
11	83222031	<b>9</b> .0	600.21	<b>9</b> .04	1.533	_
_	82260030	<b>0</b> .0	600.82	-21.00	1.783	<b>-6.149</b>
~	82242022	<b>0</b> .0	649.80	9.00	2.406	-
-	82242066	●.●	648.52	<b>9</b> 0. <b>0</b>	2.396	_
-	82242024	<b>9</b> .0	699.26	9.00	3.031	-
Н	82242968	<b>9</b> .	699.96	9.00	3.045	-0.156
-	82269019	60	699.61	9.00	3.039	•
11	83222026	0.0	799.57	19.0	2.818	_
11	83222027	<b>9</b> . <b>9</b>	701.15	-0.03	2.823	-
Ξ	83222032	0.0	700.46	9.0	2.818	•
11	83222033	<b>9</b> .	699.30	0.03	2.802	~
-	82260029	<b>0</b> .0	701.25	-21.00	3.061	~
-	82242026	<b>9</b> .0	750.35	<b>9</b> 0.	3.664	٣.
-	82242070	<b>9</b> .	750.35	<b>9</b> .00	3.668	-
II	83222034	<b>6</b>	750.93	<b>4</b> 0.0	3.448	_
II	83222035	<b>9</b> .0	750.46	<b>9</b> .0 <b>4</b>	3.440	*
11	83222036	<b>9</b> .	751.16	40.0	3.446	~
1	83222037	<b>9</b> .0	751.62	0.62	3.456	•
I	83222046	<b>6</b> .	750.70	6.65	0.444	-
I.	83222047	<b>6</b>	750.35	. e . e . e	3.440	_
⊒:	02222000	9.0	99.96/	99.0	5.452	P :
7 -	63223001		99.96/	9 . 60 7 0	5.478 4 453	41.0
<b>:</b>	62623638	9	140.04	90.0	3.12/	71.9
7.	93223040	<b>.</b> 6	749.42	9 6 9 6	3.423	2 9
;:	81001		747.04	9.6	7.150	9
	2027700 B1777071	9 9	748 40	9	7.403	: •
7.	1/9C77C0	9 9	740.43	9	7.1. 7.1.	9
- F	2702770		(D. 64C	9	071.P	- •
<b>:</b>	62224000		740.77		0.44 4.54	2 5
<b>≓</b> :	63224001	9 (	/*8*/	6.60	5.42/	- 1
Ξ;	83228000	9.0	749.67	9 e	3.427	٦,
Ξ:	83228001	9.0			5.456	7.145
= :	83229000	9	756.58	•	5.440	-9.142
I	83229661	<b>6</b> .6	750.12	6.67	4.434	141.0

Damping. 1/sec	161	-6.179	-0.168	. 161	<b>6.145</b>	<b>-6.143</b>	<b>-0</b> .172	<b>-6.171</b>	<b>6.174</b>	<b>6</b> .173	9.172		891. <b>9</b>	ָהָיבָּי הַיּבְיּי	(C)	2 5	- <b>6</b> .185	99.19	99.189	90.100	9.184	-6.193	-6.197	-6.163	9.156	9.7	<b>-6</b> . 162	<b>6</b> .161	9	191.9	79.79	9 9	20.0	9	153	7 9	4	9 9	9		90.00	128	-6.158 0.158	2	-8.163	<b>.6</b> . 191
Frequency.	1 684	4.285	4.281	4.273	4.040	4.044	4.871	4.891	4.879	5.480	5.482	0.486	5.488	5.204	5.260	80.00 0	6.051	6.6/6	6.639	6.637	6.658	6.643	6.646	6.436	6.420	6.428	6.422	6.420	6.440	6.422	6.450	6.458 4.28	0.450	428	6.430	6.432	0.4 8.4.00	6.410	9.4.0		6.436	6.424	6.422	6.422	6.432	7.217
Shaft angle, deg	20.0		98	98	0.02	0.03	<b>9</b> . <b>9</b>	<b>9</b> 0.	<b>.</b>	<b>8</b> .	<b>8</b> .6	8.	98.6	30.00 30.00	9.63	9.	<b>8</b> .6	96.	<b>6</b>	<b>.</b>	9.60	9.00	<b>8</b> .	9.65	<b>-6.6</b> 2	0.03	0.03	6.63	0.03	<b>9</b> . <b>0</b> 2	6.62	6.62	9.6	9.9	9	ē ē	ē. ē	0.00	3 . 6 . 6 .	9.90	9.00	90.0	6.6	6.67	6.67	<b>9</b> .00
Rotor speed,	761 60	10:108	200 A.	789.80	799.20	799.54	849.61	851.02	850.43	900.47	900.94	980.86	900.47	900.72	990.00	949.92	949.45	950.16	999.61	999.49	1969.66	989.84	1000.43	1000.39	999.23	999.81	999.23	988.34	1000.62	999.23	1666.39	1888.84	228.73	79.99	76.000	1000.04	- t- 000	989.23	89.68	888.10	1999.15	999.34	999.11	999.46	1666.15	1649.18
Collective pitch, deg	•	) <b>G</b>	•	6	0.0	0.0	0.0	9.0	9.0	•.	<b>6</b> .6	9.	<b>.</b>	9.	• •	9	<b>9</b> .0	<b>.</b>	<b>9</b> .	<b>.</b>	<b>.</b>	<b>9</b> .	<b>0</b> .	<b>9</b> .	<b>•</b> . <b>•</b>	0.0	<b>.</b>	<b>0</b> .0	<b>0</b> .	<b>6</b> .6	<b>9</b> .	9.6	<b>9</b> (	D 6	9.0	9.0	9.0	<b>.</b> (	9. G	9	<b>6</b> . 6	<b>9</b> .	<b>6</b> .6	9. 9	<b>0</b>	<b>o</b> .
Data point number	82260027	8224282 82242828	82243007	82260021	83222038	83222039	82242031	82242033	82243009	82242035	82243011	82250021	82260023	83222646	83222641	82242837	82243013	82250023	82242039	82243015	82250025	82260025	82263001	83222028	83222029	83222842	83222043	83222844	83222045	83223116	83223117	83223118	62223119	63224062	C00177C0	63224636	03224031	63224666	83224961	83224692	83228002	83228003	83228004	83229002	83229003	82250027
Rotor	-	•	•	• •	ï	II	-	-	-	-	<b>)</b>	<b>-</b>	-:	II	I '		<b>-</b>	-	<b></b>	<b>-</b>	-	<b>—</b>	<b>-</b>	II	1	11	I	=	<b>.</b>	I	<b>-</b>	Ξ:	<b>-</b> ;	3:	: :	<b>→</b> +		- •		11	I:	11	I	I	II	<b>-</b>

82256023         6.00         7.781         — 6.194           822276013         5.00         6.00         7.781         — 6.194           822276013         5.00         6.00         7.781         — 6.194           822276014         5.00         6.00         3.449         — 6.224           822276047         5.0         748.36         6.03         3.441         — 6.224           82223044         5.0         748.36         6.03         3.442         — 6.224           83223044         5.0         748.36         6.03         3.442         — 6.224           83223045         3.0         748.37         6.03         3.442         — 6.224           83223047         3.0         775.00         6.05         3.443         — 6.224           83223047         3.0         774.37         6.05         3.443         — 6.224           832230602         3.0         775.00         6.03         3.444         — 6.224           832230602         3.0         774.38         6.03         3.444         — 6.224           832230602         3.0         774.38         6.03         3.445         — 6.224           832230602         3.0         4.	Data point number	Collective pitch, deg	Rotor speed, rpm	Shaft angle, deg	Frequency, Hz	Domping 1/80c
3.6         7.86         2.86	0000000	6	1008	96	7 781	405
3.6         256.26         6.6         3.664           3.6         748.14         6.6         3.6           3.6         748.14         6.6         3.421           3.6         748.14         6.6         3.421           3.6         748.28         6.6         3.421           3.6         748.28         6.6         3.421           3.6         748.28         6.6         3.421           3.6         749.77         6.6         3.421           3.6         749.77         6.6         3.421           3.6         749.77         6.6         3.422           3.6         749.77         6.6         3.422           3.6         749.77         6.6         3.422           3.6         749.77         6.6         3.422           3.6         749.77         6.6         3.422           3.6         749.77         6.6         3.422           3.6         749.77         6.6         3.422           3.6         749.77         6.6         3.422           3.6         749.77         6.6         3.422           3.6         749.77         6.6         3.422	82237813	9 6	201.09	9 6	3,805	461.6
3.6         748.14         6.63         3.41           3.6         748.96         6.63         3.419           3.6         748.98         6.63         3.419           3.6         748.98         6.63         3.422           3.6         748.98         6.63         3.424           3.6         748.77         6.63         3.425           3.6         749.77         6.63         3.425           3.6         749.19         6.63         3.425           3.6         749.19         6.63         3.425           3.6         749.19         6.63         3.425           3.6         749.19         6.63         3.425           3.6         749.19         6.63         3.425           3.6         749.19         6.63         3.425           3.6         749.12         6.63         3.425           3.6         749.77         6.63         3.425           3.6         749.77         6.63         3.425           3.6         749.77         6.63         3.425           3.6         749.77         6.63         3.425           3.6         998.98         9.64	82237015	9.50	250.20	9.00	3.064	₩.177
3.6       748.96       9.64       3.419         3.6       748.72       9.66       3.421         3.6       749.88       9.65       3.424         3.6       749.98       9.65       3.424         3.6       747.91       9.66       3.424         3.6       747.91       9.66       3.424         3.6       748.72       9.65       3.425         3.6       748.13       9.65       3.425         3.6       749.13       9.65       3.425         3.6       749.13       9.65       3.425         3.6       749.13       9.65       3.425         3.6       749.13       9.65       3.425         3.6       749.13       9.65       9.65       3.425         3.6       749.77       9.63       3.425       3.446         3.6       749.77       9.63       3.446       3.446         3.6       749.77       9.63       9.64       8.422         3.6       749.77       9.63       9.64       8.422         3.6       9.98.99       9.64       8.426         3.6       9.98.99       9.64       8.426	83229046	Ø.5	748.14	0.03	٦.	<b>-0</b> .236
3.6       7.42.72       9.63       3.421         3.6       7.49.88       9.63       3.423         3.6       7.49.88       9.66       3.424         3.6       7.49.88       9.66       3.424         3.6       7.56.35       9.66       3.424         3.6       7.49.88       9.63       3.424         3.6       7.49.73       9.66       3.442         3.6       7.49.77       9.66       3.442         3.6       7.49.77       9.63       3.425         3.6       7.49.77       9.63       3.442         3.6       7.49.77       9.63       3.442         3.6       7.49.77       9.63       3.446         3.6       7.49.77       9.64       6.418         3.6       7.49.77       9.64       6.418         3.6       7.49.77       9.64       6.418         3.6       9.98.39       9.64       6.418         3.9       9.98.39       9.64       6.41         3.9       9.99.45       9.64       6.418         3.9       9.99.45       9.64       6.41         3.9       1600.15       9.64       6.42 <td>83229047</td> <td>3.0</td> <td>748.96</td> <td>9.04</td> <td>٦</td> <td><b>-0</b>.235</td>	83229047	3.0	748.96	9.04	٦	<b>-0</b> .235
3.6       749.88       9.63       3.432         3.6       749.791       9.66       9.425         3.6       749.791       9.66       3.424         3.6       759.88       9.66       3.424         3.6       759.88       9.65       3.425         3.6       759.88       9.63       3.425         3.6       751.62       9.66       3.425         3.6       751.62       9.66       3.425         3.6       751.62       9.66       3.425         3.6       751.62       9.66       3.425         3.6       751.28       9.66       3.452         3.6       751.28       9.66       3.452         3.6       751.28       9.66       3.452         3.6       751.28       9.66       3.452         3.6       751.28       9.66       3.452         3.6       9.98.99       9.66       3.452         3.6       9.98.99       9.66       3.453         3.6       9.99.45       9.64       6.41         3.6       9.99.46       9.69       6.41         3.6       9.99.46       9.69       6.42	83229048	3.0	748.72	0.03	٦.	<b>-0</b> .234
3.6       748.96       9.03       3.425         3.6       774.91       9.06       3.434         3.6       779.91       9.05       3.434         3.6       774.91       9.05       3.425         3.6       774.92       9.05       3.425         3.6       774.94       9.05       3.425         3.6       774.04       9.05       3.425         3.6       774.04       9.05       3.425         3.6       774.04       9.05       3.425         3.6       7751.62       9.06       3.425         3.6       7751.62       9.06       3.425         3.6       7751.62       9.06       3.425         3.6       7751.62       9.06       3.425         3.6       7751.62       9.06       3.425         3.6       7751.62       9.06       3.425         3.6       7751.62       9.06       9.07       9.06         3.6       9.08       9.06       9.07       9.07       9.07         3.6       1.06       9.07       9.07       9.07       9.07       9.07         3.6       1.06       9.07       9.07 <t< td=""><td>83229049</td><td>9.0</td><td>749.88</td><td>0.03</td><td>•</td><td><b>-0</b>.232</td></t<>	83229049	9.0	749.88	0.03	•	<b>-0</b> .232
3.6       749.77       9.06       3.434         3.6       750.00       3.5       3.45         3.6       750.00       3.45       3.45         3.6       750.00       3.45       3.42         3.6       750.00       3.42       3.42         3.6       751.20       9.00       3.45         3.6       751.20       9.00       3.45         3.6       751.20       9.00       3.45         3.6       751.20       9.00       3.45         3.6       751.20       9.00       3.45         3.6       751.20       9.00       3.45         3.6       9.00       9.00       3.45         3.6       9.00       9.00       3.45         3.6       9.00       9.00       9.45         3.6       9.00       9.00       9.45         3.6       9.00       9.00       9.45         3.6       9.00       9.00       9.45         3.6       1.00       9.00       9.00         3.6       1.00       9.00       9.00         3.7       1.00       9.00         3.8       1.00       9.00	83229050	9.0	748.96	0.03	٦.	<b>-0</b> .233
3.69       747.91       9.06       3.499         3.6       756.35       9.05       3.425         3.6       759.88       9.03       3.425         3.6       751.24       9.03       3.425         3.6       751.28       9.03       3.425         3.6       751.28       9.03       3.425         3.6       751.28       9.03       3.425         3.6       751.28       9.03       3.446         3.6       751.28       9.03       3.446         3.6       756.79       9.03       3.446         3.6       774.37       9.03       3.446         3.6       756.79       9.04       6.428         3.6       9.08       9.04       6.428         3.6       9.08       9.04       6.428         3.6       100       9.03       6.424         3.6       100       9.04       6.424         3.6       100       9.04       6.424         3.6       100       9.04       6.424         3.6       100       9.04       6.424         3.6       100       9.04       6.424         3.6       <	83229056	9.0	749.77	90.0	٠,	<b>6</b> .233
3.0       759.35       9.03       3.431         3.0       751.04       9.03       3.427         3.0       749.19       9.03       3.427         3.0       749.19       9.03       3.425         3.0       749.19       9.03       3.425         3.0       751.02       9.00       3.442         3.0       751.28       9.00       3.446         3.0       779.77       9.00       3.446         3.0       751.28       9.00       3.446         3.0       751.86       9.01       3.458         3.0       998.99       9.00       3.458         3.0       998.99       9.04       6.418         3.0       998.99       9.04       6.418         3.0       998.99       9.04       6.422         3.0       998.99       9.04       6.422         3.0       999.46       9.04       6.424         3.0       999.46       9.04       6.424         3.0       999.46       9.04       6.424         3.0       1000.93       9.04       6.424         3.0       1000.93       9.04       6.434	83229057	9.0	747.91	90.0	٦,	<b>-0</b> .236
3.6       756.00       0.03       3.427         3.6       749.88       0.03       3.425         3.6       751.04       0.03       3.425         3.6       751.26       0.00       3.425         3.6       751.26       0.00       3.442         3.6       751.26       0.00       3.442         3.6       751.26       0.00       3.446         3.6       751.26       0.00       3.446         3.6       751.26       0.00       3.446         3.6       777       0.00       3.446         3.6       751.26       0.00       3.446         3.6       998.99       0.00       3.458         3.6       998.99       0.04       6.418         3.6       998.99       0.04       6.418         3.6       998.46       0.04       6.424         3.6       999.46       0.04       6.424         3.6       999.46       0.04       6.424         3.6       999.46       0.04       6.424         3.6       999.46       0.04       6.424         3.6       1000.108       0.04       6.424	83236001	9.0	750.35	0.03	3.431	<del>-0</del> .222
3.6       749.88       6.63       3.425         3.6       749.77       6.63       3.442         3.6       749.77       6.63       3.442         3.6       751.62       6.60       3.442         3.6       751.62       6.60       3.446         3.6       751.86       6.61       3.446         3.6       751.86       6.61       3.452         3.6       998.39       6.61       3.458         3.6       998.39       6.64       6.418         3.6       998.39       6.64       6.418         3.6       998.46       6.64       6.424         3.9       999.46       6.64       6.424         3.9       999.46       6.64       6.424         3.9       1660.15       6.63       6.424         3.0       1660.15       6.63       6.424         3.0       1660.15       6.63       6.424         3.0       1660.15       6.63       6.424         3.0       1660.15       6.63       6.424         3.0       1660.15       6.63       6.424         3.0       1660.15       6.63       6.424 <tr< td=""><td>83236002</td><td>9.0</td><td>750.00</td><td>0.03</td><td>3.427</td><td><b>-0</b>.230</td></tr<>	83236002	9.0	750.00	0.03	3.427	<b>-0</b> .230
3.6       751.04       0.03       3.442         3.0       749.19       0.00       3.442         3.0       751.28       0.00       3.446         3.0       751.28       0.00       3.446         3.0       752.70       0.00       3.446         3.0       752.77       0.00       3.446         3.0       998.99       0.00       3.446         3.0       998.99       0.00       3.458         3.0       998.99       0.00       0.00         3.0       998.99       0.00       0.00         3.0       999.46       0.00       0.00         3.0       1000.37       0.00       0.00         3.0       1000.33       0.00       0.00         3.0       1000.30       0.00       0.00         3.0       1000.30       0.00       0.00         3.0       1000.30       0.00       0.00         3.0       1000.30       0.00       0.00         4.0       1000.30       0.00       0.00         4.0       1000.30       0.00       0.00         4.0       1000.30       0.00       0.00 <t< td=""><td>83236003</td><td>9.0</td><td>749.88</td><td>0.03</td><td>3.425</td><td>-0.224</td></t<>	83236003	9.0	749.88	0.03	3.425	-0.224
3.49.19       9.93       3.425         3.6       751.28       9.93       3.432         3.9       751.28       9.99       3.446         3.9       751.28       9.99       3.446         3.9       751.86       9.91       3.446         3.9       751.86       9.91       3.446         3.9       751.86       9.91       3.446         3.9       9.98.99       9.94       8.428         3.9       9.98.99       9.94       8.418         3.9       9.98.99       9.94       8.418         3.9       9.99.46       9.94       8.424         3.9       9.99.46       9.94       8.424         3.9       9.99.46       9.94       8.424         3.9       1000.15       9.94       8.424         3.9       1000.15       9.93       8.424         3.9       1000.15       9.93       8.424         3.9       1000.15       9.93       8.424         3.9       1000.15       9.93       8.424         3.9       1000.16       9.93       8.424         3.9       1000.16       9.93       8.421	83236004	9	751.04	0.03	3.442	-0.227
3.6       749.77       0.00       3.432         3.6       751.28       0.00       3.446         3.0       751.28       0.00       3.452         3.0       751.28       0.00       3.452         3.0       998.99       0.01       3.452         3.0       998.99       0.00       0.04       0.446         3.0       998.99       0.00       0.04       0.446         3.0       998.99       0.04       0.441       0.441         3.0       999.46       0.04       0.441       0.441         3.0       1000.43       0.04       0.441       0.441         3.0       1000.44       0.04       0.441       0.441         3.0       1000.44       0.04       0.441       0.441         3.0       1000.44       0.04       0.441       0.441         3.0       1000.44       0.04       0.441       0.441         3.0       1000.44       0.04       0.04       0.426         3.0       1000.44       0.03       0.04       0.426         3.0       1000.44       0.03       0.04       0.426         4.0       1000.43       0	83236103	9	749.19	0.03	•	<b>-0</b> .232
3.6       751.62       6.00       3.446         3.0       751.28       6.00       3.446         3.0       751.28       6.00       3.446         3.0       751.86       6.00       3.429         3.0       998.99       6.00       3.429         3.0       998.99       6.00       3.429         3.0       998.99       6.00       6.418         3.0       999.46       6.42       6.424         3.0       999.46       6.00       6.424         3.0       999.46       6.00       6.424         3.0       1000.73       6.00       6.424         3.0       1000.73       6.00       6.424         3.0       1000.73       6.00       6.43         3.0       1000.73       6.00       6.43         4.0       6.00       6.00       6.43         4.0       6.00       6.00       6.43         4.0       6.00       6.00       6.43         4.0       6.00       6.00       6.00         4.0       6.00       6.00       6.00         4.0       6.00       6.00       6.00         4.0	83236104	(A)	749.77	0.03	•	<b>-0</b> .228
3.6       751.28       0.00       3.446         3.0       750.70       0.01       3.446         3.0       77.88       0.01       3.446         3.0       998.99       0.04       0.04       0.423         3.0       998.99       0.04       0.04       0.423         3.0       998.99       0.04       0.04       0.423         3.0       1001.08       0.04       0.04       0.423         3.0       1001.08       0.04       0.04       0.422         3.0       1001.08       0.04       0.04       0.422         3.0       1000.04       0.04       0.04       0.424         4.0       1000.04       0.04       0.04       0.424         3.0       1000.04       0.03       0.04       0.434         4.0       1000.07       0.03       0.04       0.434         4.0       1000.07       0.03       0.04       0.434         4.0       1000.07       0.03       0.04       0.434         4.0       1000.07       0.03       0.04       0.04         4.0       1000.07       0.00       0.00       0.00         4.0	83237998	9.	751.62	0.00	•	-0.235
3.6       750.70       0.01       3.440         3.0       749.77       0.02       3.429         3.0       998.99       0.04       0.458         3.0       998.99       0.04       0.418         3.0       998.99       0.04       0.418         3.0       999.46       0.04       0.418         3.0       999.46       0.04       0.418         3.0       999.46       0.04       0.424         3.0       999.46       0.04       0.424         3.0       1000.15       0.04       0.424         3.0       1000.15       0.03       0.441         3.0       1000.15       0.03       0.424         3.0       1000.15       0.03       0.424         4.0       1000.35       0.03       0.424         4.0       1000.35       0.03       0.424         4.0       1000.35       0.00       0.02       0.424         4.0       1000.35       0.00       0.00       0.425         4.0       1000.43       0.00       0.00       0.00         4.0       1000.43       0.00       0.00       0.00         4.0	83237841	9.0	751.28	0.00		-0.232
3.6       749.77       0.02       3.429         3.6       998.99       0.04       0.420         3.6       998.99       0.04       0.420         3.0       998.99       0.04       0.418         3.0       998.99       0.04       0.418         3.0       999.46       0.04       0.441         3.0       999.46       0.04       0.441         3.0       1000.15       0.04       0.441         3.0       1000.15       0.04       0.441         3.0       1000.15       0.04       0.441         3.0       1000.15       0.04       0.441         3.0       1000.15       0.04       0.441         3.0       1000.15       0.03       0.441         3.0       1000.15       0.03       0.441         3.0       1000.15       0.03       0.444         4.0       1000.13       0.03       0.444         4.0       1000.13       0.03       0.444         4.0       1000.13       0.03       0.044         4.0       1000.13       0.03       0.044         4.0       1000.13       0.03       0.044	83237073	3.0	750.70	6.01	3.440	<b>-0</b> .232
3.68       751.86       -0.10       3.458         3.0       998.99       0.04       6.420         3.0       998.99       0.04       6.418         3.0       999.23       0.04       6.418         3.0       999.23       0.04       6.418         3.0       999.23       0.04       6.424         3.0       999.81       0.04       6.424         3.0       1000.15       0.03       6.424         3.0       1000.15       0.03       6.424         3.0       1000.15       0.03       6.424         3.0       1000.15       0.03       6.424         3.0       1000.25       0.03       6.424         4.0       1000.25       0.03       6.424         4.0       1000.25       0.06       6.426         4.0       1000.25       0.06       6.426         4.0       1000.26       0.06       6.426         4.0       1000.26       0.06       6.426         4.0       1000.26       0.06       6.426         4.0       1000.26       0.06       6.426         4.0       149.65       0.06       6.06	83237074	9.0	749.77	9.62	3.429	<b>-0</b> .227
3.6 998.99 9.6 4.20 3.6 998.99 9.6 9.6 4.4 188 3.6 10.6 1.5 10.6 1	83237078	3.0	751.86	<b>.</b> 6. 10	3.458	<b>-0</b> .236
3.6       998.99         3.6       998.99         3.6       998.99         3.6       999.23         3.6       999.23         3.6       999.46         3.6       999.46         3.6       999.46         3.6       999.46         3.6       1000.03         3.6       1000.04         3.6       1000.04         3.6       1000.04         3.6       1000.04         3.6       1000.04         3.6       1000.04         3.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6       1000.04         4.6	83229051	3.0	998.99	0.03	6.420	<b>-0</b> .285
3.0 998.99 3.0 6.044 3.0 1901.08 3.0 1909.23 3.0 1909.24 3.0 1900.15 4.0 1900.15 4.0 1900.15 3.0 1900.15 4.0 1900.16 3.0 1900.16 4.0 1900.16 3.0 1900.	83229052	G.0	868.88	<b>9</b> .0 <b>4</b>		<b>-9</b> .286
3.0       999.23       9.04       6.422         3.0       999.46       9.04       6.424         3.0       999.46       9.03       6.424         3.0       999.46       9.03       6.434         3.0       1000.97       9.03       6.434         3.0       1000.93       6.434       6.434         3.0       1000.93       6.434       6.434         3.0       1000.33       0.03       6.434         3.0       1000.33       0.03       6.434         4.0       999.57       0.03       6.436         4.0       50.51       0.00       6.426         4.0       100.43       0.00       6.426         5.0       5.3       0.00       6.426         4.0       100.23       0.00       6.426         4.0       100.24       0.00       6.426         4.0       100.20       0.00       6.426         4.0       100.20       0.00       6.426         4.0       100.20       0.00       6.426         4.0       100.20       0.00       6.426         4.0       100.20       0.00       6.426	83229053	3.0	998.99	40.0		<b>-6</b> .291
3.9       1991.98         3.9       999.46         4.0       999.46         5.0       999.46         6.424       6.424         7.0       1999.46         6.43       6.43         7.0       1999.46         6.43       6.43         7.0       1999.46         6.6       6.43         7.0       1999.57         8.0       6.63         8.0       6.43         8.0       6.43         8.0       6.43         8.0       6.43         8.0       6.43         8.0       6.43         8.0       6.43         8.0       6.43         8.0       6.42         8.0       6.43         8.0       6.42         8.0       6.42         8.0       6.42         8.0       6.42         8.0       6.42         8.0       6.42         8.0       6.42         8.0       6.42         8.0       6.42         8.0       6.42         8.0       6.42         8.0 <t< td=""><td>83229054</td><td>3.0</td><td>999.23</td><td>9.0</td><td></td><td><b>-6</b>.298</td></t<>	83229054	3.0	999.23	9.0		<b>-6</b> .298
3.99.46       9.99.46       9.99.81         3.0       9.99.81       9.99.81       6.424         3.0       1989.46       9.93       6.424         3.0       1989.87       9.93       6.424         3.0       1989.87       9.93       6.424         3.0       1989.83       9.93       6.43         3.0       1989.57       9.96       6.426         3.0       1989.57       9.99       6.426         4.0       59.51       9.99       6.188         4.0       199.29       9.99       6.188         4.0       199.29       9.99       6.188         4.0       199.29       9.99       6.188         4.0       149.65       9.99       6.99       6.188         4.0       150.82       9.99       6.99       6.53         4.0       149.65       9.99       6.99       6.53         4.0       149.65       9.99       6.99       6.99         4.0       149.65       9.99       6.99       6.99         4.0       150.82       9.99       6.99       6.53         4.0       150.82       9.99       6.99       6.53 </td <td>83229055</td> <td>Ø.8</td> <td>1001.08</td> <td>9.04</td> <td></td> <td><b>-8</b>.295</td>	83229055	Ø.8	1001.08	9.04		<b>-8</b> .295
3.0       999.81       6.641         3.0       1999.46       6.641         3.0       1999.46       6.424         3.0       1999.83       6.434         3.0       1999.83       6.434         3.0       1999.73       6.43         3.0       1999.73       6.43         3.0       1999.57       6.63         5.0       6.43         3.0       999.57       6.96         6.42       6.42         7.0       999.69       6.42         6.43       6.43         7.0       999.69       6.42         6.43       6.43         7.0       999.69       6.42         6.43       6.43       6.43         7.0       999.69       6.42         6.43       6.43       6.43         7.0       999.69       6.42         6.43       6.43       6.43         7.0       999.69       6.90         6.43       6.90       6.18         7.0       999.69       6.90         7.0       999.69       6.90         7.0       999.69       6.90         7.0	83229058	G.9	999.46	6.63	6.424	<b>6</b> .29
3.0       999.46       9.93.46       9.93.46         3.0       1990.15       9.93       6.434         3.0       1990.97       9.93       6.434         3.0       1990.93       6.436       6.432         3.0       1990.53       9.95       6.426         3.0       1990.53       9.96       6.426         4.0       50.51       9.96       6.426         4.0       190.51       9.90       6.168         4.0       190.43       9.90       6.188         4.0       190.20       9.90       6.188         4.0       149.65       9.90       6.90       6.188         4.0       150.83       9.90       7.536       7.536         4.0       150.83       9.90       7.536       7.594         4.0       150.83       9.90       7.516       7.594         4.0       200.16       9.90       7.517       7.594         4.0       200.16       9.90       7.517       7.594         4.0       200.16       9.90       7.517       7.594         4.0       9.90       9.90       9.90       7.594         4.0       9.90	83229059	J.0	999.81	0.04 +	6.430	-6.291
3.6       1966-15       6.434         3.6       1966-85       6.434         3.6       1966-85       6.434         3.6       1966-73       6.43         3.6       1966-73       6.43         3.6       1966-73       6.43         3.6       1966-73       6.42         3.6       1966-73       6.42         4.6       56       6.42         4.6       166-51       6.96       6.42         4.6       166-43       6.96       6.168         4.6       166-43       6.96       6.188         4.6       166-43       6.96       6.188         4.6       166-43       6.96       6.188         4.6       166-43       6.96       6.188         4.6       166-26       6.96       6.96         4.6       166-26       6.96       7.53         4.6       166-26       6.96       4.586         4.6       166-26       6.96       4.586         4.6       166-26       6.96       7.51         4.6       166-26       6.96       7.51         4.6       166-69       6.96       7.52	83236005	9. 9.	999.46	6.63	6.411	<b>-6</b> .261
3.6       1966.37       6.434         3.6       1966.39       6.432         3.6       1966.73       6.63       6.434         3.6       1966.73       6.65       6.432         3.6       999.57       6.96       6.426         3.6       599.57       6.96       6.426         4.6       49.69       6.168       6.188         4.6       196.43       6.96       6.188         4.6       166.43       6.96       5.365         4.6       156.26       6.96       7.375         4.6       156.28       6.96       4.586         4.6       156.83       6.96       4.586         4.6       156.83       6.96       4.586         4.6       266.16       6.96       3.813         4.6       266.16       6.96       3.813         4.6       266.16       6.96       3.813	83236006	89 (	1666.15	6.63 5.63	0.424	2.29
3.6       3.6       4.7       4.8 </td <td>83236007</td> <td>8. F</td> <td>1666.97</td> <td>9.6</td> <td>404.0</td> <td>- 100 - 100</td>	83236007	8. F	1666.97	9.6	404.0	- 100 - 100
3.6       3.6       4.6       5.3       6.6       6.6       6.7       6.8       6.8       7.3       7.3       7.3       7.3       7.3       7.4       6.6       7.8 </td <td>83230000</td> <td>9 (1 1 (2)</td> <td>1000</td> <td>200</td> <td>40.40</td> <td>8.7.9</td>	83230000	9 (1 1 (2)	1000	200	40.40	8.7.9
3.6     999.57     6.422       3.6     999.57     6.422       3.6     56.51     6.06     6.188       4.6     49.69     6.188       6.0     6.0     6.188       6.0     6.188       6.0     6.188       6.0     6.0       6.0     6.188       7.3     6.9       7.3     6.9       7.3     6.9       7.3     7.3       7.3     7.3       7.3     7.3       7.3     7.3       7.3     7.3       7.3     7.3       7.4     7.4       7.4     7.4       7.5     7.5       7.5     7.5       7.6     7.8       7.6     7.8       7.6     7.8       7.7     7.8       7.8     7.8       7.6     7.8       7.7     7.8       7.7     7.8       7.8     7.8       7.8     7.8       7.8     7.8       7.7     7.8       7.8     7.8       7.7     7.8       7.7     7.8       7.7     7.8       7.7     7.8 <t< td=""><td>8222008</td><td>9.6</td><td>1000.13</td><td></td><td>0.430</td><td>9.20</td></t<>	8222008	9.6	1000.13		0.430	9.20
4.0 5.0 5.3 5.3 6.3 6.4 6.4 6.4 6.4 6.4 6.4 6.4 6.4 6.4 6.4	2400070	D	999.53		6. 422	900
4.0	1/00/200	) e	000	9	6. 426	282
4.0	8004405	9 6	50.00	9 6	891.9	9-149
4.0 160.43 0.00 5.365 6.00 4.00 160.20 0.00 5.375 6.00 6.00 6.00 6.375 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.0	82244007	. 4	40 69 40 69	98	6.188	
4.0 160.20 0.00 5.375 6.00 4.594 6.00 4.594 6.00 4.594 6.00 4.580 6.00 4.580 6.00 4.580 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.	8224307	9 6	100.43	90.0	5.365	
4.6 149.65 6.00 4.594 4.0 4.6 150.82 6.00 4.580 4.580 4.0 4.0 200.16 6.00 3.813 4.0 4.0 200.51 6.00 3.813 4.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	82244069	. 4 . e	166.28	99.99	5.375	
4.0 150.82 0.00 4.580 b. 4.0 200.16 0.00 3.813 b. 4.0 200.51 0.00 3.811 b. 4.0 249.84 0.00 3.059 b.	82243829	€.	149.65	8.6	4.594	•
4.0 200.16 0.00 3.813 6.00 4.050 4.050 6.00 3.050 6.00 3.050 6.00 8.050 6.00 8.050 6.00	82244011	6.4	150.82	00.00	4.580	
4.0 200.51 0.00 3.811 L0 4.0 3.059 L0	82243031	4.0	200.16	9.00	3.813	<b>-0</b> .205
4.6 249.84 6.66 3.659 —6	82244013	4.0	200.51	<b>9</b> .00	3.811	<b>9</b> .204
	82243033	4 1	70 070	***	~ ·	•

Domping, 1/sec	<b>-6</b> . 190	9.181	- 4				-6.177	<b>9</b> .169	-0.147	. 153	6.129	4	? ?	215	-0.247	-0.240	-0.249	-0.287	<b>6</b> .271	<b>-6</b> .311	<b>-6</b> .303	6.337	<b>-0</b> .342	<b>-6</b> .382	<b>-6</b> .378			40.0	9	9 198	-6.188	<b>-6</b> . 191	<b>-6</b> .185	<b>-0</b> .186	<b>-6</b> .175	<b>-6</b> .173		_		-6.165	47.	<b>6.133</b>	<b>-0</b> .123
Frequency,	2.689	2.691	•	2.479	•	•	2.111	2.104	1.602	1.615	1.176	D 00	0.800	0.43/ A 467	1.19	1.791	1.764	3.064	3.045	4.289	4.277	5.479	5.467	6.639	6.648	6.168	6.195	0.70	100.5	10 CC M	3.639	3.047	2.682	2.672	2.455	2.453	2.305	2.311	2.100	2.100	1.586	1.588	9.906
Shaft angle, deg	•	<b>.</b>	8 8	90	98	99.	9.00	90.0	90.	9.00	<b>6</b> .00	<b>8</b> 6	9 6	9 q	8 6	90	66.6	98	90.0	9.00	<b>9</b> .00	9.00	<b>9</b> .00	<b>9</b> .00	<b>9</b> .00	9	9.99	9.0	9 6	9 6	3 6	99.	9.00	99.	9.0	9.00	<b>9</b> .00	<b>8</b> .	<b>9</b> .99	<b>9</b> .00	<b>8</b> 0.00	<b>0</b> .00	<b>9</b> .00
Rotor speed, rpm	275.16	275.04	80.807 080 000	289.57	300.23	300.23	314.77	315.59	349.92	349.22	380.16	389.26 200.04	10.880 10.003	500.38 500.58	549.61	601.41	5000	701.25	699.84	806.51	789.92	88.68	88.68	1000.08	989.73	50.51	48.75	188.55	98.20	100 00	250.78	250.08	274.92	275.63	290.16	290.39	300.59	300.00	314.77	314.77	350.51	350.27	399.26
Collective pitch, deg	4.	4 ·		÷ →	4.0	4.0	4.0	4.0	<b>4</b> .0	<b>4</b> .0	<b>4</b> •	<b>9</b> .	• •		4	9.	4.0	4	4.0	4.0	4.0	<b>•</b> .•	<b>6.</b>	<b>4.</b>	<b>9.</b>	6.			<b>D</b> 6	9 6	• • • • • • • • • • • • • • • • • • •	9	9.9	6.9	6.9	6.6	6.0	6.9	<b>9</b> .0	<b>9</b> .0	9.0	<b>6</b> .0	<b>.</b>
Data point number	82259037	82259043	82259639	82259046	82243035	82244017	82259041	82259048	82243037	82244019	82244021	8284288	67944770	8224403	82243045	82243047	82244027	82243049	82244029	82243052	82244031	82243054	82244033	82243056	82244035	82258013	82258848	82238013	07720020	R2258017	82258019	82258054	82259001	82259007	82259003	82259009	82258021	82258056	82259005	82259011	82258024	82258058	82258026
Rotor	н,	<b></b> •	<b></b>	•	<b>.</b>	<b>-</b>			<b>-</b>	<b></b>		<b>→</b> •	→ +-		•		•		-	-	<b>—</b>	<b>  </b>	<b>-</b>	<b></b> 1	<b></b> •	→•		<b></b> 4 ▶-	→ -			. 🛏	-	-	-	-	-	-	<b></b>	⊷,	<b></b>	-	-

TABLE 6.—CONTINUED

Damping. 1/sec	6.149	9.466	<b>6</b> .234	<b>-6</b> .293	<b>4</b> %. <b>9</b>	9.358 9.358	<b>-0</b> .292	9.40	-6.418		197	<b>-6.48</b> 5	-0.418	<b>6.437</b>	<b>462.9</b>	<b>-6.456</b>	<b>-0.35</b> 2	9.367	4.	-9.465	6.439	6.413	-0.421	-0.427	<b>6</b>	-0.423	<b>-0.4</b> 23	-0.427	-6.439	₽.£	<b>4.</b>	4.43	<b>-6.59</b> 7	-9.486	96.288 P	9.558	484.9	<b>-0.520</b>	<u>‡</u>	97.9	992.9	9.566	-6.583	578	4	170.9
Frequency. Hz	6.893	0.479	0.451	1.779	1.783	1.777	1.777	3.039	3.055	3.045	3.658	3.689	3.676	3.429	3.434	3.436	3.427	3.454	3.419	3,432	3,432	3.417	3.432	3.423	3.431	3.431	3.438	3.438	3.434	3.425	4.295	4.283	5.475	5.475	6.660	6.669	6.412	6.440	6.424	6.418	6.416	6.412	6.447	6.434	A 422	774.0
Shaft angle, deg	99.69	00.0	90.0	99.9	99.9	0.00	99.00	90.00	00.00	00.00	00.00	00.00	90.00	99.99	99.9	0.03	0.03	6.63	6.63	9.63	6.63	0.02	-19.96	-19.95	-19.95	-19.93	-19.92	-19.99	-19.98	-19.98	<b>9</b> .00	9.00	00.00	9.00	99.9	0.00	6.63	0.03	99.9	<b>-0.04</b>	-19.95	-19.95	-19.96	19.96	40.01	מישם מישם
Rotor speed, rpm	100.55	500.39	500.16	600.35	600.23	600.23	600.00	69.0	700.66	96.669	749.18	751.41	750.35	750.46	750.70	749.65	749.88	751.28	749.65	749.88	749.88	748.84	749.65	748.96	749.54	749.42	750.23	750.58	750.23	749.54	801.33	800.04	899.18	899.88	96.666	1000.08	999.81	1000.04	999.23	998.76	998.41	997.83	1000.62	10000	0000	880.00 880.00
Collective pitch, deg	6	9	6.9	6.9	6.9	6.9	6.9	9	9	8.9	6.9	6.9	6.9	6.9	6.9	8.9	8	9	9	9	9	9		9	9	6.9	6.9	6.9	6.9	6.9	6.9	6.9	6.9	6.0	6.9	<b>6</b> .0	6.0	6.0	6.9	6.9	6.9	6.6	6.6	6	) q	D. 0
Data point	RODERBER	82258028	82258962	82258030	82258044	82258045	82258064	82258032	82258043	82258066	82258034	82258042	82258968	83242000	83242901	8324.24.72	83242003	83242004	83242005	83242006	83242987	83242013	83242014	83242015	83242016	83242022	83242023	83243000	83243001	83243002	82258036	82258070	82258038	82258072	82258040	82258074	83242008	83242009	83242010	83242011	83242017	83242018	83242019	81242020	10001010	83242021
Rotor	-	•		-	-	-			• •			-		II	II	1	-	:	:=	:=	4 II-		:=	::	-	11	II	11	II	II	-	<b>—</b>	<b>-</b>	_	<b>-</b>	-	11	I	II	I	I	II	Ξ	:=	4 F	11

			TABLE 6.—CONCLUDED	a		
Rotor	Data point number	Collective pitch, deg	Rotor speed,	Shaft angle, deg	Frequency, Hz	Domping. 1/sec
-	R2245015	6	49 RB	6	6.164	-B. 156
•	82244039	9 6	90.001	9 6	5,338	-6. 183
• •	82245017	. 60	100.08	90.0	5.350	9.500
	82244041	60	151.29	9.00	4.549	<b>.</b> 181
	82244043	60	199.69	9.00	3.789	<b>-0</b> .227
-	82245021	9.	200.63	0.00	3.781	<b>→</b> . 222
-	82259019	<b>6</b>	275.39	00.0	2.658	<b>-6</b> .264
-	82259825	80.	275.27	00.0	2.660	<b>-6</b> . 196
-	82259021	8.0	291.33	9.00	2.422	<b>-6</b> .188
	82259027	8.0	290.98	00.00	2.426	<b>-6</b> .186
-	82244045	<b>9</b> . <b>9</b>	299.30	9.00	2.301	<b>-6</b> .186
H	82245023	<b>8</b> . <b>0</b>	300.12	9.00	2.295	<b>-6</b> .189
-	82259023	<b>9.0</b>	315.47	99.90	2.074	<b>4</b> .163
-	82259029	9.0	315.00	9.00	2.686	<b>9</b> .160
-	82244947	<b>9</b> .	379.69	99.90	1.170	<b>-6</b> .125
-	82245025	●.	379.57	99.9	1.176	<b>9</b> . 195
<b>-</b>	82245648	8.0	379.92	9.00	1.164	<b>6</b> .138
-	82245027	<b>9.0</b>	399.73	99.9	868.0	<b>J</b> 135
-	82245013	<b>9</b> .8	564.73	9.60	1.307	<b>9.329</b>
-	82245046	●.	565.43	<b>6</b> .66	1.334	<b>9</b> .452
-	82244053	●.	599.06	99.9	1.779	-6.463
_	82244055	<b>9</b> .	700.08	99.9	3.057	<b>-0</b> .502
-	82245034	<b>9</b> .	699.73	<b>9</b> 0.0	3.037	<b>9</b> .278
<b>-</b>	82244057	9.0	799.57	9.00	4.289	<b>-6</b> .557
-	82245007	9.6	800.39	<b>6</b> .66	4.295	999.
<b>-</b>	82245036	<b>.</b>	800.74	<b>8</b> .00	4.291	<b>→</b> .727
-	82245038	⊕.	800.16	<b>6</b> 0.00	4.291	-6.736
-	82245040	<b>9</b> . <b>6</b>	801.56	99.9	4.307	<b>-6</b> .698
-	82245969	<b>8</b> 9.	966.35	<b>9</b> .00	5.467	<b>-6</b> .764
<b>-</b>	82245042	<b>.</b>	999.59	<b>6</b> .60	5.498	-6.655
<b>-</b>	82245011	<b>6</b> 0	1000.08	9.00	6.672	-8.863
-	82245044	9.	999.49	98.	6.639	/9/. <b>P</b>

TABLE 7. -- REGRESSING LEAD-LAG MODE DATA IN HOVER, CONFIGURATION WITH STRUCTURAL FLAP-LAG COUPLING

Damping. 1/sec	-0.153 -0.154	6.082 5.77	157	<b>-0</b> .152	-6.156	-6.695	-6.692		• .	9.16	Υ.	Τ.	6.114	<b>-6</b> .189	<b>-0</b> .175	-0.221	<b>9</b> . 189	<b>6</b> .175	<b>6.177</b>	•	• `	9 9 9	-6.197		•	•	<b>-6.136</b>	<b>.</b> 135	-8.283	9.1/6		<u> </u>	•	9 9	470	627	<b>-6</b> . 155	7.9	9.140	-B. 157	<b>-6.153</b>
Frequency.	6.201	6.443 8.451	5.37	5.387	5.377	5.627	5.654	4.00% 90%	000. F	3.822	3.842	4.059	4.088	3.068	3.070	2.709	2.705	2.709	2.709	2.482	7.400	2.334	2.330	2.332	2.318	2.340	2.512	2.512	2.121	2.119	2.169	1.623	, po	56.	- e	450	6.918	1.166	1.156	9.441	0.463
Shaft angle, deg	6.6 6.0 6.0	6 6 9 9	9 6	90.	<b>9</b> .00	e.e.	e.e	9 6 9 6	9 6		98.	<b>6</b> .	<b>.</b> <b>.</b> <b>.</b>	<b>9</b> 0.00	<b>9</b> 0.0	<b>9</b>	90.0	9.00	99.	<b>6</b>	90.0	90.0	99.9	0.00	99.0	90.	40.0	e e	90.0		9.0	99.60		9.6	9 6		99.9	4	6.6	99.9	00.0
Rotor speed.	49.57 50.98	50.82 80.82	20.02 100.02	99.73	100.78	101.87	100.36	149.41	200.000	200.00	199.34	200.84	200.84	250.66	250.43	275.16	275.27	274.92	274.80	290.27	286.64	208.00 70 47	301.05	300.23	301.17	299.88	300.05	300.86	315.00	315.23	316.03	350.15	110.00	80.8/C	100.00	100.00	399.61	400.29	66.60		566.98
Collective pitch, deg	9 <b>9</b>	9.6	9 6	9 9	0.0	<b>.</b>	<b>0</b> .0	<b>9</b> .0	<b>9</b> 6	<b>9 4</b>		9.0	9.0	9.0	<b>9</b> .0	<b>9</b> . <b>9</b>	<b>9</b> . <b>9</b>	<b>9</b> .9	<b>9</b> .0	<b>0</b> .0	9.0	<b>D G</b>			0.0	<b>0</b> .0	<b>9</b> .	<b>0</b> .0	<b>.</b>	<b>6</b>	9 (	9 G	9.0	9 G	9 6	9 6		9	9	6	) <b>©</b>
Data point number	82239001 82242041	83222012	C19277C0	82242044	82260007	83222014	83222015	82239005	82242646	62239007 82242948	8225040	83222016	83222017	82239009	82242750	82259056	82259062	82259063	82259064	82259058	82229068	82239869	R2242908	82242052	82246001	82260011	83222018	83222019	82259060	82259072	82259073	82242010	4507470	82245063	07770011	82242012 82242056	82268013	83222020	83222021	82242060	82260015
Rotor	нн	Ξ:	<b>:</b> -	4 F-4	<b>—</b>	=======================================	=	<b></b> •	~ <b>4</b> F		-	11	=	·			_	<b></b>	<b>-</b>	⊷ :	<b>-</b> 4 •	<b></b> }-	• -	• •		-	II	II	-	<b></b> 1	<b>-</b>	}-	<b>-</b>	<b></b> 4 P-	t-	<b>→</b> ►	<b>-</b>		-		••

Damping. 1/sec	<b>6</b> .169	<b>6</b> .151	4.1	‡ :	2	6.142	9 4	: -	-6.135	<b>-0</b> .128	<b>-6</b> .129	<b>6.128</b>	τ.	4.14	6.147		92.5	137	: -:	Γ.	٠.				-	<b>6.134</b>	-0.142	97.9	9	<b>6</b> .142	<b>-0</b> .142	e. 143	٦,	9	9		<b>6</b> .142	-0.143	<b>-0</b> .142	9.142	7.9
Frequency.	0.475	1.115	1.123	1.326	410.1	1.775	707.1	1.77.1	1.524	1.532	1.545	1.533	1.783	2.406	2.396	2.65	5.040 040	2.8.5	2.823	2.818	2.802	3.061	400.0 F	3.000	3.440	3.446	3.456	3.444 446	3,432	3.429	3.427	3.425	3.429		7.41				•	3.440	3.434
Shaft angie, deg	-21.00	98.	•	96.0	99.0	9.6	9 6	9 6	9.0	9.65	0.03	<b>9</b> .0	-21.00	<b>8</b> .60	<b>6</b>		<b>9</b> 6	3 5		0.0	6.63	-21.00	9 6	9.00	40.0	9.0	0.02	6.63 6.63		90.0	0.02	9.00	6.65	9.6	<u>*</u>	98	9.93	<b>6</b> .61	<b>6</b> .0	6.67	6.67
Rotor speed, rpm	588.74			565.66	564.84	600.59	09. 666 41. 666	800.00	599.28	600.21	601.02	699.21	600.82	649.80	648.52	689.26	98.80	79.057	701.15	786.46	699.30	701.25	7.00.50	750.03	750.46	751.16	751.62	750.70	25.00	750.00	749.54	749.42	749.54	747.91	740.48	87. 62.V	749.77	749.07	749.88	750.58	750.12
Collective pitch, deg	0.0	<b>6</b> .0	• · •	<b>.</b>	9.0	<b>9 9</b>	D 6	9 6	9.0	<b>9</b> . <b>0</b>	<b>9</b> . <b>9</b>	<b>0</b> .	<b>9</b> .0	<b>.</b>	<b>.</b>	<b>.</b>	9.6		9.0	0.0	9.0	<b>.</b>		9.6	. 6	0.0	<b>9</b> .0	<b>9</b> 6	9 9	0.0	<b>0</b> .0	• •	<b>.</b>	9 G	9.6	9 6	9.	0.0	9.0	<b>9</b> .	<b>9</b> .
Data point number	82260032	82242018	82242062	82246985	0724003	82242828	92747804	82260017	83222024	83222025	83222030	83222031	82260030	82242022	82242066	47874779	82269419	83222926	83222027	83222032	83222033	82260829	07874770	81222814	83222035	83222036	83222037	83222046	83223000	83223001	83223039	83223646	83223861	63223662	025200 81227472	83224000	83224001	83228000	83228001	83229000	83229001
Rotor		<b>-</b>	<b>–</b> (	<b>⊣</b> •	r	→ -	<b></b>	• •	11	11	-	I	<b>,</b>	<b></b> •	~- p.	<b>-</b> -	<b>-</b>	ï	:=	11	I.	<b>-</b>	<b>-</b>	· -	II	11	II	] <u>-</u>	:::	II	11	II:	7:	11	1 -		II	11	I		II

Domping. 1/sec	-6.161	<b>-0.170</b>	<b>9</b>	<b>.</b> 161	<b>9.145</b>	<b>6.143</b>	<b>-0</b> .172	<b>-6.171</b>	4.7	<b>6</b> .173	-0.172	9.13	-6.16g	40.04	9.151	9	- 185 185	90.1	-a. 186						<b>-6</b> .156	<b>-9</b> .169	<b>9</b> .162	. 161 161	<b>a</b> . 161	-6.161		9 4	9	- 163	-B. 162		<b>J</b> 163	<b>-0</b> .161	<b>-9</b> .159	<b>-6</b> . 158	<b>-6</b> . 158	<b>-0</b> .159	<b>a</b> . 163	<b>4</b> .163	<b>.6</b> . 191
Frequency,	3.684	4.285	4.281	4.273	4.040	4.04	4.871	4.891	4.879	5.480	5.482	5.488	5.488 5.68	5.264	5.260	80.0	6.951	8.6/6	6.639	6.637	6.658	6.643	6.646	6.436	6.420	6.428	6.422	6.420	6.440		6.436	6.438 438	817.8	6.428	6.432	6.411	6.422	6.430	6.411	6.436	6.424	6.422	6.422	6.432	7.217
Shaft angle, deg	-21.66	9.99	<b>.</b>	<b>9</b> .00	0.02	0.03	<b>9</b>	<b>9</b> .00	90.00	<b>9</b> .00	<b>6</b>	80.00	9.00	9.9 ?	6.63	90.0	9.00	9.00	9.00	90.0	9. 9.	96.	9.00	-0.02	-0.02	0.03	0.03	0.03	. 6. . 63	9.62	9.62	29.9 10.0	9	60.0	10.0	9.0	0.03	0.03	90.00	<b>9</b> .	<b>9</b>	-6.61	0.67	0.07	<b>6</b> .60
Rotor speed, rpm	751.52	801.21	800.63	799.80	799.20	799.54	849.61	851.02	850.43	966.47	900.04	900.00	906.47	866.72	996.69	78.848	949.45	958.16	999.61	999.49	1969.66	999.84	1666.43	1000.39	999.23	999.81	999.23	999.34	1666.62	999.23	1666.59	+9.9991	1000	28.68	1000.04	998.41	999.23	69.66	998.18	1000.15	999.34	999.11	999.46	1666.15	1049.18
Collective pitch, deg	9.	0.0	<b>9</b> .	<b>9</b> .	• •	<b>9</b> .	<b>9</b> . <b>9</b>	<b>.</b>	<b>9</b> . <b>9</b>	<b>9</b> .0	<b>9</b> .	9. 9.	9.6	9.	9.6	9 (	<b>.</b>	9.	9. 9	<b>9</b> .	<b>9</b> .0	<b>0</b> .0	<b>o</b> .	<b>9</b> .	<b>0</b> .0	<b>.</b>	<b>o</b> .	<b>9</b> . <b>9</b>	<b>o</b> .	<b>9</b> .6	9 ( 9 (	<b>9 4</b>	9	9 6	6	9.0	0.0	<b>9</b> . <b>0</b>	<b>0</b> .0	<b>9</b> . <b>9</b>	<b>0</b> .0	<b>0</b> .0	<b>0</b> .	<b>9</b> .	<b>0</b> .
Data point number	82260027	82242028	82243007	82260021	83222038	83222039	82242031	82242033	82243009	82242035	82243011	82258021	82260023	83222040	83222041	8224263/	82243013	82250023	82242939	82243915	82250025	82260025	82263001	83222028	83222029	83222042	83222043	83222044	83222045	83223116	85223117	83223118	0100100	83224003	83224030	83224031	83224060	83224061	83224092	83228002	83228003	83228004	83229862	83229003	82250027
Rotor	-	-	<b>-</b>	<b>-</b>	=	I	<b></b>	<b>—</b>		-		<b></b> 4 :	٦;	I	Ι,		<b></b> -	<b></b>	<b></b>	<b>—</b>		<b>-</b>	<b>-</b>	11	11	1	I	11	1	I:	Ξ:	] <b>:</b>	: =				I	==	==	11	11	11	II	:	<b>-</b>

Damping. 1/sec	<b>-6</b> .198	-0.072	6.675	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		9		- 129	4	<b>6</b> .175	₩.172	<b>-0</b> .254	<b>-0</b> .228	<b>6.243</b>	-0.243	<b>-0</b> .251	<b>6</b> .249	9.248	80.79	247.0	247.	25.0	9.242	4.246	6.243	77.9	77.79	978	<b>6</b> .241	-6.234	9.249	-6.256	9.54	-6.249	4.244	9.245	-6.245	707.9	6.246	4.24	6.246	9.7.9	<b>-6.238</b>	-6.238
Frequency, Hz	7.781	6.457	6.478	6.459	0.040	5.65 60 60 60 60 60 60 60 60 60 60 60 60 60	• • •	4.682 595	708.0	1.170	1.168	1.535	1.532	2.825	2.827	3.431	3.432	3.432	3.427	5.4.50	3.431	3.434	3.442	3.436	454.6	104.0	**************************************	2.442	446	3.434	3.440	3.450	3.448	3.432	3.432	3.427	7.4.6	0.440	5.4.5	5.448	3.423	5.448	3.436	3.429
Shaft angle, deg	9.00	6.67	9.07	6.67 70.0	6.67	6.67	(a.e)	<b>6</b> .67	) d d	) e	6.67	6.1	9.11	9.60	<b>9</b> 0.00	<b>9</b> .	<b>9</b> .00	90.0	<b>9</b>	6.63	6.63	6.63	6.65	-0.05	9.0	49.9		9.60	7 P. G	9.00	6.63	0.0	0.03	0.03	-0.67	6.67	-19.92	-19.92	-19.97	-19.98	-19.98	-19.97	-20.00	-19.99
Rotor speed,	1098.75	56.47	48.96	56.61	26.45	99.78	200.38	200.15 100 61	10.00E	200.35 400.54	<b>49.007</b>	599.98	599.98	799.80	766.92	749.42	749.54	749.54	749.19	750.23	749.42	749.77	750.12	749.65	749.88	40.04/	750.35	750.03	2.00/ 2.00/ 2.00/	749.54	750.23	751.04	750.70	749.42	749.42	748.96	750.46	750.58	750.00	750.35	748.96	750.35	750.00	749.54
Collective pitch, deg	0.0	3.0	3.0 0.0	<b>6</b> .0	<b>9</b> .0	o.	۵. ۱	9 G	9 G	) F	9 6	9.0	J.B	3.0	3.0	J. 0	3.0	<b>9</b> .0	⊕. ⊕.	<b>9</b> :0	0.0 0.0	<b>9</b> .0	<b>9</b> .0	<b>9</b> :	ю. •	۵. ۱. و	<b>0</b> 0	D (	<b>D C</b>	9 6	9 P	3.0	3.0	<b>9</b> .0	9. 9.	<b>9</b> .0	9.0 0.0	9	ю. О.	o. v	<b>0</b> .0	. o	9.n	3.0
Data point number	82258829	83244666	83244001	83244002	83244663	83244006	8324466/	63244668	820447CD	83244011	83244012	83244015	83244016	83244017	83244018	83244019	83244020	83244021	83244022	83255000	83255001	83255002	83255833	83255834	83256000	63236901	83256032	65256655	832308/8 178870F8	83256972	83258000	83258001	83258030	83258031	83258037	83258038	83244023	83244024	83255003	83255004	83256002	83256003	83258002	83258003
Rotor	-	11	11	    		<b>:</b>	=:	I I	::	- L	:-	I	II	II	II	11	11	11	11	11	H	11			=	1;	11:	<b>:</b>	11		11	II	11	11	=======================================	11	II	II	I	II	=	Π	II	=

	Domping. 1/sec	-0.243	<b>-9</b> .244	<b>9</b> .5 <b>4</b>	<b>-6</b> .256	<b>-6</b> .256	<b>-6</b> .258	-6.276	-6.271	-8.29 <del>4</del>	-6.296	907.9	9 6	787.9	107.9	267.9	200.0	187.9 9		97.7	28.5	292	<b>-0</b> .288	<b>-0</b> .286	<b>-0</b> .285	<b>-0</b> .283	<b>-6</b> .280	<b>-6</b> .286	<b>-9</b> .282	207.9	286	<b>-6</b> .294	-6.296	<del>-0</del> .299	<b>-6</b> .284	<b>-6</b> .291	<b>-6</b> .282	<b>6.289</b>	-6.29e	/07. P •	797.0	987.9	36	<b>6</b> .286	
	Frequency. Hz	3.448	•	3.432	3.436	4.051	4.047	5.252	5.254	6.428	6.430	0.430	45.4	6.45e	0.4.0	9.450	•				A.28			6.428		6.420	•	6.443	6.436	9.450	6.436	6.434	6.422	6.428		6.441	6.434	6.422	454.0		6.412	0.420	70.4	6.424	
a	Shaft angle, deg	-19.93	-19.94	-19.98	-19.98	6.63	0.03	0.03	6.63		9.93	20.00	9.6	9.6	9.6	9.6	9.6	8 8	6.6	3 8	9 6	8 6	9.0	96.	6.67	6.67	0.03	0.03	6.67		9.6	-19.92	-19.91	-19.91	-19.94	-19.94	-20.00	-19.99	-19.98	D . C	98.61	00.00 00.00		-19.94 -19.94	
TABLE 7.—CONTINUED	Rotor speed, rpm	750.58	749.19	749.42	749.88	799.78	799.66	899.44	899.56	999.34	999.57	1666.15	26.656	999.46	04.000	1999.83	1666.27	1861.52 860.60	80. BBB	1002.24	97.199	10.000 17.000	1001.55	1000.04	999.81	999.11	1666.27	1000.97	1666.73	1999.73	99.99	889.82	888.88	999.23	1000.50	1000.97	1000.50	999.34	1000.04	989.46	988.76	989.46		989.23	
-	Collective pitch, deg	9,	9.0	a.e	3.0	<b>9.</b> 0	<b>9.</b> 0	o.0	9.0	0.D	<b>6</b> .0	9 ( ? !	۵. ۱۳۱	B. 1	9 (1 7 )	B. 6	9 (°	9.0	9.0	9 G	9.6	9.6	9 6	9.7	3.0	3.0	3.0	J.0	⊕. ⊕.	B. 1	9 <b>G</b>	9 69	9.0	3.0	9. 9.	9. p	<b>0</b> .0	9. 9.	<b>6</b> .0	B. 1	B. (	ا د. ق	D (1	9 <b>6</b>	
	Data point number	83258032	83258033	83258039	83258040	83244025	83244026	83244027	83244028	83244029	83244030	83244031	83244032	83244036	83244037	83245000	83245861	83249000	83240001	83250000	63236661	9000000 81050006	83251000	83251001	83251022	83251023	83251028	83251629	83252000	83252001	83252854	87244073	83244034	83244035	83249002	83249003	83250002	83250003	83250006	83250007	83251002	83251003	4701070	83251839 83251838	
	Rotor	-	::	11	11	11	II	11	. []	II	=	I	II	I	Ι:	Ξ:	1;	= :	=:	<b>:</b>				:=	ï	II	11	11	11	I	II	7 -	:::	II	I	11	11	11	11	I	I	I	<b>⊒</b> ;	==	

	Damping. 1/sec	-6.291	<b>-6</b> .285	-6.288	<b>6</b> .512	<b>4</b> .556	<b>4</b> .579	<b>9</b> .260	<b>98</b> .288	- 288 - <del>P</del>	<b>9</b> .588	<b>4</b> .791	<b>-6</b> .696	<b>-0</b> .678	<b>4</b> .723	<del>-0</del> .723	
	Frequency, Hz	6.430	6.441	6.418	3.450	3.461	3.452	3.471	3.448	3.450	3.454	6.449	6.451	6.457	6.457	6.440	
<b>a</b>	Shaft angle, deg	-19.93	-20.00	-20.00	0.07	6.67	6.67	-19.95	-19.97	-19.96	-19.96	<b>. . . . . . .</b>	<b>6</b> . <b>9</b>	-20.00	-20.00	-20.00	
ABLE 7.—CONCLUDED	Rotor speed, rpm	999.68	1661.32	999.23	750.58	750.70	750.12	751.39	749.65	749.65	750.12	999.46	999.92	999.92	1000.04	998.65	
	Collective pitch, deg	3.0	3.0	0.0 0.0	<b>9</b> .0	<b>.</b>	<b>6</b> .0	6.9	6.0	<b>6</b> .0	6.6	6.9	<b>6</b> .0	6.0	6.0	6.6	
	Data point number	83251031	83252002	83252003	83259022	83259023	83259024	83259021	83259025	83259026	83259027	83259081	83259082	83259083	83259084	83259085	
	Rotor	11	11	==	II	ΙΙ	II	II	II	II	11	Ξ	II	II	Π	11	

TABLE 8.--REGRESSING LEAD-LAG MODE DATA IN FORWARD FLIGHT, CONFIGURATION WITHOUT STRUCTURAL FLAP-LAG COUPLING, 750 RPM

Domping. 1/sec	-0.150	-6.156	9.147	-6. 145	\$ P	9.145	4.9	<b>-0.142</b>			_	-6.138	•	_	<b>-6.133</b>	<b>-6</b> .136	<b>9</b> .7	₽ <del>1</del> .	- P	-6.146	<del> </del>	<b>-6</b> .163	-0.162	<b>-6</b> .173	٣.	Τ.	Ξ.	-6.153	٦.	٠.	<b>₽</b>	47	\$ .	4.7	7	141.9	<b>4</b> .138	-6.138	Τ.	٠.	٠.	<b>-6</b> .166	<b>-0</b> .169	<b>-9</b> .176	<b>6</b> .171	<b>-6</b> . 190
Frequency, Hz	3.431	3.442	3.454	3.429	3.427	3.434	3. <del>+ +</del> +	3.440	3.440	3.446	3.434	3.436	3.44	3.442	3.438	3.452	3.458	3.448	3.461	3.442	3.450	3.456	3.452	3.450	3.458	3.425	3.427	3.434	3.434	3.425	3.438	3.436	5.429	3.431	5.431	3.429	3.436	3.440	3.432	3.436	3.446	3.446	3.440	3.434	3.434	3.446
Shaft angle, deg	-6.67	<b>-6.6</b> 7	-1.99	-1.99 	-4.02	-4.02	-6.03	-6.03	-8.63	-8.03	-10.07	-16.07	-12.04	-12.04	-12.04	-12.05	-14.04	-14.04	-15.96	-15.96	-15.96	-18.02	-18.02	-19.64	-19.64	89. 9	68. <del>9</del>	<b>0</b> 0.00	<b>9</b> 0.00	9.00	-2.00	-2.00	4.64	14.04	-6.eg	<b>-6.0</b> 2	-7.93	-7.92	•	٠	٠	-12.01	-12.01	-12.00	-12.00	-14.00
Advance	0.095	6.693	6.693	0.093	6.093	0.093	0.002	0.032	0.093	6.693	6.693	8.096	6.695	6.697	969.0	960.0	960.0	86.0	650.0	86.0	960.0	6.698	6.095	9.00	6.034	0.149	0.150	6.150	9.159	6.150	9.146	6.148	<b>9</b> .159	0.147	0.149	0.149	0.149	0.146	0.149	6.150	0.149	9.146	0.148	0.150	6.158	0.150
Rotor speed.	749.54	750.46	751.39	749.42	749.19	749.88	750.70	750.35	750.46	750.93	749.88	750.12	750.70	750.58	750.35	751.39	751.74	750.93	751.97	750.46	751.04	751.39	750.93	750.81	750.81	748.96	749.19	750.00	750.00	750.00	750.12	750.00	749.42	749.54	749.65	749.54	750.12	750.35	749.65	750.00	759.46	759.46	750.12	750.00	750.00	750.00
Collective pitch, deg	9.	•	<b>0</b> .0	<b>9</b> . <b>9</b>	<b>.</b>	9.6	<b>0</b> .0	<b>9</b> .0	<b>9</b> . <b>9</b>	<b>9</b> .	<b>9</b> . <b>9</b>	<b>9</b> .0	<b>9</b> . <b>0</b>	<b>9</b> . <b>9</b>	9.9	9	. w	9	9	9 6		6	9.0	9.0	0.0	0.0	<b>0</b> .0	<b>9</b> .0	<b>0</b> .0	0.0	<b>9</b> .0	<b>9</b> .	<b>9.</b>	<b>9</b> .0	ø.	<b>9</b> .	<b>0</b> .0	<b>9</b> .0	<b>0</b> .0	<b>9</b> . <b>9</b>	0.0	9.9	0.0	<b>9</b> .0	<b>9</b> .0	<b>9</b> .
Data point number	83222648	83222049	83222050	83222051	83222052	83222053	83222054	83222055	83222056	83222057	83222058	83222059	83222060	83222061	83222062	83222063	83222064	83222065	A3222066	83222067	83222068	83222069	83222070	83222071	83222072	83222073	83222074	83223002	83223003	83223004	83222075	83222076	83222077	83222078	83222079	83222080	83222081	83222082	83222083	83222084	83222085	83222086	83222087	83223005	83223006	83223007
Rotor	11	=	==	11	==	==	11	=======================================	11	II	II	11	11	=======================================	11	I	I	:=	:=	:=	-	: -	: =	II	H	I	11	11	11	11	II	11	=	II	I	11	11	11	II	II	II	II	II	II	=	11

	Damping, 1/sec	485	-6.194	-:	٦.	٠.	-6.195	•••	-6.198	٠.	Ξ,	٦,	6.148	٠, ١		<b>*</b> • • • • • • • • • • • • • • • • • • •				9 9	9 - 9	- e			-6.192		-6.201	<b>-0</b> .205	-0.201	•	9-13-6-13-6-13-6-13-6-13-6-13-6-13-6-13-	•	9.161	•	•	•	<b>-0.159</b>	•	•	•	ַ,	•	٦,	9	-
	Frequency, Hz	477	3.448	3.435	3.431	3.436	3.440	3.450	3.432	3.432	3.438		5.452	454.0	5.446	5.446	***	5.455	5.451	5.4.5	3.442	0.400 4.430	3.442	3.431	3.452	3.413	3.440	3.44	3.448	3.450	3.41/	3.449	3.436				3.419		3.436		3.454	3.454	404.0	5.448 4.48	) )
	Shaft angle, deg	44 00		-16.00	-16.00	-16.00		-18.00	-20.00	-20.00		0.00	-2.00	-2.60	99.	99.4	•	<b>8</b> .9	•			10.00	•	٠	• •	-14.00	-16.00	•	-18.00	-18.66	60 60 60 60	9 6	-2.04	-3.99	-3.99	-6.03	-6.03	-8.07	-8.67	-8.07	-8.63	-10.03		-10.63	•
B.—CONTINUED	Advance	450	50.00	6.156	0.150	0.150	9.159	6.150	6.150	6.150	9.200	9.266	0.200	0.200	6.200	9.200	9.200	0.200	6.200	9.299	997.9	9.700	90.400	200.0	9.200	0.200	0.200	0.200	9.200	0.200	6.249	9.240	9.248	0.248	0.250	0.251	0.250	0.251	0.250	0.253	0.250	6.251	6.251	6.251	647.0
TABLE 8	Rotor speed, rpm	750 00	750.00	750.00	759.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.60	750.00	750.00	750.00	750.00	759.66	750.66	99.96	759.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	748.61	750 48	750.12	749.07	749.30	748.84	748.38	748.38	749.54	748.61	750.93	751.28	756.93	78.81	131.40
	Collective pitch, deg	6	9	9.0	<b>9</b> .0	0.0	<b>9</b> .0	<b>6</b> .6	<b>0</b> .0	<b>.</b>	<b>9</b> .0	<b>6</b> , <b>6</b>	9. 9	<b>S</b>	9 (	9.0	9	9.0	9.0	9. G	9.0	D 6	9 6	) <b>c</b>	9.0	0.0	0.0	<b>9</b> .	<b>0</b> .0	<b>6</b>	9 6 9	) G	9.0	0.0	9.0	0.0	9.	<b>9</b> .0	0.0	9.	<b>0</b> .0	9.0	9 (	<b>9</b> 6	) )
	Data point number	RESTORAGE	83223009	83223011	83223012	83223013	83223014	83223015	83223016	83223017	83223018	83223019	83223020	83223021	83223022	83223823	85225824	83223025	83223026	83223027	8282228	87957750	83223838	83223932	83223033	83223034	83223035	83223036	83223937	83223038	83223841	83223643	83223044	83223045	83223046	83223047	83223048	83223049	83223050	83223051	83223052	83223053	\$322385 \$35555	83223833	00007700
	Rotor	-	:=		11	=	11	11	11	=	= ;	I			Ξ:	Ξ:	= 1	=:	=:	7;	<b>-</b>	7.	4 h-	:=	II	II	11	11		=:	7.	; <u>-</u>	: ==	=======================================	11	=	II	1	=			= :	⊒:	7.	<b>-</b>

Domping. 1/sec	<b>-6</b> . 199	<b>-6</b> .189		<b>-9</b> .167	<b>-6</b> .169	<b>-6</b> .159	<b>-8</b> .165	-0.156	<b>-9</b> .153	<b>-6</b> . 158	<b>-9</b> .156	<b>6</b> .137	-0.147							•		•	•	•	•	•	•	-6 - 188	┰	┺.	٦.	┺.	٣.	<b>-0.165</b>	٦.	Τ.	╌	٣.	╌	٣.	<b>-6</b> .161	٣.	<b>-6</b> .149	-0.162	-6.151	-0.153
Frequency.	3.454	3.452	3.442	3.438	3.427	3.427	3.436	3.411	3.438	3.440	3.44	3.440	3.419	3.450	3.452	3.438	3.454	3.444	3.427	3.440	3.425	3.442	3.452	3.432	3.442	3.44	3.446	3.442	3.442	3.438	3.438	3.442	3.434	3.436	3.446	3.440	3.434	3.434	3.442	3.442	3.440	3.444	3.446	3.425	3.450	3.452
Shaft angle, deg	-11.96	-14.07	-14.07	-14.04	0.02	6.61	90.0	-2.02	-2.02	-2.02	-2.02	-3.99	90.7	4.02	4.02	<b>8</b> 8.99	-5.99	-5.99	-7.99	-7.99	-7.99	-7.99	-10.03	-10.03	-10.03	0.02	0.02	<b>6</b> .	-1.99	-1.99	96. <del>†</del>	-3.99	-6.93	-6.03		8.80	-8.02	<b>40</b> .89	-6.65	<b>. . . . . . . . . .</b>	-2.02	-2.02	-3.96	-3.99	-3.99	-3.99
Advance ratio	0.252	0.245	0.248	0.247	0.294	9.295	0.296	9.388	0.301	0.296	0.296	9.300	0.297	0.302	0.298	0.299	0.297	0.295	0.233	9.302	0.299	0.299	0.302	0.303	0.298	0.347	0.346	0.349	0.348	0.350	0.351	9.347	0.348	0.348	6.350	9.354	0.351	0.348	0.397	0.395	0.460	0.401	9.499	0.402	0.399	0.399
Rotor speed,	751.16	750.58	749.88	749.30	748.96	749.19	749.77	747.68	750.00	750.00	750.46	750.00	748.38	750.81	750.93	749.65	751.04	750.23	748.49	749.54	748.61	749.88	750.35	749.19	749.77	750.23	750.46	750.58	750.12	749.88	749.77	750.12	749.42	749.65	750.23	749.88	749.19	749.19	750.00	750.00	750.00	750.23	750.23	748.61	750.81	750.93
Collective pitch, deg	9.	9.9	<b>9</b> .0	<b>0</b> .0	<b>0</b> .0	0.0	0.0	0.0	<b>9</b> .0	0.0	0.0	<b>6</b> .6	<b>0</b> .0	9.0	0.0	0.0	9. ¢	9.6	9.0	9.9	9.0	9.	<b>9</b> . <b>0</b>	9.0	9.0	<b>9</b> .0	<b>0</b> .0	<b>9</b> .0	0.0	<b>9</b> .0	0.0	0.0	<b>0</b> .0	<b>9</b> .	<b>9</b> .0	0.0	0.0	0.0	0.0	0.0	<b>9</b> .0	0.0	0.0	0.0	0.0	0.0
Data point number	83223057	83223058	83223059	83223060	83223063	83223064	83223066	83223067	83223068	83223069	83223086	83223070	83223073	83223074	83223075	83223076	83223077	83223078	83223079	83223080	83223081	83223082	83223083	83223084	83223085	83223087	83223088	83223089	83223090	83223091	83223092	83223093	83223094	83223095	83223096	83223097	83223098	83223099	83223100	83223101	83223102	83223103	83223104	83223105	83223106	83223107
Rotor	11	I	=	11	=	11	11	11	11	11	11	II	11	11	11	11	11	II	Ξ	=	Ξ	Ξ	II	Π	11	11	II	11	==	11	11	11	11	11	=	11	11	11	11	Ι			11		H	II

Domping. 1/sec	6 6 6 6 6 6 6 6 6 7 7 7 5 6 7 7 7 5 6 6 6 6	6.157 6.157 6.255 6.255 6.255	22222222222222222222222222222222222222	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
Frequency.	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2		, in	nnnnnnnnnnnnnnnnnnnnn 84444444444444444	2000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Shaft angle, deg	6.00 8.00 8.00 8.00 8.00 8.00 8.00		77779998888888888888888888888888888888	2	8 8 9 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Advance ratio	9.399 9.499 9.447 9.447	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	9 8 8 8 8 8 8 8 8 8 9 9 9 9 9 9 9 9 9 9	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0000000 1
Rotor speed,	751.51 751.51 749.54 756.35	749. 36 749. 19 750. 12 748. 96 748. 96	750.83 750.81 752.69 751.28 748.84 749.54 748.61	750.00 748.30 748.30 748.42 750.23 748.61 750.13 750.12 750.46 750.46 750.46	756.35 756.58 748.96 751.28 749.54 756.81
Collective pitch, deg	0000	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	<b>၁၈၈</b> ၈၈၈၈၈၈	๑๑๑๑๑๑๑๑๑๑๑๑๑๑๑๑๑๑ ๓๓๓๓๓๓๓๓๓๓๓๓๓๓๓๓	
Data point number	83223168 83223169 83223116 83223111 83223111	83223113 83223114 83223114 83235185 83235186	8323618/ 83236108 83236108 83236110 83236111 83236112 83236114	83236117 83236118 83236118 83236120 83236121 83236121 83236124 83236124 83236128 83236128 83236138 83236138 83236138 83236138 83236138	83237005 83237005 83237007 83237008 83237009 83237010
Rotor					.======

Damping, 1/sec	-0.245	-0.238	-0.236	6.233	-0.233	-0.228	-6.230	-0.223	-0.221	-6.217	-6.214	9.7.9	6.233	6.243	9.24	97.9	4.6	252. 8.5.5.	9.50	6.227	-6.230	-0.229	<b>-0</b> .226	<b>-6</b> .218	<b>-0</b> .230	•	•	6.215	197.9	296	217			-0.241	<b>-0.244</b>	-0.229	-0.241	9.240	<b>-6</b> .226	-0.231	-6.227	9.224	9.7
Frequency.	3.423	3.419	3.427	3.432	3.432	3.440	3.421	3.413	3.427	3.429	3.421	•	0.40 F04	•		0.4.0 4.4.4		7.43		3.423	3.429	3,421	3.438	3.419	3.427	3.427	3.419	3.421	2.4	3.442	3.431	3.43	3.436	3.425	3.427	3.423	3.425	3.429	3.436	3.425	454.	5.438	M74.0
Shaft angle, deg	-10.07	-10.07	-12.04	-13.64	-13.93	-15.97	-15.97	-18.01	-18.01	-19.94	-19.95	9.0	9.0-	, ,	99.00	- 10.00 - 10.00	10.00	12.61	10.51	76.51-	79.51-	-13.97	-16.02	-16.91	-16.01	-16.01	-18.00	-18.00	CB. B. I	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	25.01	88	88.98	89.8	<b>89.8</b>	-10.04	-10.04	-10.04	-10.04	-12.01			) D.C.
Advance	9.146	9.146	0.145	6.145	9.145	0.145	0.148	0.148	0.147	0.149	0.145	6.192	∵`	6.197	- •	9 6	. *	. d	900	791.0	101	9.196	6.195	0.198	0.197	0.195	0.196	0.197	9.180	9 6	•	• * :	0.244	0.247	0.248	0.247	0.245	0.246	0.244	0.247	0.249	0.248	ac7 . a
Rotor speed, rpm	749.54	749.67	749.77	750.35	750.23	751.16	749.42	748.84	750.00	750.35	749.65	750.12	749.888	740.19	750.30	750.12	736.40	750.30	7100.12	749.63	750.00	749.30	750.93	749.42	750.00	750.00	749.54	749.65	750.81	740.42	75.97	749.65	750.23	749.30	749.42	749.30	749.42	749.77	750.35	749.54	750.35	750.58	71.90/
Collective pitch, deg	3.6	3.0	<b>9</b> .0	ы н 60 с	) F	0.	3.6	9.8	3.0	3.0	<b>9</b> .0	9.	9 (P	8°.	9 (°	S) (		9 G	9.6	9 6	) M	9 6	3.0	3.0	3.0	3.0	3.0	G.0	9.0	9.6	•	) M			•	•	a.0	3.0	•	3.0	•	9. 9.	<b>9</b> .0
Data point number	83237012	83237013	83237014	83237015	81237917	83237018	83237019	83237020	83237021	83237022	83237023	83237024	83237025	83237026	6323/62/	8323/828	620/675	6323/636	6527631	6323/632 8137941	00010700 AFACTORA	83237035	83237036	83237037	83237038	83237039	83237040	83237041	83237042	8323/843	440/0700	81217846 81217846	83237047	83237048	83237049	83237050	83237051	83237052	83237053	83237054	83237055	83237056	/ca/czcg
Rotor	11	11	I	<b>-</b> -	; :		I	II	II	11	11	1	Ξ:	Ξ:	<b>∷</b> :	<b>-</b>	<b>:</b>	- I	<b>-:</b>	<b>:</b> -	11	:=	:=	II		11		I		<b>-</b>	11	11	:=		=======================================	=	Π	II	I	11		I:	<b>.</b>

Damping, 1/sec	-0.205	-0.220	-0.218	-0.207	-6.213	-6.191	-6.201	-6.185	-0.210	-0.210	-0.206	-9.196	-0.211	-0.198	-0.200	6.235	-0.257	-0.227	-0.240	-0.236	-0.232	-0.238	-0.224	-0.220	-0.206	-0.220	-0.227	-0.197	-9.200	-0.200	961.9	96.90	70.107	9 9	4	9	480	9	9	90.00	40.100	10.04	9.240	240.0	6.62.6	
Frequency.	3.417	3.421	3.427	3.431	3.421	3.429	6.410	3.446	3.425	3.425	3.425	3.419	3.415	3.419	3.423	3.421	3.419	3.432	3.421	3.409	3.419	3.417	3.432	3.425	3.432	3.427	3.421	3.417	3.444	3.434	3.442	3.436	5.438	3.440 4.440	944	244	44.4	1 C 1 C 1 C 1 C 1 C 1 C 1 C 1 C 1 C 1 C	3.432	0.4.0	5.450	3.442	5.458	0.444 444	* C * P	7++-0
Shaft angle, deg	-13.97	-13.97	-13.97	-16.07	-16.07	9	-16.08	-18.02	-18.02	-18.02	-18.02	-19.94	-19.95	-19.94	-19.95	-7.95	-7.96	-7.96	-8.03	-8.03	-10.03	-10.03	-10.03	-12.04	-12.04	-12.04	-12.04	-13.97	-13.96	-13.97	-16.04	-16.04	16.64	15.64	7.90	17.90	17.90	08.71-	+ m. o. c.	08.81-	0.01 0.01	CB. B. I	89.0 89.0	9.60	\$ 6	10.01
Advance	0.251	0.249	0.244	0.247	0.248	0.250	0.243	0.247	0.250	0.249	0.251	0.245	0.245	0.241	0.246	0.296	0.298	0.293	0.295	0.295	0.301	0.304	0.299	0.303	0.300	0.299	0.239	0.303	0.300	0.298	0.301	6.288	0.294	6.299	90.00	9.00	067.0	67.9	6.56	6.29/	0.298	6.29/	0.347	440.0	6.546	ø. 3 <b>4</b> 0
Rotor speed,	749.19	749.54	749.88	750.23	749.54	750.00	748.96	751.16	749.42	749.42	749.65	748.72	748.61	748.84	•	748.84	748.72	749.77	748.84	•	748.84	748.72	750.00	749.42	750.12	749.77	749.19	748.84	750.93	750.12	750.46	749.88	756.93	750.23	750.00	759.00	71.96/	// · P+/	750.93	748.65	749.42	740.00		756.58	750.58	9/ - 90/
Collective pitch, deg	6	3.0	3.0	3.0	3.0 3.0	3.0	a.0	3.0	9.0 9.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	9.0	3.0	3.0	3.0	3.0	3.0	9.0	3.0 0.0	3.0 9.0	3.0	9. 9.	8.0 0.	а. 6	9. 9.	9. °	o	9.6	9.6	9.6	9.0	9 ·	9 (	9. e	9.0	6.0 6.0	9 (	ر د ه. د	D. C
Data point number	83237058	83237059	83237060	83237061	83237062	83237063	83237064	83237065	83237066	83237067	83237068	83237069	83237070	83237071	83237072	83237075	83237076	83237077	83237079	83237080	83237081	83237082	83237083	83237084	83237085	83237086	83237087	83237088	83237089	83237090	83237091	83237092	83237693	83237094	63237693	6323/636	189/570	6527/696	8323/889	8525/100	83237101	8323/162	83237103	8525/164	83237185	92727186
Rotor	Ξ	II	11	=======================================	<b>.</b>	11	=	11	Ξ	11	=======================================	11	=	=	Π	11	11	11	11	Π	II	11	11	11	Π	=	=	11	1	11	I		= ;	<b>:</b> :	7.	<b>:</b> :	<b>-</b> :	7:	<b>≓</b> :	<b>⊒</b> :	Ξ:	= :	Ξ:	=:	=:	1

Domping. 1/sec	-6.227	-6.226 0.226	107	-9.211	-6.165	<b>.</b> 181	-0.178	<b>-0</b> .166	-6.170	-0.155	-6.175	-0.186	-0.170	-6.195	<b>-6</b> .188	-0.421	-0.432	-0.432	-0.429	-0.427	-6.430	-0.422	-0.432	<b>-0</b> .422	-0.424	-0.435	-0.445	6.440	-0.427	-0.429	-0.429	-0.430	-0.435	-0.431	-6.434	-0.436	-0.429	-0.420	-0.420
Frequency,	3.436	5.425	3.436	3.429	3.448	3.452	3.448	3.429	3.452	3.442	3.442	3.448	3.456	3.460	3.461	3.429	3.44	3.429	3.438	3.436	3.44	3.427	3.434	3.438	3.436	3.436	3.440	3.427	3.438	3.450	3.417	3.417	3.429	3.434	3.434	3.432	3.423	3.417	3.419
Shaft angle, deg	10.00	99.91-	-12.64	-12.04	-14.68	-14.08	-14.08	-14.07	-16.04	-16.04	-16.04	-18.01	-18.01	-18.01	-18.01	-11.99	-12.00	-14.00	-14.03	-15.97	-15.97	-17.97	-17.97	-20.00	-20.00	-15.97	-15.97	-18.01	-18.02	-20.00	-20.00	-20.00	-16.01	-16.01	-16.01	-18.05	-18.05	-20.00	-20.00
Advance ratio	0.350	9.348	9.040	0.344	0.351	0.350	0.346	0.351	0.350	0.350	0.350	0.351	6.349	0.349	0.349	960.0	0.002	0.003	0.095	6.093	6.035	0.095	0.093	0.093	0.094	0.145	0.143	0.147	0.148	0.145	0.146	9.148	0.197	Ø. 196	6.197	0.197	0.195	0.198	0.199
Rotor speed,	750.12	749.42	750.38	749.65	750.70	751.16	750.93	749.42	750.81	750.00	750.12	750.23	750.93	751.04	751.39	749.65	750.81	749.65	750.35	750.23	750.81	749.54	749.88	750.58	750.23	750.12	750.46	749.42	750.46	751.39	748.72	748.84	749.65	750.00	750.00	750.23	749.19	748.96	749.67
Collective pitch, deg	9.0	B. 1	9 G	9 6	9.9	9.0	3.0	3.0	3.0	Ø.0	9.0	9.0	Ø.6	9.0	0.D	<b>6</b> .0	9.9 9	6.0	6.0	<b>6</b> .0	6.0	6.0	6.0	6.0	6.0	6.0	6.9	6.0	6.9	6.9	6.0	6.0	6.0	6.0	6.0	<b>6</b> .0	6.0	9.9	8.0
Data point number	83237107	83237108	83237169	83237111	83237112	83237113	83237114	83237115	83237116	83237117	83237118	83237119	83237120	83237121	83237122	83243003	83243004	83243005	83243006	83243007	83243008	83243009	83243010	83243011	83243012	83243013	83243014	83243015	83243016	83243017	83243025	83243026	83243018	83243019	83243020	83243021	83243022	83243023	83243024
Rotor	11	<b>-</b>	: <u>-</u>	:=	: =	11	11	11	=	=	=	II	II	11	==	=	II	=	11	=	==	==	11	II	=	11	11	11	11	11	II	11	II	II	II	11	11	II	11

TABLE 9. -- REGRESSING LEAD-LAG MODE DATA IN FORWARD FLIGHT, CONFIGURATION WITHOUT STRUCTURAL FLAP-LAG COUPLING, 1000 RPM

Damping. 1/sec	 -6.164	<b>-6</b> .163	<b>-6.163</b>	_	9.161	*	•	-	162			٠.	-B. 168	-0.158	-0.157	<b>-6</b> .158	-6.157	<b>.e</b> . 158	<b>-0.155</b>	-0.158	<b>-6</b> .157	-0.157	<b>-9</b> .168	<b>-0</b> .164		-a.169	•	•	•	9	701.0		•	-8, 165		-0.164	<b>-9.168</b>	-6.176	-6.172	<b>-9</b> .186	-6 -184	•	9.199		<b>-0</b> .206
Frequency.	6.428	6.440	6.426	6.422	6.409	6.405	6.436	6.438	6.439	A 432	6.432	6.428	6.422	6.422	6.430	6.430	6.430	6.424	6.411	6.428	6.441	6.434	6.430	6.416	6.422	6.422	6.428	6.412	6.414	6.418	24.0	6.432 8.418	A. 428	6.420	6.438	6.430	6.438	6.443	6.447	6.426	6.428	6.418	6.414	6.432	6.414
Shaft angle, deg	0.02	0.02	-1.97	-1 97	-4.62	76 7-	16.8	46	, d	, e		19.00	-11.97		•	-14.00	-18.04	-16.04	-17.98	-17.98	-19.64	-19.64	9.00	9.00	<b>9</b> .00	<b>6</b> .9	-2.01	-2.01	80.5-1	-3.98	رن دور دور	9 46 6 4	7.00	66. 4-	-10.00	-16.66	-12.04	-12.04	-12.02	-13.96	-13.96	-16.01	-16.00	-17.97	-17.97
Advonce	0.044	0.042	0.043	9 944	9.045	9 944	9.04	977	9.0 8.45	9.6	176	9.044	9.044	9.043	0.043	0.043	0.043	0.043	0.043	0.043	0.043	0.043	0.097	960.0	6.095	0.095	9.00.0	0.097	6.697	6.697	6.697	200	0.00	0 6	656	6.697	6.097	6.097	0.097	6.697	0.097	6.697	6.697	969.6	9.096
Rotor speed, rpm	69.666	1000.62	989.34	FC 606	59.766	997.50	1996	1000	900	44. 000 L	1888 15	- C C C C C C C C C C C C C C C C C C C	40.000	40.000	1000.04	999.92	999.92	94.000	998.41	999.81	1000.85	1999.15	1000.04	999.11	999.57	999.34	999.92	998.65	998.88	999.23	1661.32	77.000	10.000 10.000	45.000	1666.85	1000.27	1666.97	1001.43	1661.55	999.46	999.68	998.88	998.53	1000.04	998.53
Collective pitch, deg	<b>9</b> . <b>9</b>	0.0	9.9	S	6	6		•	9 6	9		9	6	0.0	0.0	9.0	9.0	9.0	9.6	9.0	0.0	0.0	0.0	<b>6</b> .6	<b>0</b> .0	<b>0</b> .0	<b>9</b> .	<b>0</b> .0	<b>9</b>	<b>9</b> (	<b>S</b>	9 6	9 9		6	9.0	0.0	0.0	0.0	9.0	0.0	<b>0</b> .0	<b>0</b> .0	<b>9</b> .0	<b>©</b>
Data point number	83223120	83223121	83223122	83223123	83223124	83223125	83223126	B1221127	8422428	84224129	83223130	83223131	83223132	83223133	83223134	83223135	83223136	83223137	83223138	83223139	83223140	83223141	83224004	83224005	83224006	83224029	83224007	83224008	83224009	83224010	83224011	2124776 81224817	81004814	83224015	83224016	83224017	83224018	83224019	83224020	83224021	83224022	83224023	83224024	83224025	83224026
Rotor		<b>-</b>	11	=	=	:=	-	: =	: -	:=	:=	:=	=======================================	I	I	Π	11		11	=======================================	=======================================	Π	11	11	11		II	1	I	Ι;	::	<b>:</b>	- L	:=	:=	Ξ	II	11	11	II	=	11	-	II	II

Damping. 1/sec		-6.204	6.204	- 19t	<b>9</b> .179	<b>J</b> 175	<b>.</b> 178	4.174	-e. 163	<b>6.179</b>	. 188	-0.176	<b>4.174</b>	<b>-9</b> .169	<b>-9</b> .169	<b>-9</b> .176	<b>J</b> 172	<b>b</b> . 173	<b>-8</b> .165	<b>-9</b> .166	9.176	- <b>6</b> .168	<b>6</b> .172	<b>-6</b> .162	-0.176	<b>-9</b> .160	<b>-9</b> .162	<b>6</b> .177	-0.175	<b>-6</b> .173	-0.170	-9·198	-9·190	- 183 - 183	-8.187	- F. 20/	-0.202	C07.0	- Fe 193	-9.200	<b>6</b> .212	-0.212	<b>-0</b> .207	<b>-0.208</b>	9.212	-0.210	<b>-0</b> .202
Frequency.		6.428	6.420	6.639	6.639	6.639	6.412	6.434	6.434		6.652	6.652	6.639	6.436	6.438	6.639	6.639	6.639	6.424	6.428	6.639	6.639	6.639	6.443	6.438		6.432	6.639	6.639	6.424	6.428	6.639	6.639	6.447	6.426	6.639	6.639	0.450	6.438	6.436	6.639	6.654	6.436	6.432	6.639	6.652	6.453
Shaft angle, deg	;	-19.64	-19.65	90.00	<b>9</b> 0.00	0.00	<b>9</b> . <b>90</b>	9.60	9.62	0.01	-2.00	-2.00	-2.00	-2.02	-2.02	-4.00	<b>7</b> .00	<b>-4</b> .00	4.02	-4.02	99.9	99.9	96.99	-5.99	-5.99	-5.99	99. 99.	<b>-8</b> - <b>8</b>	<b>8</b> 9.	-7.99	-7.99	-10.00	-10.00	-10.03	9	<b>N</b> (	., .		N	N.	•	▼ '	•	-14.00	-16.90	-16.99	-16.02
Advance ratio	1	80.00	6.695	0.149	0.142	0.149	9.148	9.148	9.146	9.152	0.149	9.146	9.148	9.146	9.159	0.148	0.148	0.149	6.150	0.147	9.148	6,148	9.148	_	_	0.148	0.148	0.149	0.147	0.148	0.148	0.149	0.148	9.148	6.148	6.149	9.148	8. L.S	9.140	<b>9.159</b>	0.148	0.147	0.149	6.149	0.147	0.147	0.149
Rotor speed,		999.57	999.11	1000.08	1001.13	999.38	998.30	1666.64	1000.15	55.000	1666.31	1000.08	1000.08	1666.27	1666.39	1666.68	98.86	1666.68	999.34	999.57	96.666	19.666	1666.31	1666.97	1000.39	998.41	999.92	1000.43	999.84	999.46	999.46	999.84	900.00	1001.08	999.23	888	1666.31	1666.15	1666.27	1666.15	1000.78	1000.08	1000.15	999.81	999.26	98.666	1001.68
Collective pitch, deg		<b>.</b>	0.0	<b>9</b> . <b>0</b>	<b>.</b>	0.0	6	6	6		9	6	0.0	0.0	0.0	0.0	0.0	<b>6</b> .60	0.0	6		6	9	9	0.0	0.0	0.0	0.0	0.0	<b>0</b> .0	<b>6</b> .6	<b>6</b> .6	<b>6</b> .0	<b>9</b> .	<b>9</b> .	Ø.	<b>.</b>	9.	<b>9</b> .	<b>.</b>	<b>.</b>	<b>6</b> .	<b>0</b> .0	<b>0</b> .0	<b>0</b> .0	<b>0</b> .0	<b>9</b> .
Data point number		83224027	83224028	82263003	82263005	82263917	83224032	83224033	83224058	83224059	82263004	82263006	82263018	83224034	83224035	82263007	82263008	82263019	83224036	83224037	82263009	82263828	82263021	83224038	83224039	83224040	83224041	82263010	82263022	83224042	83224043	82263011	82263023	83224044	83224045	82263012	82263024	83224045	83224047	83224048	82263013	82263025	83224049	83224050	82263014	82263626	83224051
Rotor			11		-	-	1	1	:=		; <b>-</b>		-	II	Π	<b>-</b>		-	II	=	; <b>-</b> -			11	: =	II	11	~	-	=======================================	11	<b>-</b>	<b>—</b>	=		_	н;	-		II	-	<b>-</b>	II	11	<b>-</b>	<b>-</b>	II

Rotor	Data point	Collective	Rotor speed,	Advance		Frequency,	Domping.
	10001	pitch, deg	ud.	19110	angle, deg	ž	
11	83224052	9.	1000.62	0.148	-16.03	6.440	<b>-0</b> .202
_	82263015	6.6	999.84	6.148		6.639	-0.205
	82263027	<b>6</b> .6	999.84	0.148	-18.00	6.648	-6.216
11	83224053	<b>0</b> .0	999.81	9.148	-18.00	6.432	-0.212
II	83224054	<b>0</b> .0	999.23	0.147	-17.99	6.424	-6.207
11	83224055	<b>9</b> .	998.88	6.148	-17.99	6.429	-0.208
-	82263016	<b>6</b> .	1000.08	9.148	-29.69	6.639	-0.207
<b></b> 4	82263028	<b>9</b> .9	1000.43	0.148	-20.00	6.658	-6.201
	83224056	<b>0</b> .0	1001.20	0.147	-19.64	6.44/	6.268
I.	83224057	<b>9</b> .0	1000.39	0.147	-19.64	5.4.5 5.4.5 5.4.5	987.9
⊶.	82263829	<b>9</b>	1000.55	0.202	9.0	6.60	90.0
<b>-</b> •	82264001	9.	40.000	6.199	9.00	240.0	
<b>-</b> :	82264002	<b>9</b> .0	1661.72	0.200	9.0	40.0	2
11	83224062	<b>9</b>	9000.100	6.189	9.62	0.4.7	- •
I	83224063	9.	999.57	90.199	6.62	6.420	9 - 7 0
II	83224064	9. 9.	999.92	0.197	6.62	6.454	∵`
<b>-</b>	82263030	<b>0</b> .0	1001.25	9.200	-2.66	6.658	2.5
<b>)</b> 0	82264003	<b>9</b> .	1000.55	6.199	-2.66	6.656	9 186
) 	82264004	<b>9</b>	1661.13	6.198	-5.8	6.62	9.19
Ξ:	83224065	<b>9</b> (	808.80	6.201	-2.06	474.0	9 6
<b>⊒•</b>	83224866	s 6	000 t	9.00	98.7-	0.420	• `
<b></b>	02203031	<b>D</b> 6	1909.70	9.50	9 9	9.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00	- P
• ⊷	82264003	• •	90.000	900	9	6.646	-6.178
•=	83224067		1901.43	661.6	-3.95	6.451	· `•
: =	83224068	9	000 000 000	961.0	66.5-	6.422	٠.
; <del>-</del> -	82263032	9	96.666	0.201	-6.90	6.652	-0.178
	82264008	0.0	000	0.200	-6.90	6.643	-0.190
H	82264009	0.0	1000.08	0.199	-6.99	6.646	<b>-6.185</b>
11	83224069	<b>6</b> .0	998.99	9.201	-5.99	6.422	•
11	83224070	<b>6</b> .6	999.92	<b>9</b> .199	-5.99	6.432	<b>-9.182</b>
11	83224071	<b>9</b> .	998.76	0.201	-5.99	6.420	•
I	83224072	<b>9</b> .0	999.57	<b>6</b> . 198	-5.99	6.432	•
<b></b> .	82263933	<b>6</b>	999.02	0.201	8 9	20.00 0.00 0.00 0.00	•
-	82264010	0.0	1000.78	6.199	99.00	6.606	•
<b>-</b>	82264011	9.0	1991.25	9.788 0.000	<b>8</b> 8	0.007 6.648	907.0
٠ ;	82264612	<b>9</b>	96.666	907.9	9.0	6.640	
11	83224073	<b>9</b> 6	L . 688	6.261	20. 	0.420	9
7 .	4/04/70	9.0	1000 .62		7	•	
<b>:</b>	632240/3	<b>D</b> 0	80.888 78.000	70 C	8. /- 8. /-	6.432 6.432	
:-	0705761010		10.000 1000	000		•	•
→ -	02203034		500	707.0	9.00	A. 66	•
<b></b> 1-	02204013	9 6	00.000	n a	9. 4.	A 541	
- :	B1224011	9 6		9 6	•	•	
77	//047700	9.9	00.088	•		4	•

number	pitch, deg	ğ	ratio	angle, deg	ž	1/10
83224079	9	999.11	6.199	-10.03	6.428	-0.196
82263035	0.0	1661.68	0.203	•	6.674	- <b>6</b> . 199
82264015	<b>0</b> .0	1000.20	6.198	-12.00	6.648	-0.213
82264016	9 0	1666.26	6.200	. •	6.648	9.298
62264017	9 (	991.00	D (	•	0.000	997.9
83224686	9 d	47. 800 44. 800		-12.02 -12.02	0.420 A 418	202
1004770	9.6	0000		•		9 2 4
2024776	<b>D</b> 6	/D: 000	97.0	12.02	6.43¢	986
870F3CG	9		9.506	11.02	A 550	10.5
82263636 82264018	9 6	1000.00	207.0	20. 4. 20. 4.	6.652	288
R2264019	) G	1999.78	60.00	-14.00	6.656	961.6-
R2264026	9 6	1000.55	9 1 20	-14.00	6.652	661
81224084	) <b>G</b>	0000	55.6	1 1 90	6.422	
R3224085	) <b>G</b>	70.800	197	4.98		
81224086	) <b>G</b>	1999.27	6 C	14.00	6.440	
B12248B7	•	1.0001	90.0	41-	A 438	88
00477C0	9.6	000	0 . O	1 4	87. W	9 9
82264821	•	9000	207.0	20.02	9	20.0
02204021 02364023	9 9		907.0		A. 650	4 55
7704070		2000	907.0	99.99	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 201
83224888 83224888	9.6	999.46	000	-16.01	6.432	671.9
83224089	9	18.000	6.197		6.436	-6.189
83224090	9.9	999.57	6.199		6.432	-6.199
83224091	0.0	999.92	0.200	-16.01	6.438	┺.
82263938	<b>9</b> .0	1666.31	0.200	•	8.666	٠.
82264924	0.0	1661.84	6.197	-18.00	6.682	٦.
82264025	<b>9</b> . <b>9</b>	1000.08	6.199	-18.00	6.658	٠.
82264026	0.0	1001.13	0.200	-18.66	6.670	<b>6</b> .177
82263939	<b>0</b> .0	999.61	0.202	-20.00	6.662	<b>-0</b> .180
82264027	0.0	999.73	<b>6</b> .200	-20.00	6.658	
82264928	0.0	1000.66	6.189	-20.00	6.672	
82264029	0.0	1000.43	0.197	-20.00	6.668	٦.
82264030	0.0	1666.68	6.251	0.00 0.00	6.650	<b>-6</b> .185
82264031	<b>0</b> .0	999.61	0.250	<b>0</b> 0.00	6.645	٠.
83224094	0.0	999.92	0.250	0.62	6.432	٣.
83224095	0.0	1000.97	0.249	0.02	6.445	<b>-6</b> .181
83224096	0.0	1000.04	0.249	0.02	6.434	<b>6</b> .177
82264032	0.0	98.866	0.250	-2.60	6.650	<b>-6</b> .187
82264033	0.0	999.84	0.251	-2.00	6.646	-0.180
83224097	0.0	1000.97	0.248	-2.06	6.445	-6.177
83224098	0.0	999.23	0.249	-2.06	6.426	9.166
83224099	9.9	1000.97	•	•	6.445	-0.172
82264034	9	1991.92		96.4	6.660	-0.189
82264035		989.28	9.250	4	6 641	•
	);					

Domping. 1/sec	-0.196	-6.188	<b>6</b> .213	<b>-0</b> .208	-6.206	<b>-0</b> .200	-0.202	-0.211	<b>-0</b> .200	<b>-0</b> .195	<b>-9</b> .286	<b>-9.196</b>	<b>-0</b> .199	<b>-6</b> . 199	-0.195	-0.201	<b>.188</b>	<b>-0.194</b>	-0.205	<b>-0</b> . 192	-0.201		-0.189	<b>-0</b> .199	٠.		٠.	-0.190	<b>J</b> 177	-9·186	┺.	-0.195	197	ا ا	-0.188	٦.	-0.181	٠.	٠.	-6.180	-0.177	-0.166	<b>-0</b> .172	- <b>9</b> .189	901	-6.160	
Frequency.	6.428	6.674	6.648	6.648	6.666	6.426	6.418	6.432	6.426	6.652	6.652	6.656	6.652	6.422	6.412	6.440	6.438	6.648	6.650	6.652	6.656	6.432	6.436	6.432	6.438	999.9	6.682	6.658	6.670	6.662	6.658	6.672	5.658	6.650	6.645	6.432	6.445	6.434	6.650	6.646	6.445	6.426	6.445	6.660	6.641	6.434	
Shaft angle, deg	-10.03		-12.00	-12.00	٠	•	-12.02	-12.02	-12.02	-14.00	-14.00	-14.00	-14.00	-14.00	-14.00	-14.00	-14.00	-16.00	-16.00	-16.00	-16.00	-16.01	-16.01	-16.01	-16.01	-18.00	-18.00	-18.00	-18.00	-20.00	-20.00	-20.00	-26.66	0.00	90.00	0.02	0.02	9.02	-2.00	-2.00	-2.06	-2.06	-2.06	96.4	7	-3.99	
Advance	6.199	0.203	<b>6</b> .198	<b>6</b> .266	6.199	0.197	0.201	6.201	0.200	0.202	0.199	6.199	6.198	69.199	0.197	<b>6</b> .198	0.199	0.202	0.200	9.200	6.199	60.199	0.197	9.199	0.200	0.200	6.197	6.199	0.200	0.202	9.200	0.199	6.197	0.251	<b>9</b> .220	0.250	0.249	0.249	0.250	0.251	0.248	0.249	0.249	0.250	950	0.252	
Rotor speed, rpm	999.11	1001.60	1000.20	1000.20	1001.60	999.34	998.53	999.57	999.11	1000.08	1000.43	1000.78	1000.55	88.08	998.07	1000.27	1000.15	999.49	98.86	1000.08	1666.43	999.46	999.81	899.57	999.92	1606.31	1661.84	1999.98	1001.13	999.61	999.73	1666.66	1666.43	1666.68	999.61	999.92	1000.97	1000.04	96.666	999.84	1666.97	999.23	1666.97	1001.02	900	999.92	
Collective pitch, deg	•	<b>9</b> .	<b>•</b> . <b>•</b>	<b>.</b>	<b>9.</b>	9.0	9.0	9.	9.0	6	9,0	0.0	9.0	6	9.0	9.0	0.0	9.	0.0	9.0	0.0	9.0	0.0	0.0	0.0	9.0	<b>9</b> . <b>0</b>	<b>9</b> .0	. <b>0.0</b>	<b>9</b> .0	o. O	<b>0</b> .0	<b>9</b> .	<b>0</b> .0	<b>o</b> .	<b>9</b> . <b>9</b>	<b>9</b> .	<b>9</b> . <b>9</b>	<b>9</b> . <b>9</b>	<b>.</b>	<b>9</b> . <b>9</b>	9.0	9.0	9	•	90.	
Data point number	83224079	82263035	82264015	82264016	82264017	83224080	83224081	83224082	83224083	82263036	82264018	82264019	82264020	83224084	83224085	83224086	83224087	82263037	82264021	82264022	82264023	83224088	83224089	83224090	83224091	82263638	82264024	82264025	82264026	82263039	82264027	82264028	82264029	82264030	82264031	83224094	83224095	83224096	82264032	82264033	83224097	83224098	83224099	82264034	ROOKABIK	83224100	
Rotor	11		-	-		11	Ξ	11	I	-		-		1	II	11	=======================================	_	· <b></b>	-	-	=======================================	II	II	1	-		-	-	1	-	<b>—</b>	-	<b></b>	_	<b>.</b>	I	II	-	-	11	II	Ξ	-	•	·=	

Domping. 1/sec	6.165	7	6.198	<b>-0</b> .192	<b>-9.196</b>	- 183 183	-8.185	-6.182	-6.200	9.180	-6.28/ 0.28/	907.0	797.9	25.6	4	9	9	481	\$ 5 \$ \$	-e. 197	-0.224	<b>-6</b> .231	<b>-0</b> .228	<b>-0.216</b>	-6.182	9	9.18/	2 4	9	9.163	-0.202	-0.176	<b>-6</b> . 181	-6.184	9.195	<b>-0</b> .182	<b>-9</b> .176	-0.18¢	-6-184	<b>-6</b> .175	4	e 166	<b>-6</b> .172
Frequency.	6.428	0.450	6.648	6.648	6.664	6.436	6.424	6.428	6.666	6.6/2	6.436	0.428	6.422	0.00 0.00	6.00 6.00	0.00.00 0.00.00		A A A 2	A 610	6.639	6.639	6.672	6.639	6.639	6.639	6.639	6.432	6.424	0.420 4.48	5.45	6.445	6.441	6.434	6.424	6.432	6.432	6.445	6.639	6.639	6.436	6.434	6.441	6.434
Shaft angle, deg	-4.99	20. F		8.9	<b>8</b> .9	-5.92	-5.92	-5.92	<b>8</b> :	86. 87	<b>8</b> 6	8.0	66.7-		15.00 15.00	- 12.08 - 12.08	11.00	B 4		15.96	-18.00	-18.00	-20.00	-20.00	90.0	<b>.</b>	0.02	9.0	9.0	9 6		96.	-6.61	-6.91	-0.01 -0.01	<b>9.0</b>	\$.9	-2.60	-2.00	-2.62	-2.02	-2.02	-2.02
Advance	6.259	9.251	0.250	0.250	0.250	0.250	0.249	0.251	0.250	0.249	0.251	6.248	0.248	907.9	407.0	6.232 6.252	707.0	<b>6</b> .232	0.434 0.750	9.250	0.252	0.253	0.250	0.250	6.301	9.301	0.297	6.298	200	800.	207.0	0.382	0.298	0.302	9.301	0.298	9.388	9.388	6.301	0.301	0.299	0.299	6.300
Rotor speed, rpm	999.34	999.57	+0.000 17.000	999.73	1666.96	1000.04	989.11	999.34	1000.90	1991.48	1886.64	999.04	998.65	1666.33	400 CO	96.99	40. Bac	28.02 000 000		98.55	1666.26	989.38	1000.66	1000.90	999.73	999.14	999.81	88. 886 60. 606	94.600	1000 KO	1999 73	1000.27	89.68	998.76	999.46	1000.15	1001.20	96.666	1000.20	1999.94	999.81	1000.62	888.82
Collective pitch, deg	•	• •		•	0.0	<b>9</b> . <b>9</b>	0.0	<b>.</b>	⊕.	•	• •	9. 9	<b>.</b>	D. 6	<b>D</b> (	<b>D G</b>		<b>9</b> 6	9.0	9 6	6	0.	9.0	9.0	<b>.</b>	<b>0</b> .0	<b>9</b> .0	9.0	<b>9</b> 6	9 6	) G	9	9.6	<b>9</b> . <b>0</b>	<b>9</b> . <b>9</b>	0.0		<b>9</b> .0	<b>9</b> .	<b>9</b> .	<b>0</b> .	<b>9</b> . <b>9</b>	<b>9</b> .
Data point number	83224101	83224102	82264836	82264037	82264038	83224104	83224105	83224106	82264039	82264040	83224107	83224105	83224109	82264641	82204042	62264643	02204044	62264643	82284843	82264048	82264049	82264050	82264051	82264052	82264053	82264054	83224110	83224111	63224112	81228005	81228006	83228007	83228008	83228009	83228010	83229004	83229005	82264055	82264056	83224114	83224115	83224116	83224117
Rotor	11:			• ~			11		<b></b>	-	=		Ξ,	→ -	<b>-</b> , ,		<b></b>	<b></b>	→ ►	-1 for	• •	-	-	H	-	-	<b>-</b>	Ξ:	<b>:</b>	1.	: -		II	II	11	=======================================	II	-		=			

	Damping. 1/sec	-0.178	<b>6</b> .171	\ \frac{1}{2}		9 - 9	2 2	9	6.179	97.9	<b>-0</b> .204	<b>-6</b> .201	<b>6</b> .185	96.196	-8.198 6.198	6. 188 198	28.4	96. 4	797.9	297	<b>-0</b> .202	-6.197	. 185	<b>.</b> 191	- <b>6</b> .189	-e. 193	\$ 7.5 \$ 6	7 9 9	-0.277	-0.274	<b>-6</b> .293	-6.293 -293	97.9	215	<b>.e</b> . 181	-0.212	<b>-6</b> .194	<b>-6</b> . 195	<b>-6.197</b>	e . e		- 6 - 188
	Frequency, Hz	6.414	6.438	6.456	0.44.0 0.45.0	9.00.0	6.03	677	6.434	6.434	6.639	6.639	6.424	6.428	6.430	6.422	6.448	9.0	6.63% A.40	6.445	6.457	6.451	6.639	6.639	6.639	6.639	9.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00	6.634	6.639	6.639	6.639	6.639	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	6.639	6.639	6.639	6.639	6.424	6.428	6.426	0.4	6.635
	Shaft angle, deg	-2.62	-2.02	-2.62	7.62		Be	7	, <b>5</b> ,	5	<b>8</b> .9	<b>8</b> .9	-5.96 	10.00	-5.96 -1.96	90.01 	96.0		B 8	20.7-	-7.99	-7.99	-10.00	-10.00	-12.00	-12.00		1 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	-16.00	-16.00	-18.00	99.00	99.96	98.0	90.0	9.0	8.	<b>6</b> .9	6.01	9.62	9.67	-2.00
TABLE 9.—CONTINUED	Advance	6.366	0.382	6.299	. 6 . 6 . 6 . 6 . 6	90.00	9.367 9.366	200	0.297	6.297	6.238	6.298	0.298	9.786	6.298	9.700	6.29/	887.0	87.0 404	292.6	0.298	6.386	0.299	0.299	9.300	6.299	900	6. 293 391	6.288	0.297	6.299	6.295	867.0 101.0	9.350	9.348	0.350	0.353	9.346	9.350	<b>9</b> .358	9 . O	<b>6</b> .352
TABLE 9	Rotor speed, rps	997.95	980.34	999.23	8. See .	+0.888	1886.50	000	999.46	989.46	1000.08	1000.20	998.53	888.888	868	4.000	1999.94	1000.00	1200.43	1909.73	1901.43	1666.85	1661.13	1666.43	1001.37	1661.64	888.88	986.30	1666.43	1666.28	1001.13	1867.58		1888.88	1666.43	1661.48	1666.68	988.46	888.68	989.57	0.00	998.32
	Collective pitch, deg	•.	•	• •	•		P. G			•	•.	0.0	•••	•••	•	9.0	9.0			•	• •	•	9.0	<b>.</b>	•	9.0	<b>9</b> . <b>0</b>	D 6	9	0.0	<b>.</b>	<b>9</b> . 6	<b>P</b> •	9.6	6	0.0	<b>6</b> .6	<b>9</b> .0	<b>.</b>	<b>.</b>	Ð (	9 6
	Data point number	83228011	63228012	83228013	53228014	45256	87278403 81228415	81228618	83228017	83228018	82264059	82264060	83228019	83228020	63228021	83228022	83228023	90767060	20040778	81228024 81228024	83228026	83228027	82264063	82264064	82264065	52254966	52264067	82204666 82264666	82264070	82264071	82264072	82264073	\$7040770	82284078	82264077	82264078	82264079	83229006	83229007	83229008	82278668	82264081
	Rotor	=======================================	<b>—</b>	=:	Ξ.	•	<b>- :</b>	:=	1 11	: <b>=</b>	-	-	=======================================	I	<b>I</b>	<b>.</b>	Ξ,	→ -	- E	:	::	II	-	-	-	<b></b> •		→	•	-	<b>—</b>	<b></b>	→	<b>→</b>	• •		-	11	=	I:	<b>:</b>	

	Domping. 1/sec	-6.187	- P. 183	9.1	-8.184 	<b>-6</b> .185	9.130	-6.183	-6.175	-6.184	-9.186	-6.263	797.9	-6.193	-6.19Z	-0.203	9.211	<b>-9</b> . 508	<b>-0</b> .200	<b>-9.225</b>	<b>9</b> .237	- <b>6</b> .219	-6.226	6.525	4.32/	6.5	\$ 5°	6.53 6.13	19.363	-B. 383	<b>-6.435</b>	97.9	464.6	9.436	C81.9-	6.236	717.9	-6.264	95. S	407.00	797.9	97.9	6.223	97.99	9	•
	Frequency.	6.424	6.422	6.434	6.434	6.637	6.639	6.424	6.430	6.422	6.455	6.639	6.658	6.416	6.424	6.428	6.422	6.639	6.639	6.639	6.639	6.658	6.639	9.0°0	0.00 01.00		000.0		689	6.701	6.695	6.711	6.721	6.748	6.640	6.639	6.652	6.420	6.424	6.4 4.4	6.43	6.637	6.643	0.4.0	0.4-7 6.4-28	) d + · · >
	Shaft angle, deg		-1.99	-1.99	-1.99	<b>8</b> 6. <b>†</b>	<b>8</b> .	7.65	<b>7</b>	4.03	7.62	8. 9	99.9	88. r.	-5.98	-5.98	-5.98	<b>98</b> . <b>8</b>	<b>8</b> .	-10.00	-16.98	-10.00	-10.00	-12.00	'n,	99.41	B 4	2 4	90.51	-16.99	-18.99	-18.00	-20.00	-20.00	9.9	<b>9</b> .00	9.00	<b>9</b> .0	9.00	90.0	98.0	-2.66	-2.99		8 6 F 7	•
TABLE 9.—CONTINUED	Advance	0.350	6.351	0.350	6.349	0.351	0.349	0.352	6.349	9.348	0.347	9.348	0.351	6.349	9.351	0.349	9.351	6.351	6.356	6.351	0.352	<b>6</b> .349	9.348	9.349	9.338	6.506	6.04g	- 25. 4 - 25. 4	9.50	9.350	6.356	6.356	0.348	0.348	9.488	9.388	69.	6.397	9.396	6.397	6.398	6.461	0.403	6.461 100	9. <del>4</del> 86	30t-3
TABLE 9	Rotor speed, rpm	999.23	999.23	1000.27	1000.04	998.67	1666.31	999.34	89.68	999.11	1001.90	1000.43	999.84	998.65	89.68	898.68	998.99	1000.43	1000.20	1000.55	1000.08	1000.90	1001.25	1999.98	999.84	24.000 000	1999.66	1000.33	1000.45	1866.98	96.666	1666.26	1000.43	1002.30	1000.20	989.73	1666.55	999.11	999.46	1666.85	1001.55	999.62	999.49	998.65	998.18	999.40
	Collective pitch, deg	9.0	<b>.</b>	•.•	<b>0</b> .0	•.•	<b>0</b> .0	<b>0</b> .0	<b>9</b> .	•.	<b>.</b>	<b>9</b> .	<b>o</b> .	<b>9</b> .	●.	•.•	•.•	<b>9</b> . <b>0</b>	<b>9</b> . <b>9</b>	<b>0</b> .0	<b>0</b> .	•. •	•.	<b>9</b> .0	9.0	<b>.</b> (	9. G	P	. d		0.0	0.0	<b>9</b> .0	<b>.</b>	<b>.</b>	<b>0</b> .0					<b>6</b>			<b>9</b> .0	<b>9</b> . 6	D.
	Data point number	83229010	83229011	83229012	83229013	82264082	82264083	83229014	83229015	83229016	83229017	82264084	82264085	83229018	83229019	83229020	83229021	82264086	82264087	82264088	82264089	82265001	82265902	82265003	82265004	62265000	62265000	10000770	82265000	82265010	82265011	82265012	82265013	82265014	82265015	82265016	82265017	83229022	83229023	83229024	83229025	82265918	82265919	83229826	6322902/	07067700
	Rotor	11	11	=	II	-	-	==	=	=	=	<b>-</b>	<b>-</b>	=	I	1	II		-	-	<b>—</b>		<b></b>	ы.	⊶.	<b></b> •	<b> 1-</b>	<b></b> 1-	<b>-</b>	• •		<b>-</b>	<b>-</b>		-	<b></b> (	<b>-</b>	1	I	ij	I '		<b>-</b>	<b>:</b>	<b>:</b>	7 7

Domping, 1/sec	-0.207	-9.208	-6.198	-6.185	-6.203	-6.183	191	-0.213	-0.214	<b>6</b> .218	<b>9</b> .219	-6.313	<b>9</b> .318	<b>-6</b> .392	<b>-0.374</b>	<b>-6</b> .358	<b>-0</b> .462	<b>19.47</b>	-0.471	<b>-0</b> .237	<b>-0</b> .236	<b>-6</b> .221	<b>-0.243</b>	<del>-0</del> .216	<b>-0</b> .217	<b>9</b> .214	<b>9</b> . 793	<b>-0</b> .227	<b>-0</b> .212	<b>-6</b> . 199	<b>6</b> .201	<b>6</b> .205	<b>6</b> .201	-6.194	-e.195	<b>9</b> . 191	<b>-6</b> .199	<b>9</b> 9.799	<b>9</b> .708	-0.261	<b>-0</b> .272	-0.417	-0.463	-0.426	-6.488	-0.477
Frequency,	6.436	6.679	6.654	6.438	6.456	6.438	6.440	6.643	6.648	6.641	6.645	6.643	6.650	6.682	6.688	6.701	6.688	6.717	6.705	6.658	6.646	6.430	6.430	6.434	6.654	6.650	6.656	6.652	6.432	6.438	6.426	6.666	6.654	6.428	6.438	6.441	6.434	6.658	6.656	6.674	6.656	6.678	6.689	6.699	6.699	6.695
Shaft angle, deg	-1.99	8	8.7	68.5	- J. 188	8.7	3.	<b>8</b> .99	8.9	<b>8</b> .	<b>8</b> .	-10.00	-10.00	-12.00	-12.00	-14.00	-14.00	-14.00	-16.00	9.60	98.0	0.01	90.0	99.9	-2.00	-2.00	-2.00	-2.00	-1.97	-1.97	-1.98	<b>8</b> . +	8.7	4.04	7.7	<b>5</b> . <b>7</b>	<b>*</b> 0. <b>†</b>	<b>98</b> .9	<b>98</b> .9	<b>8</b> .89	<b>8</b> .89	-10.00	-10.00	-12.00	-12.00	-14.00
Advance	●.398	6.388	9.	0.462	6.461	6.401	9.386	0.401	<b>6</b> .486	0.402	<b>9</b> .401	0.402	0.403	<b>9</b> .492	0.402	<b>6</b> .401	6.388	9.499	9.396	9.459	0.451	0.449	<b>9.448</b>	0.447	6.456	9.448	<b>6.45</b> 6	0.451	<b>6</b> .448	0.451	0.449	0.452	9.458	0.451	9.453	9.448	<b>6.</b> 448	<b>9.</b> 459	<b>9</b> .448	0.453	0.451	9.47	0.449	6.459	6.459	0.451
Rotor speed.	1999.64	1991.72	1000.43	1999.15	1000.04	1666.15	1000.27	989.38	1000.08	999.02	989.38	998.55	998.91	1000.66	1666.96	1000.31	999.26	1001.37	999.73	1999.43	999.49	999.57	999.68	999.69	1000.08	999.61	1000.08	999.73	89.666	1000.04	998.99	1000.68	999.61	989.57	989.57	1000.39	999.92	1000.55	1666.26	1666.78	999.49	1000.08	1000.55	1999.43	1000.43	998.44
Collective pitch, deg	•	• •	•. •	<b>.</b>	0.0	•	•. •	•.•	•. •	0.0	0.0	•. •	<b>9</b> . <b>•</b>	•.•	••	9.0	•.•	0.0	9.	0.0	0.0	9.0	0.0	0.0	⊕.	<b>•</b> . <b>•</b>	0.0	9.0	●.	<b>9</b> .	<b>⊕</b> .	<b>.</b>	<b>6</b> .0	<b>9</b> .	©.	<b>.</b> .	●.	9.0	<b>•</b> .•	<b>9</b> . <b>0</b>	0.0	9.0	9	9 9	9	•
Data point number	83229029	82265929	82265021	83229030	63229031	83229032	83229033	82265022	82265023	82265924	82265025	82265926	82265027	82265028	82265929	82265930	82265031	82265932	82265934	82265035	82265036	83229035	83229036	83229037	82265037	82265938	82265939	82265040	83229038	83229039	83229040	82265041	82265042	83229042	83229043	83229044	83229045	82265943	82265944	82265045	82265046	82265647	82265648	82265049	82265050	82265051
Rotor	II	<b>-</b>	-	=	11	11	=	-	<b>-</b>	<b>~</b>	-	-	-	-	-		-	-	-	-	-	II	II	II	-	-	-	-	II	11	II	-	~		I	11	II	-	-	<b>—</b>	H	-				•

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	<b>6</b> .148
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	9.148
	9.147
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Damping. 1/sec	-0.293	-8.294	<b>-6</b> .286	-0.284	<b>-0</b> .285	-0.284	-0.282	<b>-6.283</b>	-6.271	-0.278	-0.274	<b>-0</b> .269	-6.289	<b>-6</b> .293	-6.28/	-6.285	-6.286 -	-6.281	<b>-0.274</b>	-0.274	-9.267	- <b>9</b> .261	-0.253	<b>-9</b> .255	-0.239	<b>-0.231</b>	<b>-0</b> .297	-0.293	-9.287	-0.282	697.9	67.0	9.530	907.9	4. 3.4. 3.4.	9.53 9.93	777.0	6.223	-6.213	-6.225	<b>-0</b> .225	<b>-6</b> .277	<b>-6.271</b>	-0.236	٠	-6.254
Frequency, Hz	6.430	6.436	6.441	6.420	6.422	6.426	6.434	6.432	6.432	6.424	6.434	6.426	6.426	6.432	6.428	414	6.420	6.434	6.438	6.443	6.432	6.428	6.432	6.426	6.424	6.409	6.420	6.436	6.428	6.422	6.424	6.424	0.422	0.424 6.418	0 7 7	6.436	0.71.0	6.426	6.452	6.428	6.428	6.420	6.426	6.426	6.420	6.414
Shaft angle, deg	-16.88	-10.00	-12.01	-11.97	-14.80	-14.00	-16.04	-16.04	-17.97	-17.97	-19.96	-19.97	-8.67	-8.67	-16.63	-10.03	-12.00	-12.88	-13.93	-13.93	-15.97	-15.97	-17.98	-17.98	-19.94	-19.94	-8.0 <del>4</del>	-8.9 <del>4</del>	-10.01	-10.60	-12.65	-12.04	40.01	45.05	10:11	+0.+I	70.01	-15.97	CO. 20.	-18.65	-18.04	96.6-	96.6-	-12.05	-12.05	-12.07
Advance ratio	0.147	9.147	0.147	0.148	9.146	9.146	0.149	0.147	9.146	0.147	0.148	0.149	6.197	0.198	0.198	<b>9</b> .199	0.202	0.195	0.198	0.199	6.197	0.197	0.198	0.199	9.194	0.195	0.244	0.249	9.248	0.248	0.250	0.250	9.226	6.236	0.740	6.246	0.24/	0.248	0.248	0.249	0.249	9.301	9.301	9.236	0.297	0.299
Rotor speed.	1000.04	1999.59	1001.32	989.34	999.69	1000.04	1000.85	1000.62	1000.73	1000.04	1001.08	1999.27	999.46	999.92	80.66	998.65	999.23	1000.39	1666.85	1001.32	1666.56	1000.27	1000.62	999.92	898.68	998.30	998.88	1999.94	898.68	999.23	999.57	999.57	888	888.68	+0.888	1000	04.000	999.46	999.00	999.57	999.81	998.88	999.57	999.46	999.46	998.88
Collective pitch, deg	6	9.0	9.	9.0	3.0	3.0	3.0	3.0	9.N	3.0	3.0	3.0	9.B	3.0	ø.n	ø.n	3.0	3. <b>0</b>	3.0	Ø.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	J. 0	<b>9.0</b>	ю. Ф.	<b>6</b>	<b>9</b> .01	9.0	9.0	9. e	D. (	B. 0	ы. В.	a. b	0.0 0.0	3.0	3.0	0.D	a.0	3.0
Data point number	83236030	83236031	83236032	83236033	83236034	83236035	83236036	83236037	83236038	83236039	83236040	83236041	83236043	83236044	83236045	83236046	83236047	83236048	83236049	83236050	83236051	83236052	83236053	83236054	83236055	83236056	83236057	83236058	83236059	83236060	83236061	83236062	83236863	83236864	63236663	63230006	1999570	83236068	83236069	83236070	83236071	83236074	83236075	83236076	83236077	83236078
Rotor	11		Ξ	=	==	==	11	=	11	<b>!</b>	II	I	II	-	<b>.</b>	1	II	I	11	=	1	11	II	11	II	11	II	II	1	II	I	I:	<b>⊒</b> :	<b>-</b>	<b>:</b>	<b>→</b> .	- :	1	I	<b>:</b>	1	==	=======================================	1	=======================================	11

Damping.	- <b>6</b> .254 - <b>6</b> .212	6.213	9.58	-0.205	<b>-9.204</b>	-6.202	<b>6.210</b>	-6.213	112.6	-9.261 9.261	2.7.9 6.7.9	907.0	200	22.4	-9.205	<b>6</b> .197	-0.201	-6.167	<b>-6.178</b>	-0.202	<b>6</b> .178	-9.597	40.00	9.03 9.03 9.03	9.00e	70.0	25.4	567	-6.581	-6.595	<b>-0.592</b>	9.546	- 569 - 569	<b>-6</b> .559	<b>-0</b> .562	-6.5 <del>48</del>	<b>6.544</b>	<b>9</b> .269	•	-6.583	<b>-0</b> .597	<b>9</b> .576
Frequency. Hz	6.428	6.428	6.420	6.418	6.438	6.449	6.428	6.418	6.432	6.416	0.432	0.410 0.410	)		6.430	6.428	6.440	6.440	6.430	6.426	6.447	6.436	6.434	6.440	6.432	0.44	6.432 8.433	6.434	6.436	6.432	6.428	6.428	6.443	6.430	6.440	6.440	6.430	6.438	6.432	6.429	6.440	6.438
Shaft angle, deg	-12.67	-14.04	2 C C C C C C C C C C C C C C C C C C C	15.99	-16.00	-17.97	-17.97	-17.97	- (	-10.03	-16.63	18.21-	12.50	-12.80	-14.01	4	-14.00	-15.97	-15.97	-15.97	-15.97	-2.03	-2.63	-2.62	20 C	88.7°	2 4 3 4		-8.67	-8.67	-10.00	-10.00	-10.00	-12.04	તં	÷	*	-16.04	8	-17.97	-17.97	-19.93
Advance ratio	<b>6</b> .298 <b>6</b> .362	0.299	767.0	0.299	0.299	0.301	6.386	9.388 9.000	67.0	6.545	7.5	9.04g	340	6.350	9.351	9.359	9.348	9.348	0.348	0.347	0.347	0.042	<b>6</b> .844	6.649 6.45	4.0	6.045		0.046	9.046	0.042	0.044	9.046	0.047	0.041	0.041	0.045	9.046	9.945	0.045	6.044	6.642	0.044
Rotor speed, rpm	999.69 999.81	999.57	0.000	998.76	1000.15	1661.43	888.68	998.76	1666.64	80.00 80.00	78. 888 000	0/.000 000	1999.03	25.060	25.008	89.68	1000.27	1666.39	999.46	999.57	1666.97	999.48	999.23	000 F3	70.988	78.888	P0.000	11.000	900.34	998.99	998.88	998.65	999.92	86.868	1000.27	1000.04	999.23	1000.04	999.23	998.30	999.81	889.81
Collective pitch, deg	9.9 9.9	9.6	9 6	9 <b>9</b>	3.0	<b>9</b> .0	<b>9</b> .9	B (	۹. ۱۵.	<b>9</b> .6		B 6	9 6	9 69	. E.	9.0	3.0	0.E	3.0	3.0	<b>6</b> .0	<b>.</b>	œ.	<b>9</b> .0	9.0	D 4		9 6	9	6.6	6.6	6.6	<b>9</b> .	<b>6</b> .0	6.6	<b>6</b> .0	<b>9</b> .0	<b>6</b> .0	<b>9</b> .9	<b>.</b>	<b>.</b>	<b>5</b> .
Data point number	83236079	83236081	83236883	83236084	83236085	83236086	83236087	83236888	53236889	83236898	63236691	28992269	81016894	83236095	83236096	83236097	83236098	83236099	83236100	83236101	83236102	83242024	83242825	83242826	6224262/	62642626	81042010	83242031	83242032	83242033	83242034	83242035	83242036	83242037	83242038	83242039	83242040	83242041	83242042	83242643	83242044	83242845
Rotor	H H	1:		II	11	11	1	I:	= :	<b>:</b>	<b>∃</b> :	<b>-</b> -	- h-	: -		=	Ξ	H	II	11	=	I:	=:	=:		- F		:=	: !	I	=======================================	11	11	=	=	11	11	=	11	I	11	11

Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Advance ratio	Shaft angle, deg	Frequency.	Damping 1/sec
II	83242046	9.	989.46	9.947	-19.93	6.432	-0.592
II	83242047	9.9	999.57	0.043	-19.93	6.438	-0.578
Ξ	83242048	9.0	989.34	0.042	-19.93	6.430	<b>-9.566</b>
II	83242049	9.9	1888.84	0.097	-15.98	6.441	<b>-9.561</b>
11	83242050	0.0	1000.15	6.697	-15.98	6.443	<b>-6</b> .558
=======================================	83242051	6.6	1000.04	960.0	-18.02	6.440	-0.548
Ι	83242052	Ø.	1000.15	6.697	-18.02	6.441	<b>-9</b> .552
11	83242053	<b>9</b> .	1000.15	969.0	-19.97	6.443	-6.547
II	83242054	9.9	999.11	6.098	-19.96	6.430	-6.577
II	83242055	9.9	999.81	969.6	-19.97	6.438	<b>-0</b> .555
11	83242056	9.9	999.92	860.0	-19.97	6.441	<b>-9.566</b>
11	83242057	0.9	1969.85	9.148	-18.00	6.451	-6.573
11	83242058	0.0	1000.04	9.148	-18.00	6.440	-6.543
II	83242059	<b>0.</b> 0	1000.27	0.147	-17.99	6.447	<b>-6</b> .558
11	83242060	6.9	1000.50	9.149	-19.95	6.440	<b>-6</b> .558
11	83242061	0.9	998.53	0.149	-19.98	6.418	-0.569

TABLE 10. -- REGRESSING LEAD-LAG MODE DATA IN FORWARD FLIGHT, CONFIGURATION WITH STRUCTURAL FLAP-LAG COUPLING, 750 RPM

Domping. 1/sec	-6.150	<b>-6</b> .150	9.14	<b>-6.145</b>	<del>*</del> - <del>*</del> •	9.145	47.9	<b>-9.142</b>	<b>9.139</b>	<b>-6.138</b>	<b>6.137</b>	-6.138	-6.138	<b>6.137</b>	<b>Ja.</b> 133	┺.	Τ.	٣.	9. - 48	<b>-9.146</b>	↽	-	Ξ.	~.	┯.	-	- 150 - 150	-6.153	_		<b>P</b> :	9 9		<b>†</b>	9	9	3 5	97	146		9	9 9		- •	9	301.0
Frequency.	3.431	3.442	3.454	3.429	3.427	3.434	J. ++	3.440	3.440	3.446	454.0	3.436	3.444	3.442	3.438	3.452	3.458	3.448	3.461	3.442	3.450	3.456	3.452	3.450	3.450	3.425	3.427	3.434	3.434	3.425	0.400	5.456 4.456	0.459	24.5 44.4	4 430	27.C	446	3,430	436	7.446	7 448		0.440	+ P + P + P + P + P + P + P + P + P + P	0.434 444	.,
Shaft angle, deg	6.67	<b>-0.0</b> 7	-1.99	-1.99	-4.02	-4.02	-6.63	6.63	-6.63	-8.63	-10.07	-10.07	-12.04	-12.04	-12.04	-12.05	-14.04	-14.04	-15.96	-15.96	-15.96	-18.02	-18.02	-19.64	-19.64	8. 9	6.69 6-1	9.00	9 . 99 9 . 9	<b>6</b>	-2.66	-2.66	***	<b>5</b> 4	- 6	70.07	00.7-	-19.90	-10.00	15.55	10.00	20.07	-12.61	20.51	- 15.08 - 15.08	20.1
Advance ratio	6.695	6.693	6.693	0.093	0.093	6.693	6.632	6.632	0.093	6.693	0.093	9.096	0.095	6.697	969.0	960.0	969.0	860.0	660.0	860.0	950.0	869.0	6.695	9.686	9.634	0.149	<b>9.159</b>	6.150	6.156	6.156	6.146	5 1 4 5			9 4	9 . 43 140	9 146	64.	47.0	. e	0 . A	0 1 1		9.50	0	
Rotor speed,	749.54	750.46	751.39	749.42	749.19	749.88	750.70	750.35	750.46	750.93	749.88	759.12	750.70	750.58	750.35	751.39	751.74	750.93	751.97	750.46	751.04	751.39	750.93	750.81	750.81	748.96	749.19	750.00	750.00	750.00	750.02	740.45	71.61/	749.04	749.54	750.12	750.15	749.65	750 00	750.46	750.48	756.40	21.96/	99.96	75.00	9.95
Collective pitch, deg	6	0.0	<b>9</b> . <b>9</b>	<b>.</b>	<b>9</b> . <b>9</b>	<b>9</b> . <b>9</b>	<b>9</b> .0	<b>0</b> .0	<b>9</b> .	<b>9</b> .	• •	<b>.</b>	•	<b>o</b> .	<b>.</b>	<b>.</b>	<b>9</b> . <b>0</b>	0.0	<b>9</b> .0	<b>9</b> .0	<b>0</b> .0	<b>6</b> .0	<b>0</b> .0	<b>9</b> .	<b>.</b>	<b>.</b>	<b>6</b> .	<b>0</b> .0	<b>6</b> .	<b>6</b> .6	9.0	D 6	Þ. (	Đ <b>G</b>		P	9 4	. c	9 6	9 6	9 6	9.0	9.6	9.0	<b>P</b> 6	<b>P</b> .
Data point number	83222048	83222049	83222050	83222051	83222052	83222053	83222054	83222055	83222056	83222057	83222058	83222059	83222060	83222061	83222062	83222063	83222064	83222065	83222066	83222067	83222068	83222069	83222670	83222671	83222072	83222073	83222074	83223002	83223003	83223004	852220/5	832220/6	1/07770	8/87770	8/077700	0322200 03222000	62242601 64333963	81222881	81222084	222220 22222085	0227700 0422230	62277666	83222887	65223663	6222366	10007700
Rotor		H	11	11	11	==	11	==	=======================================	11	11	11	1	11	==	=	11	11	Ξ	=	==	=	11	=======================================	11	=	=	11	=	H	<b>:</b> :	<b>::</b>	Ξ:	<b>-</b> -	::			::		: <u>-</u>	::			<b>-</b>	<b>]</b> :	1

Damping. 1/sec	-0.184	-0.19¢	-0.201	-9.196	- 198 - 198	<b>-6</b> . 195	-0.202	-6.198	_	-0.159	<b>-0</b> .160	. <del>1</del> 8	<b>6</b> .154	9.148	4.9	<b>9</b> .149	9.14	-0.160	•	-0.182	<b>-6</b> .191	-0.188	<b>-0</b> .193	<b>-0</b> .198		<b>-6</b> .189	<b>-6</b> .201	<b>-0</b> .205	-0.201	<b>-9</b> .204	•	•	<b>-6.155</b>	<b>-0</b> . 161	-0.151	<b>6</b> . 151	. 161 161	<b>-6</b> .159	-0.181	<b>69.169</b>	-0.184	<b>-6</b> .179	-0.196	487	108	) q	9
Frequency,	3.448	3.448	3.435	3.431	3.436	3.440	3.450	3.432	3.432	3.438	3.438	3.432	3.434	3.440	3.440	3.44	3.433	3.431	3.436	3.442	3.438	3.438	3.442	3.431	3.452	3.413	3.440	3.444	3.448	3.450	3.417	3.452	3.440	3.436	3.427	3.427	3.423	3.419	3.419	3.436	3.423	3,454	424	3.454	477	7.440 4.60	3.446
Shaft angle, deg	-14.00	-14.00	-16.00	-16.00	-16.99	-18.00	-18.00	-20.00	-20.00	0.00	9.00	-2.00	-2.00	8.7	8.7	99.99	99.99	80.89	8.89	-16.00	-10.00	•	-12.00	-12.00	-14.00	-14.00	-16.00	-16.00	-18.00	-18.00	<b>9</b> .00	-6.61	-2.04	-2.04	-3.99	-3.99	6.03	-6.93	-8.07	-8.07	-8.07	-8.63	-10.03	1.0 01.	00.0	-10.03	•
Advance ratio	0.150	0.150	6.156	0.150	9.159	6.158	9.159	9.159	6.158	9.200	6.200	9.500	9.200	6.200	9.200	9.200	6.200	0.200	9.200	6.200	9.200	9.200	0.200	0.200	0.200	0.200	0.200	0.200	0.200	0.200	0.249	0.248	0.245	0.248	0.248	0.250	0.251	0.250	0.251	0.250	0.253	0.250	9 251	25.0	136.4	6.20	0.24B
Rotor speed,	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	750.00	759.00	750.00	759.00	750.00	750.00	750.00	750.00	748.61	751.16	750.46	750.12	749.07	749.30	748.84	748.38	748.38	749.54	748.61	750.93	751 28	750.01	780.007		751.28
Collective pitch, deg	0.	0.0	<b>9</b> .0	<b>0</b> .0	<b>0</b> .0	0.0	0.0	9.6	9.	9	9	9	9	9	6	6	9	9	6	9.0	9.0	9.0	9.0	0.6	0	0.6	<b>9.</b>	0.0	0.0	9.0	<b>9</b> . <b>9</b>	0.0	9.0	<b>9</b> .0	<b>9</b> .	9.0	0.0	0.0	0.0	6	0.0	0		9	) d	D	D.
Data point number	83223008	83223009	83223011	83223012	83223013	83223014	83223015	83223016	83223017	83223018	83223019	83223020	83223021	83223022	83223023	83223024	83223025	83223026	83223027	83223028	83223029	83223030	83223031	83223032	83223033	83223034	83223035	83223036	83223037	83223038	83223841	83223042	83223043	83223044	83223045	83223046	83223047	83223048	83223049	83223050	83223051	83223052	A3223053	8122184	0.22230 0.22230 0.22230 0.22230	63223933	00007700
Rotor	=======================================	11	II	=	=	===	11	=======================================	I	Ι	II	11	II	I	11	II	Π		11		II	II	II	11	II	11	11	11	11	II	II	II	<b>!</b>	11	=	Ξ	11	II		11	II	11		: -	<b>-</b> -	<b>7</b>	1

Damping. 1/sec	-6.199	<b>. 189</b>	-0.178	_	_	-	<b>.</b> 165	<b>9.156</b>	_	-	<b>a</b> . 156	_	9.147	_	_	_	<b>69.169</b>	_	_	<b>-0</b> .166	-6.173	<b>-6</b> .186	_	-	_	~	₹.	Τ.	<b>-9</b> .159	٦,	- 1	201. <b>9</b>	- '	9	- •		٦,	~ •	٦,	9/1.9	Ξ,	_			<b>4</b> .151	-6.153	
Frequency,	3.454	3.452	3.442	3.438	3.427	3.427	3.436	3.411	3.438	3.440	3.44	3.440	3.419	3.450	3.452	3.438	3.454	4.44	3.427	3.440	3.425	3.442	3.452	3.432	3.442	M. 444	3.446	3.442	3.442	5.438	5.4.58	2.442	†?†.?	5.4.5 4.4.4	7.4	24.0	# ? ! ? !	454.0	5.442	5.442	2.44e	77.7	3.446	3.425	3.450	3.452	
Shaft angle, deg	-11.96	-14.07	-14.07	-14.04	0.02	6.91	<b>8</b> .9	-2.02	-2.02	-2.02	-2.62	-3.99	<b>8</b> . <b>†</b>	4.62	4.62	<b>8</b> .9	-5.99	-5.99	-7.99	-7.99	-7.99	-7.99	-10.03	-10.03	-10.03	0.02	9.62	<b>6</b> .9	-1.99 -1.99	88. L-	<b>8</b> 3	7 4	2 i	3.5	9.0	<b>3</b> 6	79.9-	\$ .	6. e	6.6	-2.62	-2.02	80.51 10.08	-3.99	-3.89	-3.99	
Advance ratio	0.252	0.245	0.248	0.247	0.294	9.295	0.296	9.388	9.301	0.296	0.296	<b>9</b> .399	0.297	9.302	<b>9</b> .298	0.289	6.297	0.295	6.238	6.302	6.288	0.299	0.302	0.303	0.298	6.347	9.346	<b>6</b> .349	6.348	6.336	6.351	747.0	9.5	6.040	9.50	400.00	6.531	6.040 101	/RC.D	6.395	9.400	9.401	. <del>1</del> 60	9.402	9.399	6.388	
Rotor speed.	751.16	750.58	749.88	749.30	748.96	749.19	749.77	747.68	750.00	750.00	750.46	750.00	748.38	750.81	750.93	749.65	751.04	750.23	748.49	749.54	748.61	749.88	750.35	749.19	749.77	750.23	750.46	750.58	750.12	749.88	749.77	750.12	747.47	749.65	7.96.7	749.88	B	749.19	120.00	750.00	750.00	750.23	750.23	748.61	750.81	750.93	
Collective pitch, deg	•.	<b>•</b> .	<b>0</b> .0	•.•	<b>9</b> . <b>9</b>	<b>•</b> .•	<b>9</b> .	<b>•</b> .•	9.0	•.	<b>.</b>	•.•	•.•	<b>.</b> .	9.0	•.•	0.0	9	9.0	0.0	9.0	<b>9</b> .6	9.6	<b>9</b> .	<b>0</b> .0	•.•	<b>0</b> .0	<b>.</b>	0.0	<b>0</b> .0	<b>.</b>	9.6	<b>9</b> (	<b>9</b> .6	Ð. (	9.0	<b>9</b> .	<b>9</b> .0	D :	<b>9</b> .	9.0	<b>9</b> .	<b>.</b>	<b>•</b> .	<b>0</b> .0	<b>.</b>	
Data point number	83223857	83223058	83223059	83223060	83223063	83223064	83223066	83223067	83223068	83223069	83223086	83223070	83223073	83223074	83223075	83223076	83223977	83223078	83223079	83223080	83223081	83223082	83223083	83223084	83223085	83223087	83223088	83223089	83223090	83223091	83223092	63223093	83223684	83223095	63223686	83223097	82223698	83223099	83223100	83223101	83223102	83223103	83223104	83223105	83223106	83223107	
Rotor tested	==	<b>:</b>	11	I	11	II	11	II	11	11	11	11	11	II	Π	II	Ξ				Ξ	11	11	11	11	11	11	11	11	11	I	Ξ:		Ξ:	<b>⊒</b> :	I:	-		11	=	11	=	11	=	=======================================	11	

Damping. 1/sec		<b>-6</b> .162	8/1.9		27.9	9 4	- •	9 9 9	9.5	25.4	262	-A 254	-0.245	-0.257	-9.261	-0.263	-0.253	<del>-0</del> .252	-0.255	<b>-6</b> .257	-0.256	9.254	<b>-9</b> .255	9.256	<b>-8</b> .251	6.249	6.249	9.7	4.64	243	-0.245	-0.241	<b>-0</b> .243	-0.245	<b>-0</b> .257	<b>-0.258</b>	•	-0.256	40.23	807.9 P	75.252	162.9	24.5	R\$7.9
Frequency,	3.460	3.460	3.436	J. 448	7.7	2.45		3.442		777	3.436	4.50	3.436	3,458	3.450	3.436	3.444	3.434	3.440	3.431	3.431	3.440	3.434	3.434	3.440	3.442	5.448	5.458 8.48	0.4.5 4.4.6	5. <del>1.</del> 6.	3.423	3.429	3.44	3.434	3.454	3.454	3.446	3.444	5.448	5.458	2.448	5.452	3.456	***·
Shaft angle, deg	-6.63	6.03	89.9			55. F	70 CP	7	, P 9	9.6	2.6		-3.99 -3.99		-3.98	13.00 10.00	98.9	98.9	-7.99	-7.99	-10.00	-16.66	•	-11.96	-13.99	-13.99	-15.93	-15.93	10.01	10.64	-18.94	-19.96	-19.96	-19.96	-3.96	-3.96	-6.0 <del>4</del>	-6.9 <del>4</del>	-8.07	6.67	-10.64	-10.07	-12.62	12.61-
Advance ratio	6.399	9.466	0.447	6.447	<b>6</b> .43	6.45	6.40e	9. 44.0 0. 44.0	9.6	4.09.0	0.03.0	900	400.0	90.0	969.6	69.695	6.695	0.095	6.095	0.095	960.0	0.097	9.692	6.694	9.034	9.00	0.002	6.695 905	0.00.0	6.69.0	500	6.695	6.695	0.034	0.149	0.151	9.150	0.150	<b>6.156</b>	9.150	0.150	9.149	6.149	<b>9</b> .152
Rotor speed,	751.51	•	749.54	750.35	30 - 34/	749.30	D . 04/	71.00.12	7.04/	71.96/	749.65	750.50	749.54	751.16	750.58	749.54	759.12	749.42	750.00	749.19	749.19	750.00	749.42	749.42	750.00	750.12	750.58	749.77	748.00	750.46	748.72	749.19	750.35	749.65	750.35	750.35	749.88	749.65	750.12	749.30	750.12	756.35	•	749.88
Collective pitch, deg	•.	•.	<b>9</b> .	<b>.</b>	<b>D</b> (	9.0	9 G	9. C	Ð 6	P	9.6	•	9 6			3.0	9.7	9.1	3.0	3.0	3.0	3.0	3.0	3.0	<b>9</b> .0	<b>0</b> .0	<b>9</b>	o. •	<b>9</b> (1	9 <b>•</b>	9 6	3.0	3.0	3.0	3.0	3. <b>0</b>	a.e	3.0	<b>6</b>	<b>9</b> .	<b>6</b> .0	<b>9</b> .0	<b>6</b> .0	6. O
Data point number	83223166	83223109	83223110	83223111	83223112	63223113	62223114	61162250	81255005	81255887	81255000 81255008	8 1255000	83255010	83255011	83255012	83255013	83255914		83255916	83255017	83255018	83255019	83255020	83255021	83255022	83255023	83255024	63255025	630550	6323362/ 81355638	83255029	83255030	83255831	83255032	83255035	83255036	83255037	83255038	83255839	83255840	83255841	63255842	83255843	82222844
Rotor	=	II	I	<b>:</b>	<b>⊒</b> ;	<b>-</b>	7 -	7:		::		:=	:=		:=	=======================================	==	=	II	=	=	=			I		=:	= :	<b>≓</b> ;	<b>:</b>	:=	II	11	II	11	1	=	1	I	= :	Ξ:	= ;	=:	=

bomping.	42.9	9 244	-6.241	-6.242	-0.240	-0.241	-0.239	-0.232	-6.239	-0.233	<b>9.264</b>	-0.256	-0.256	-0.256	-0.263	<b>-0</b> .255	<b>-0</b> .249	-6.247	<b>-6</b> .248	9.24	-6.243	<b>-0</b> .244	<b>-0</b> .229	-0.240	<b>-0</b> .235	-0.237	-0.239	<b>6.256</b>	-6.238	-0.226 0.226	-6.23e	-6.223	-0.228	-6.224	6.208	-0.221	<b>-0</b> .223	<b>6</b> .218	<b>-0</b> .253	-0.264	<b>-0</b> .262	-0.261	-6.249		770 9	117.0
Frequency.	7 420	3,442	3,431	3.429	3.438	3.450	3.444	3.431	3.434	3.440	3.438	3.432	3.440	3.427	3.425	3.427	3.448	3.446	3.448	4¥.0	3.448	3.423	3.434	3.434	474.6	3.427	3.438	3.434	3.442	3.448	404.0	3.432	3.425	3.421	5.429	3.423	3.442	3.436	3.438	3.432	3.446	3.434	3,429	777 5	CF7 P	110
Shaft angle, deg	14 94	-14.04	-16.88	-16.98	-18.65	-16.05	-19.97	-19.97	-19.98	-19.98	9.95	<b>-6.0</b> 2	<b>-6.0</b> 2	<b>-8</b> . <b>9</b> 2	<b>-8</b> . <b>6</b> 2	<b>-8.0</b> 2	-10.06	-10.06	-10.06	-11.95	-11.95	-11.95	-14.06	-14.06	-14.06	-14.06	-15.93	-15.93	-15.93	-15.93	/B: / L=	76.71-	/B./L-	-17.97	33. SI-	-19.95	-20.00	-20.00	-6.02	-6.93	-6.93	-6.93	-7.99	-7 99	7 00	50·1
Advance	150	151	150	6,151	0.151	6.158	6.151	0.151	6.152	9.150	0.197	<b>9</b> .198	<b>9</b> .580	0.201	0.200	6.199	<b>9</b> .195	6.197	<b>9</b> .196	<b>6</b> .198	<b>9</b> .198	<b>6</b> .195	9.196	<b>6</b> .198	9.196	●. 198	<b>6</b> .198	0.197	. 198	6.197	0 0	6.197	981.9	6.196	6.201	0.202	6.291	9.500	0.249	0.248	0.249	0.253	0.243	9.248	870	) + 4 · 0
Rotor speed, rpm	748 72	74.9 77	749.67	748.96	749.88	750.93	750.58	749.42	749.65	750.23	749.77	749.30	749.88	748.96	748.72	748.96	756.58	750.58	750.58	750.46	756.93	748.84	750.00	750.00	750.00	749.30	750.35	750.23	750.81	750.70	750.12	749.77	748.50	749.07	748.50	748.84	750.23	749.88	749.54	749.07	750.12	749.30	748.72	750.00	740 10	D D
Collective pitch, deg			• • • • • • • • • • • • • • • • • • •		9.6	9.0	9.0	9.0	9.5	3.0	9.5	<b>9</b> .0	<b>0</b> .0	<b>9</b> .0	۵.6	<b>0</b> .0	<b>⊕</b> .n	<b>⊕</b> .n	<b>9</b> .0	<b>⊕</b> .n	<b>0</b> .0	٥.6	a.e	o.n	<b>9.0</b>	<b>9.0</b>	<b>0</b> .0	<b>0</b> .0	<b>0</b> ,	<b>0</b> .0	D.O.	٠, هـ	<b>.</b>	<b>9</b> .0	D. 70	<b>9.</b> 0	o.0	<b>9.0</b>	3.0	3.0	9.0		) <b>(</b>	• <b>•</b>	; ; ;	D .
Data point number	#1255644	81255646	81255A47	83255848	83255849	63255650	83255851	83255052	83255853	83255854	83256004	83256005	83256006	83256007	83256008	83256009	83256010	83256011	83256012	83256013	83256014	83256015	83256016	83256017	83256018	83256019	83256020	63256021	83256022	83256023	83256024	83256025	83256026	83256027	63256028	63256629	83256030	83256031	83256834	83256035	83256036	83256837	A1256A18	81256A19	0700000	9490C7C9
Rotor	=	: =	: =	: =	:::	II	II	-		11	II	11	11	11	11	11	=	=	II	II	11	11	11	=	11	II	=			I	-	I	I	I	=	Ξ	Ξ	Ξ	11	II	11	=	: -	:-	: :	

ត្រាំស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្នាស់ស្ 	Data point number	Collective pitch, deg	Rotor speed,	Advance ratio	Shaft angle, deg	Frequency, Hz 3.427	Damping, 1/sec
0.256 0.256 0.257 0.258 0.258 0.258 0.259 0.250 0.		9 <b>9</b> .	749.30	0.247	-10.03	3.432	6.245
9.256 9.251 9.243 9.243 9.243 9.243 9.243 9.243 9.243 9.243 9.243 9.254 9.253 9.254 9.255 9.		3.0	748.72	0.244	-12.04	3.421	<b>-0.234</b>
0.251 0.243 0.2448 0.2488 0.2488 0.255 0.255 0.255 0.255 0.256 0.256 0.256 0.256 0.256 0.256 0.256 0.256 0.266		3.0	748.72	0.250	-12.04	3.421	-0.228
0.251 0.249 0.249 0.240 0.254 0.254 0.255 0.255 0.255 0.255 0.256 0.		<b>9</b> .0	750.93	0.251	-12.64	5.456	9.24
0.248 0.243 0.243 0.248 0.248 0.248 0.259 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.248 0.250 0.250 0.248 0.299 0.299 0.298 0.298 0.298 0.298 0.298 0.298 0.298 0.298 0.298 0.298 0.298 0.298 0.298 0.244 0.298 0.298 0.244 0.298 0.298 0.244 0.298 0.298 0.244 0.298 0.298 0.244 0.298 0.244 0.298 0.244 0.244 0.298 0.244 0.		a. •	750.12	0.251	-12.04	25.00	6.24
9.243 9.246 9.248 9.248 9.259 9.255 9.255 9.256 9.257 9.256 9.256 9.256 9.256 9.256 9.257 9.256 9.256 9.256 9.256 9.257 9.256 9.257 9.256 9.257 9.256 9.256 9.257 9.256 9.256 9.256 9.257 9.257 9.257 9.257 9.257 9.257 9.257 9.257 9.256 9.256 9.256 9.257 9.		<b>9</b> .0	750.70	0.249	-14.04	5.440	[2. <del>9</del>
0.242 0.248 0.258 0.259 0.250 0.		J. 0	750.23	0.243	-14.04	6.400	6.223
9.248 9.259 9.259 9.259 9.259 9.259 9.259 9.298 9.299		3.0	749.77	0.242	-14.04	454.0	-8.23g
9.248 9.255 9.255 9.255 9.255 9.255 9.255 9.255 9.256 9.257 9.256 9.257		<b>9</b> .0	748.72	0.248	-14.04	3.421	-6.224
9.259 9.252 9.252 9.252 9.253 9.254 9.254 9.254 9.256 9.256 9.256 9.256 9.256 9.256 9.256 9.257 9.258		3.0	749.65	0.248	-16.04	3.436	<b>-6</b> .213
9.253 9.255 9.255 9.256 9.257 9.257 9.257 9.256 9.256 9.256 9.257 9.257 9.256 9.257 9.		3.0	749.42	0.259	-16.04	3.436	<b>6</b> .213
9.252 9.252 9.256 9.		<b>6</b>	749 77	6.253	-16.04	3.438	<b>-0</b> .220
0.256 0.256 0.256 0.256 0.248 0.248 0.248 0.256 0.		•	749 65	A 252	-17.98	3.442	<b>9</b> .208
0.246 0.246 0.246 0.248 0.248 0.248 0.248 0.248 0.248 0.298 0.298 0.298 0.298 0.299 0.299 0.299 0.299 0.298 0.		9.6	0.614 46 46	9.50	17 98	3 450	2.2
9.256 9.		D •	740.53	0.436 0.53	00.71-1	434	192
0.256 0.248 0.298 0.298 0.298 0.298 0.298 0.398 0.		P (	/D.U.	4.434 4.04	17.00	777	200
9.248 9.248 9.248 9.248 9.298 9.298 9.344 9.398		9.0	140.00	0.240	00.71	4.4	400
6.248		<b>D</b> .01	74.84/	BC7.B	80.00	4 446	204
9.249 9.296 9.296 9.296 9.296 9.298 9.309		<b>9</b> .0	750.12	6.24g	000	77	45.6
6.296		B. (	749.77	0.240	96.91	3.442	96.4
6.298		B. 0	749.77	6.248	000	2.4.5	97.9
6.299 6.299 6.299 6.390 6.390 6.390 6.390 6.390 6.390 6.390 6.290 6.		<b>9</b> .0	740.00	0.530	79.0	10.4 14.4 14.4	74.6
6.299 -7.99		<b>9</b> .0	749.54	6.298		2.45	107.P
6.299 6.399 6.399 6.399 6.399 6.299 6.299 6.299 6.299 6.299 6.2988 6.2988 6.2		D.0	726.23	900		7.7	977
6.297 6.308 6.308 6.308 6.308 6.308 6.308 6.2988 6.2988 6.2		ص. ا	748.96	6.299	66./-	5.428 1.428	6.243
9.399 9.399 9.399 9.399 9.298 9.298 9.298 1.10.90 9.298		G.0	749.19	0.297		5.452	<b>7 7 7 7 7 7 7 7 7 7</b>
9.399 9.392 9.393 9.299 9.298 9.298 1.10.001 9.298 1.10.005 9.399 1.12.00 9.399 1.12.00 9.399 1.13.00 9.398		۵. ۵.	749.88	9.399	-7.99	004.0	97.70
6.382 6.381 6.386 6.298 6.298 6.298 6.386 6.		<b>3.0</b>	751.16	9.380	66.7-	3.452	<b>9</b> .23 <b>6</b>
6.299		3.0	749.88	0.302	-10.01	d. 438	6.233
9.388 9.298 9.298 9.298 9.298 1.19.06 9.298 1.10.00 9.301 1.12.00 9.302 1.11.99 9.303 1.12.00 9.304 1.12.00 9.304 1.12.00 9.304 1.12.00 9.306 1.13.00 9.306 1.13.00 9.306 9.306 1.13.00 9.306 9.307 9.306 9.306 9.306 9.307 9.306 9.307 9.306 9.307 9.306 9.307 9		J. 0	749.65	6.301	-10.01	3.432	<b>-6</b> .236
9.299 9.298 9.298 9.298 9.298 1.10.06 9.300 1.12.00 9.300 1.12.00 9.300 1.12.00 9.300 1.13.96 9.300 1.13.96 9.300 1.13.96 9.300 1.13.96 9.300 1.13.96 9.300 1.13.96 9.300 1.13.96 9.300 1.13.96 9.300 1.13.96 9.300 9.30		3.0	750.00	9.388	-10.01	3.438	<b>6.</b> 238
9.298 9.298 9.296 19.96 9.298 9.399 112.99 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96 9.399 113.96		3.0	750.12	0.299	-10.01	3.442	<b>9</b> .238
9.298 9.296 9.298 1.10.066 9.300 9.300 1.12.000 9.300 1.12.000 9.300 1.13.000 9.300 1.13.000 9.300 1.13.000 9.300 1.13.000 9.300 1.13.000 9.300 1.13.000 9.300 1.13.000 9.300 9.300 1.13.000 9.300 9.300 9.300 1.13.000 9.300 9		3.0	749.42	6.298	-10.05	3.429	9.549
9.296 9.298 1.12.00 9.300 1.12.00 9.300 1.12.00 9.300 1.13.00 9.298 1.13.00 9.298 1.13.00 9.298 1.13.00 9.298 1.13.00 9.298 1.13.00 9.298 1.13.00 9.298 1.13.00 9.298 1.13.00 9.298 1.13.00 9.300 1.13.00 9.300 1.13.00 9.300 1.13.00 9.300 9.300 1.13.00 9.3		6	759.35	0.298	-10.03	3.438	<b>-0</b> .232
0.298		9.5	750.00	0.296	-10.06	404.6	<b>-0.243</b>
6.366 6.361 6.362 6.366 6.366 6.366 6.298 6.298 6.296 6.296 6.296 6.296 6.296 6.296 6.296 7.454 6.295 7.454 7.454 7.454 7.454 7.454 7.454 7.454 7.454 7.454 7.454 7.454 7.454 7.454 7.454 7.454		6	751.51	0.298	-10.06	3,454	<b>-9</b> .238
6.299 -11.99 3.432 -6 6.299 -11.99 3.446 -6 6.298 -13.96 3.454 -6 6.298 -13.96 3.454 -6 6.299 -13.96 3.454 -6 6.295 -13.96 3.444 -6 6.295 -13.96 3.444 -6 6.295 -13.96 3.444 -6		9 6	749.88	9.390	-12.00	3.431	9.249
9.299 9.296 9.298 1.13.96 3.454 9.298 1.13.96 3.454 9.299 1.13.96 3.454 1.3.96 3.454 1.3.96 1.444 9.295 1.4.96		9	750.00	195	-12.00	3.432	<b>-0</b> .228
9.298		9 6	750.55	200	11.00	3.440	<b>-0</b> .232
9.298			766.53	667.0	40.04	442	A 228
6.298		P 6	764 48	9000	90.11	4.454	198
6.299 -13.96 3.444 -0 6.295 -13.96 3.446 -0 6.396 -16.11 3.446 -0		P (	97.107	067.0	96.1	484	790
6.295 -13.96 3.446 -6		B. 0	731.16	0.730	90.1		100.0
6.244 6.306 11.81 0.446 6.307 11.81		B. ?	/56.23	887.0	10.80	444	4.60
.42 6.388 -16.11 5.454 -18.		<b>9</b> .	750.35	6.295	08.01-	944.0	99.
		S. 8	749.42	. 300 . 300	10.1	*****	107.0

Domping. 1/sec	-6.187	-9.205	9.198	-0.207	<b>19</b> .191	-6.188	-6.189	. 191 191	ا 139	<b>-6.171</b>	9.249	<b>6</b> .258	<b>-0</b> .252	-6.246	<b>-0</b> .221	<b>-6</b> . 228	<b>6</b> .234	<b>-6</b> .212	<b>-0</b> .22 <b>0</b>	<b>-0</b> .207	<b>-6</b> .233	<b>-0</b> .182	<b>-6</b> .198	<b>-6</b> . 194	-6.203	<b>-6</b> .186	<b>-6.165</b>	<b>9.176</b>	<b>-6</b> .187	9.176	- F	71.9	<u> </u>	<u> </u>	4	4 4	288	-0.578	-6.572	-6.581	<b>-6</b> .577	.581 6.581	<b>-6</b> .581	<b>49.264</b>	<b>-0.574</b>
Frequency.	3,442	3.446	3.444	3.434	3.44	3.4	3.450	3.454	3.446	3.450	3.440	44.	3.442	47.47	3.436	3.432	3.427	3.438	3.450	3.423	3.429	3.440	24.0	3.427	3.440	3.425	3.427	3.442	3.444	3.467	3.458	5.44e	5. 4. E	3.436	4 448	3.456	3.456	3.448	3.454	3.460	3.456	3.448	3.44	3.446	3.450
Shaft angle, deg	-16.11	-16.11	-17.98	-17.97	-17.98	-17.97	-20.00	-20.00	-20.00	-20.00	-8.00 -8.00	8.9	98. 98.	8-1-8-1-8-1-8-1-8-1-8-1-8-1-8-1-8-1-8-1	-8.90 -8.00	<b>8</b> .	<b>8</b> .	-10.00	-10.03	-10.02	-10.03	-12.04	-12.04	-12.04	-12.04	-14.01	-14.00	-14.00	-14.00	-16.01	-16.01	16.91	10.01	117.00	17.99	-17.99	-12.06	-12.07	-12.07	-14.00	-14.00	-16.04	-16.04	-17.97	-17.97
Advance	905	9.303	6.295	0.298	9.296	0.298	<b>9</b> .288	6.386	9.301	9.301	9.348	9.351	6. GA	0.347	6.351	0.351	<b>6</b> .348	Ø+0. ●	0.353	0.352	0.353	0.348	0.348	6.351	6.348	0.352	9.348	0.351	0.352	0.340	6.336	0 . c	900	. 540 747	448	345	6.694	6.693	0.091	6.693	6.691	0.093	0.093	9.00	<b>6</b> . <b>6</b> 9 <b>4</b>
Rotor speed,	756. 12	750.35	750.23	749.19	750.00	750.00	750.12	750.35	749.54	749.77	749.88	749.88	750.00	749.54	749.77	749.30	748.84	756.66	750.81	748.72	749.30	749.77	749.65	748.72	750.00	748.49	748.49	749.65	750.00	751.39	750.46	749.65	740.30	750.12	749 46	75. 12	749.77	749.54	749.77	750.23	750.12	749.19	749.67	749.19	749.54
Collective pitch, deg				9.0	<b>9.</b> 0	3.0	3.0	<b>3.0</b>	<b>9</b> .0	<b>d.</b>	3. <b>0</b>	<b>9</b> .0	٠. ا	. O.	9.0 9.0	о. Р	o.n	۵.0	3.0	3.0	3.0	3.0	3.0	3.0	J. 0	<b>3.0</b>	3.0	<b>9.</b> 0	д. Ф.	<b>.</b> .	<b>.</b> .	0.7·	B. (	P	• • • •	9 6	•		9	6.6	6.6	<b>9</b> . <b>9</b>	<b>9.9</b>	<b>0</b> .0	<b>6</b> .
Data point number	A1250A2A	83258021	83258822	83258023	83258624	83258025	83258026	83258827	83258028	83258029	83258834	83258835	83258836	83258841	83258042	83258843	83258644	83258645	83258046	83258647	83258048	83258649	83258050	83258051	83258852	83258053	83258054	83258055	83258056	83258057	83258858	83258659	9252666	63236601	1000TC	84258864	83259828	83259029	83259030	83259031	83259032	83259033	83259034	83259035	83259036
Rotor	11	:=	:=	Ξ	Ξ	=	=	=	=	II	II	=		=	=	II	=	11	11	11	=======================================	=======================================	11	=	II	II	11	11	II	11	II	Ξ:	;;		-	- F	:=	: [	=======================================	II	Π	Π	II	II	=======================================

Domping. 1/80c	-6.578	985. P	<b>6.578</b>	<b>-9.567</b>	<b>-8.577</b>	<b>-0.575</b>	<b>-9.567</b>	<b>-8.575</b>	<b>-6</b> .578	<b>-6.576</b>	<b>-0.573</b>	<b>-9</b> .561	<b>-8</b> .575	<b>-0</b> .586
Frequency.	3.465	3.456	3.454	3.460	3.460	3.442	3.446	3.429	3.461	3.450	3.438	3.440	3.450	3.438
Shaft angle, deg	-19.98	-19.98	-16.05	-16.05	-18.01	-18.01	-20.00	-20.00	-15.97	-15.97	-18.01	-18.01	-20.00	-20.00
Advance	6.693	9.00	9.148	9.148	9.148	6.149	9.144	6.143	0.195	9.196	0.197	6.196	9.195	9.196
Rotor speed, rpm	750.70	750.23	749.77	750.23	750.35	749.19	749.30	748.26	750.58	749.65	748.96	749.19	750.23	749.19
Collective pitch, deg	9.9	9.9	6	6	9.9	6	9.0	9.	6	6	6	9	9.9	9.
Data point number	83259637	83259838	83259839	83259040	83259841	83259042	83259843	83259044	83259045	83259046	83259047	83259648	83259049	83259850
Rotor	II	II	II		===	=	=	I	=				Ξ	=

TABLE 11. - REGRESSING LEAD-LAG MODE DATA IN FORWARD FLIGHT, CONFIGURATION WITH STRUCTURAL FLAP-LAG COUPLING, 1888 RPM

Damping. 1/sec	-8.164	9.165	9 6	9.161	-0.163	<b>. 160</b>		<b>-8.162</b>	9 9		9	-6.158	-6.157	<b>-6</b> . 158	-6.157	-6.158	-a.155	-6.138	9 9	100	9 <del>9</del>	-6.167	<b>-6</b> .169	<b>9</b> .169	-6.167	-0.166	-6.168	791.9	9 9	-6.163	-0.165	-0.164	-6.164 	- <b>6</b> .168	-0.176	<b>-6.172</b>	-6. 186	9.184	-6.286	- 193 193	<b>-6.263</b>	<b>-0</b> .206
Frequency,	6.428	6.440	6.422	6.469	6.405	6.436	6.438	6.432	6.432	A 428	6.422	6.422	6.430	6.430	6.430	6.424	6.411	6.428	6.44	6.430	6.436	6.422	6.422	6.428	6.412	6.414	6.418	24.4	6.418	6.428	6.420	6.438	6.430	6.438	6.443	6.447	6.426	6.428	6.418	6.414	6.432	6.414
Shaft angle, deg	6.62		) G	4.02	<b>5</b> .	<b>6.04</b>	40.0	10.00 10.00	8. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.		-11.97			-14.00	-16.04	-16.04	-17.98	-17.98	49.64	* G	9 6	98.	1 <del>0</del> .01	-2.01	-2.01	86.51 10.08	86.5	20.0		-7.99	-7.99	-10.00	-10.66	-12.04	-12.04	-12.02	13.96	-13.96	-16.01	-16.00	•	-17.97
Advance	6.044	0.642	940	0.045	9.04	<b>9</b> .0	0.044	6.645	9.044	44	440.0	0.043	0.043	0.043	0.043	0.043	0.043	250.0	9. 6 5. 6	9.6	> 00 90 90 90 90 90	6.692	9.682	9.00	0.097	6.697	6.697	60.00 00.00	80.0	660.0	6.68	660.0	0.097	6.697	6.697	6.697	6.697	6.097	0.097	0.097	960.0	0.636
Rotor speed,	69.68	1000.62	50.000 50.000	997.95	997.60	1000.39	1000.62	28.88	1999.15	2000	900.00	999.34	1000.04	999.92	999.92	999.46	998.41	10.000 10.000	1996.85	2000.13	999.11	999.57	989.34	999.92	998.65	888.88	999.23	1861.32	77.000 00 800	1000.04	999.34	1666.85	1000.27	1666.97	1001.43	1001.55	999.46	999.69	998.88	998.53	1000.04	998.53
Collective pitch, deg	•	9.0	9 6	0.0	0.0	<b>0</b> .0	0.0	<b>.</b>	<b>6</b> 6		9 6	9.9	0.0	<b>9</b> .0	<b>.</b>	<b>0</b> .0	<b>.</b>	9 (	<b>5</b> 6	•	9 G	9.9	0.0	<b>.</b>	<b>0</b> .0	<b>6</b> .	<b>6</b>	S	9 G	9	0.0	<b>6</b> .6	<b>6</b> .0	<b>9</b> .	<b>9</b> .0	<b>6</b> .0	<b>6</b> .0	<b>6</b> .	0.0	<b>6</b> .	0.0	<b>9</b> .
Data point number	83223120	83223121	83223123	83223124	83223125	83223126	83223127	83223128	83223129	001C77C0	83223132	63223133	83223134	83223135	83223136	83223137	83223138	83223139	83223140	1410776	83224004	83224006	83224029	83224007	83224008	83224009	83224010	63224011	21972248 21972278	83224014	83224015	83224016	83224017	83224018	83224019	83224620	83224021	83224022	83224023	83224024	83224025	83224026
Rotor	11	=:	 -	: ::	Ξ	11	1	I	==	: E	7 14		1	=	11	<b>!</b>	<b>I</b> :	= :	===	-	==		Ξ	11	=	I	I:	7:	::	:=	I	==	II	11	11	=	II	=======================================	11	II	=	II

Domping. 1/sec	-0.204	<b>-9.204</b>	+01.0+	6.179			<b>-6.174</b>	-0.163	<b>6</b> .178	-e. 180	-6.176			•	•	-0.172	<b>6.173</b>	-6.165	<b>-9</b> .166	-6.176	. 168 88	<b>4</b> .172	-0.162	<b>-0</b> .176	-B. 168	-0.162	-6.177	<b>-6.175</b>	6.173	<b>-6.176</b>	-0.198 -0.198	-6.196 	-6.189	-6.187	6.287	-9.202	-0.205	-0.193	-0.286	-0.212	-0.212	-0.207	-0.208	-0.212	-0.210	-0.202
Frequency,	6.426	6.420	6.639	6.639	6.639	6.412	6.434	6.434	6.428	6.652	6.652	6.639	6.436	6.438	6.639	6.639	6.639	6.424	6.428	6.639	6.639	6.639	6.443	6.438	6.414	6.432	6.639	6.639	6.424	6.428	6.639	6.639	6.447	6.426	6.639	6.639	6.438	6.438	6.436	6.639	6.654	6.436	6.432	6.639	6.652	6.453
Shaft angle, deg	-19.64	-19.65	<b>9</b> 0.00	8.	8.0	<b>9</b> .	<b>9</b> . <b>9</b>	0.03	6.01	-2.00	-5.6	-2.8	-2.02	-2.02	8.7	<b>8</b> .†	8.7	4.02	4.02	<b>8</b> .9	<b>8</b> .9	<b>8</b> .9	-5.99	-5.99	-5.99	<b>8</b> .	-8.80 -8.80	<b>8</b> .	-7.99	-7.99	-10.00	-16.96	-10.03	-10.03	-12.00	-12.00	-12.07	-12.08	-12.08	-14.00	-14.00	-14.00	-14.00	-16.00	-16.00	-16.02
Advance ratio	9.00	0.095	0.149	0.142	6.149	9.148	9.148	9.146	0.152	9.149	9.146	9.148	9.146	6.150	9.148	9.148	0.149	0.150	0.147	9.148	9.148	0.148	0.150	6.148	6.148	<b>6</b> .148	0.149	9.147	9.148	9.148	0.149	9.148	<b>9</b> .148	0.148	0.149	9.148	6.150	0.149	9.159	9.148	0.147	0.149	6.149	9.147	0.147	6.149
Rotor speed, rpm	989.57	999.11	1000.08	1001.13	999.38	998.30	1000.04	1666.15	999.57	1000.31	1000.08	1000.08	1000.27	1000.39	1999.98	989.88	1000.08	999.34	999.57	96.666	999.61	1000.31	1666.97	1000.39	998.41	999.92	1000.43	999.84	999.46	989.46	999.84	98.86	1001.08	999.23	999.38	1666.31	1000.15	1000.27	1000.15	1000.78	1000.08	1000.15	999.81	989.26	86 666	1001.66
Collective pitch, deg	•	•	<b>6</b> .0	<b>.</b>	<b>.</b>	<b>.</b>	9.0	9.0	9.	9	9.6	9.6	9.	9.9	9.0	9.0	0.0	9.	9.	9.0	9.9	<b>9</b> . <b>9</b>	<b>9</b> . <b>9</b>	0.0	●.●	<b>9</b> . <b>0</b>	0.0	<b>9</b> .0	9.0	<b>9</b> .0	9.0	<b>9</b> .0	<b>9</b> .	<b>9</b> .	<b>6</b> .	•.	<b>.</b>	<b>0</b> .0	<b>0.0</b>	0.0	0.0	9.0	9.6	6	6	9
Data point	83224027	83224028	82263003	82263005	82263017	83224032	83224033	83224058	83224059	82263004	82263006	82263018	83224034	83224035	82263007	82263008	82263019	83224036	83224037	82263009	82263020	82263021	83224038	83224039	83224040	83224041	82263010	82263022	83224042	83224043	82263011	82263623	83224044	83224045	82263012	82263024	83224046	83224047	83224048	82263013	82263025	83224049	83224050	82263014	82263026	83224051
Rotor	11	11	-		<b>-</b>	=	=======================================	II	Ξ	-		-	11	=	-		<b>-</b>	=	I	; <b></b>	<b>—</b>	<b>~</b>	11	=	=	=======================================	-		11	11	<b>-</b>	<b>—</b>	I	11	<b>-</b>	<b></b>	11	II	11	<b>-</b>	<b>-</b>	II	II	•		<b>'</b> =

Rotor tested	Data point number	Collective pitch, deg	Rotor speed,	Advance ratio	Shaft angle, deg	Frequency.	Domping. 1/sec
)   				<b>l</b>			
11	83224052	•••	1000.62	6. 148 8 48	-16.63	6.440	<b>-6</b> .202
-	82263015	•.•	999.84	9.748	-18.99	6.639	<b>-6</b> .205
	82263627	•.•	999.84	0.148	-18.00	6.648	<b>-6</b> .21 <b>0</b>
11	83224853	•.•	999.81	<b>6</b> .148	-18.00	6.432	<b>-6</b> .212
<b>.</b>	83224054	•.•	999.23	0.147	-17.99	6.424	<b>-0</b> .207
11	83224055	•.•	998.88	<b>9.1</b> €	-17.99	6.420	<b>-6</b> .2 <b>08</b>
-	82263016	•.•	1000.08	<b>6</b> .148	-20.00	6.639	<b>-6</b> .207
-	82263628	•.•	1666.43	0.148	-20.00	6.658	<b>-6</b> .201
11	83224056	•.•	1661.26	9.147	-19.64	6.447	<b>-6</b> .269
11	83224857	0.0	1000.39	0.147	-19.64	6.438	<b>-6</b> .206
<b>-</b>	62263029	•.•	1000.55	0.202	<b>6</b> .66	6.658	<b>9</b> . 180
-	82264001	• •	999.84	Ø. 199	<b>6</b> .66	6.643	<b>-6</b> .186
-	82264002	0.0	1001.72	9.200	99.9	6.664	<b>6.179</b>
==	83224062	•.•	998.18	6.199	0.02	6.412	<b>-6.169</b>
11	83224063	•.•	999.57	6.199	0.62	6.428	<b>6</b> .178
11	83224064	•.•	999.92	0.197	0.02	6.444	<b>6</b> .172
-	82263030	•.•	1001.25	0.200	-2.00	6.668	<b>6.179</b>
<b>-</b>	82264003	0.0	1000.55	6.199	-2.00	6.650	<b>98</b> . <b>9</b>
-	82264004	•.•	1661.13	6.198	-2.00	6.658	<b>-6</b> .186
11	83224065	•.•	998.99	0.201	-2.06	6.424	<b>6</b> .169
I	83224066	•.•	999.46	9.198	-2.06	6.428	<b>-6</b> .167
·	82263631	0.0	1666.78	0.201	8.	6.669	<b>6.17</b>
	82264005	0.0	1666.96	0.201	8.†	6.656	. 165 55
-	62264007	•.•	1666.26	0.200	8.7	6.646	6.178
11	83224067	•.	1661.43	6.199	-3.95	6.451	9.18
11	83224068	•.	996.99	6.199	-3.99	6.422	<b>-0</b> .162
-	82263032	•	98.88	0.201	<b>8</b> .99	6.652	<b>.</b> 178
	82264008	<b>9</b> . <b>9</b>	999.49	<b>9</b> .200	<b>9</b> 8.9	6.643	-6.199
-	82264009	<b>9</b> .9	1666.65	<b>6</b> . 199	<b>98</b> .99	6.646	<b>6</b> . 6
	83224069	<b>.</b>	998.99	6.201	-5.99	6.422	<b>-0</b> .166
=	83224070	•.	999.92	6.199	-5.99	6.432	<b>-6</b> .182
11	83224071	•.	998.76	0.201	5.98 8.5	6.429	<b>6</b> .171
<b>:</b>	83224072	•.•	989.57	6.198	-5.99	6.432	ન આ
-	82263033	•.•	999.62	0.201	<b>8</b> 8.	6.639	<b>-6</b> .195
-	82264010	•.•	1666.78	6.199	<b>88.89</b>	6.656	<b>-0</b> .2 <b>0</b> 2
-	82264011	0.0	1001.25	9.266	<b>8</b> .89	6.662	<b>-9.206</b>
-	82264012	•.•	98.88	0.200	<b>8</b> .86	6.648	<b>-6</b> .206
II	83224073	•.•	999.11	0.201	-7.99	6.428	¥ 9.
II	83224074	•.•	1666.62	<b>9</b> .199	-7.99	6.443	<b>-0</b> .192
11	83224075	<b>9</b> . <b>9</b>	999.68	<b>6</b> .199	-7.99	6.432	<b>-6</b> .182
Ξ	83224076	•.•	999.34	0.196	-7.89	6.432	<b>7</b> . <b>9</b>
-	82263034	<b>.</b>	1001.13	0.202	-10.00	6.666	<b>-0</b> .2 <b>06</b>
-	82264013	•.	98.88	6.199	-10.00	6.646	<b>6</b> .211
-	82264014	<b>9</b> .	999.26	0.198	-10.00	6.641	<b>6</b> .211
11	83224077	<b>0</b> .0	998.88	<b>6</b> . 199	-10.03	6.424	<b>-0</b> .206
11	83224078	0.0	998.88	0.201	-10.03	6.424	-0.212

Damping. 1/sec	-6.196	- <b>6</b> . 199	<b>-0.213</b>	-6.208	997.9	9.786	207.0	112.9	-6.209	- P. 195	-0.200	-6.196	-6.199	86 - 98 - 188	-a. 195	<b>-9.291</b>		48.184	-9.292 	<b>-0</b> .192	-6.291	-6.179	. 189	-6. 199	<b>-6</b> .187	- P	-0.182	96.196	\ 		7/-	9	9	2 4	9,175	-6.181	J. 177	-6.187	<b>-6</b> .180	<b>-6</b> .177	<b>9</b> .168	<b>-6</b> .172	-6.189	196	<b>6.169</b>
Frequency.	6.428	6.674	6.648	6.648	0.000	6.426	6.418	6.432	6.426	6.652	6.652	6.656	6.652	6.422	6.412	6.448	6.438	6.648	6.650	6.652	6.656	6.432	6.436	6.432	6.438	6.666	6.682	6.658	6.6/8 6.6/8	6.662	9.00	2/0.0		6.65	6.432	6.445	6.434	6.650	6.646	6.445	6.426	6.445	6.660	6.641	6.434
Shaft angle, deg	-16.63	-12.00	-12.63	-12.00	-12.66	-12.62	-12.62	-12.62	-12.62	-14.00	-14.00	-14.00	-14.00	-14.00	-14.00	-14.00	-14.00	-16.00	-16.00	-16.00	-16.00	-16.01	-16.01	-16.01	-16.01	18.99	-18.96	-18.90	-18.66	-20.00	20.00	-26.06 20.05	99.97	9 6	000	6.62	0.02	-2.60	-2.00	-2.06	-2.06	-2.06	1	7	-3.99
Advance ratio	6.199	0.203	6.198	0.200	60.199	6.197	0.201	0.201	0.200	0.202	6.199	6.199	0.198	<b>6</b> . 199	0.197	<b>6</b> . 198	6.199	0.202	0.200	0.200	0.199	0.199	0.197	6.199	0.200	0.200	6.197	0.199	9.286	0.202	907.0	6.198	0.13/	9.23.	9.50	9.249	0.249	0.250	0.251	0.248	6.249	0.249	0.250	0.250	0.252
Rotor speed,	999.11	1901.69	1000.20	1666.26	1991.69	999.34	998.53	999.57	999.11	1000.08	1000.43	1666.78	1000.55	998.99	998.97	1000.27	1000.15	999.49	96.666	1666.68	1000.43	999.46	999.81	999.57	999.92	1000.31	1001.84	1000.08	1661.13	999.61	57.588	1999.56	1000	900.00	-0.000	1999.97	1000.04	96.66	48.000	1000.97	999.23	1666.97	1861.62	90 000	999.92
Collective pitch, deg	6	0.0	9.6	•	9.	<b>9</b> . <b>9</b>	<b>9</b> .	<b>9</b> .	<b>0</b> .	<b>9</b> .	<b>9</b> .	<b>9</b> .	<b>9</b> .	<b>9</b> .	<b>9</b> .	<b>9</b> .0	<b>9</b> .0	<b>9</b> .	<b>9</b> .0	<b>9</b> .6	<b>9</b> .	<b>0</b> .0	<b>9</b> .	<b>9</b> .0	<b>9</b> .	<b>9</b> .0	9	9.6		D	9 6	) <b>(</b>	6	9.0	9.0	0.0	0.0	0		•	9.0				
Data point number	83224079	82263035	82264015	82264016	82264017	83224080	83224081	83224082	83224083	82263036	82264018	82264019	82264020	83224084	83224085	83224086	83224087	82263037	82264021	82264022	82264023	83224088	83224089	83224090	83224091	82263038	82264024	82264025	82264026	82263939	82264827	82264028	#7040770	82284838	81224894	83224095	83224096	82264032	82264033	83224097	83224098	83224099	82264034	82284035	83224100
Rotor	II	-	_	<b></b> (	-:	I	I	I	=	<b></b>		-	<b></b>	=	=	=	II	-	<b>-</b>	-	-	=	11	<b></b>	11	-	_	-	<b>-</b>	⊶•	~•	→ •	I-	-4 F-		: <u></u>	I	; <del></del>	-	=	II	II	-	-	<u> </u>

Domping. 1/sec	-0.165 -0.171	-6.199	-0.192	-9.196	3 4	<b>6</b> .182	<b>-9</b> .200	-0.198	- <b>6</b> .207	282	<b>-8</b> .201	-0.195	-0.195	- <b>a</b> . 195	<b>-0.182</b>	-8·184	-6.200	100	<b>6</b> .231	-0.229	-0.216	<b>9</b> .182	-6.183	-0.187	-0.173	9.184	9 9	9 6	4. 4. 176	-9.181	-0.184	-0.195	-0.182	<b>-0</b> .176	- <b>6</b> . 184	<b>6</b> .184	<b>-6</b> .175		<b>-6</b> .168	
Frequency,	6.428 6.438	6.648	6.648	6.664	6.436 424	6.428	8.666	6.672	6.436	7	6.639	6.639	6.639	6.639	6.641	6.662	6.639	6.63	6.672	6.639	6.639	6.639	6.639	6.432	6.424	6.426	• •	٠,	. <del>.</del> .	6.434	6.424	6.432	6.432	6.445	6.639	6.639	6.436	6.434	6.441	6.434
Shaft angle, deg	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	7 <b>9</b>	99.9	-6.00 -	, i	-5.92	8.8	-8.80 -8.00	<b>8</b> 8	8 8 9 7	-10.99	-10.66	-12.00	-12.00	•	-14.90	-16.00	90.0	18.00	-20.00	-20.00	99.90	96.90	6.62	9.95	9.60 9.60	999	8	9 6	6	9	6.61	40.0	<b>-0.04</b>	-2.00	-2.00	-2.62	-2.62	-2.62	-2.02
Advance	6.256 6.251	6.250 6.250	6.256	<b>6</b> .25 <b>6</b>	9.236	0.251	6.250	6.249	6.251 6.251	9.240 9.248	0.250	6.254	0.252	0.252	0.252	0.252	9.250 250	9.436	<b>6</b> .253	0.250	0.250	6.301	9.301	0.297	6.298	6. 28. 0.	4.23.7 4.29.4	067.0	392	9.298	6.302	6.301	6.298	6.300	6.300	6.301	6.301	6.298	0.299	0.300
Rotor speed,	999.34 999.57	999.73	999.73	1000.90	000	900.34	1000.90	1661.48	1000.04	+ C. MOO	1000.55	999.84	1666.98	999.84	998.32	989.96	1000.90	00.000 t	987.986	1000.66	1000.90	999.73	999.14	999.81	66.866	4. 000 4. 000	40.04 40.04	1000	1000.73	69.660	998.76	999.46	1666.15	1001.20	96.666	1000.20	1000.04	999.81	1000.62	999.92
Collective pitch, deg	<b>66</b>	9 <b>0</b>	0.0	<b>.</b>	P 6		9.0	•	<b>©</b> 6	P. G		9.0	0.0	<b>9</b> . <b>9</b>	<b>0</b> .0	Ø.	<b>.</b>		9 6	0.0	0.0	•	•	<b>6</b> .0	<b>.</b>	<b>9</b> . 0	P			6	9.0	0.0	0.0	<b>0</b> .0	<b>0</b> .0	<b>.</b> .	<b>9</b> . <b>9</b>	<b>.</b>	<b>9</b> . <b>9</b>	<b>.</b>
Data point number	83224101	82264036	82264037	82264938	83224184	83224106	82264039	82264040	83224107	81224180	82264041	82264042	82264043	82264044	82264045	82264046	82264047	82284848	82264858	82264051	82264052	82264053	82264054	83224110	83224111	62224112	67224113	0777000	81228007	83228008	83228009	83228010	83229004	83229005	82264055	82264056	83224114	83224115	83224116	83224117
Rotor	H H :		-	<b>-</b> :	<u> </u>	:=	-	-	<b>"</b> !		-	•	-	-	<b>-</b>	<b>-</b>	<b></b>		-	-	-	⊷ -	- ;	=	Ξ:	Ξ:	::	::	- L	-	11		II	II	-		II			

Damping. 1/sec	-6.178 -6.171		6.187		•	•	9 9	20.00	٠.	<b>-0</b> .196	-0.190	-8·199	<b>-6.193</b>	- <b>9</b> .196	-0.202 0.203	9.762	282	161	-6.185	<b>.</b> 191	<b>-6</b> .189	-e. 193	-0.244	-0.242 0.242	e . 588	77.9	707	100	<b>6</b> .326	-6.348	-0.215	<b>-6</b> .181	<b>-0</b> .212	•	•	-0.197	-a. 183	-6.194	-6.189	<b>-8</b> .188
Frequency.	6.430 8.430	6.445	6.639	6.445	6.440	6.434	6.434	6.639	6.424	6.428	6.430	6.422	6.440	6.639	6.639		6.457	6.451	6.639	6.639	6.639	6.639	6.639	6.639	6.684	9.92	9.0.0 9.4.4	0.0	6.639	6.639	6.639	6.639	6.639	6.639	٦.	6.428	6.426	6.418	6.639	6.635
Shaft angle, deg	-2. <b>6</b> 2 -2. <b>6</b> 2	-2.67 -2.62	<b>8</b> 8	B 5	4.61	-4.01	÷ .0.		-5.96	-5.96	-5.96	-5.96	-5.96	-8.00	8 8 8 9	88./-	25.7°	20.7	-10.00	-10.00	-12.00	-12.00	-14.00	•	-16.00	99.91-			-28.86	-20.00	96.	99.99	9.00	9.00	<b>6</b> .9	.e.e.	<b>-6</b> . <b>6</b> 2	-6.62	-2.00	-2.60
Advance ratio	6.388 6.382	6.301	6.388	6.366 6.366	0.299	0.297	6.297	000° G	<b>6</b> .298	6.300	0.298	6.300	0.297	<b>6</b> .288	<b>9</b> .299	9.399	. 29 v	400	95.0	6.239	0.300	<b>9</b> .288	9.300	6.299	<b>6</b> .361	6.239	67.58 00.780	0.03	0.00 0.00	9.301	9.350	9.348	6.356	0.353	0.346	0.350	6.356	9.348	6.351	0.352
Rotor speed,	997.95	1889.23 1888.58	999.84	1999.38	999.92	999.46	999.46	00.000	998.53	998.88	998.99	998.41	1999.64	1000.08	1000.43	1666.73	1666.73	26.00	1966.65	1999, 43	1661.37	1001.84	96.666	999.38	999.84	1969.43	1666.28	1991	900 84	9000	1000.08	1999.43	1001.48	1000.08	999.46	89.66	999.57	998.88	999.84	998.32
Collective pitch, deg	<b>0</b> 0 0	<b>.</b> 6	9.0	9 6	9.0	<b>0</b> .0	<b>.</b>	D 6	9 6	9.6	9.	<b>9</b> .0	0.0	0.0	<b>9</b> .0	<b>9</b> .	9 6	9.0		6	0.0	<b>6</b> .0	<b>9</b> .	<b>6</b> .0	<b>9</b> .0	9 (	9.0	9.0		6	9.0	9.0	9.0	0.0	9.0	<b>9</b> .0	<b>9</b> .0	<b>9</b> .0	9.0	<b>9</b> .
Data point number	83228011 83228012	83228014	82264057	82264838	83228016	83228017	83228018	80040770	83228019	83228020	83228021	83228022	83228023	82264061	82264062	83228024	83228025	07007700	82226827 82264863	82264064	82264065	82264066	82264067	82264068	82264869	82264076	82264071	7/040779	822648/3 82264874	82264975	82264976	82264077	82264078	82264079	83229006	83229007	83229008	83229009	82264080	82264081
Rotor	HH?		<b> •</b>		11				11		II			-	- :		<b>:</b>				-	-	-	-	⊷ ,	→•	P	<b></b> •	<b></b>	•			-	-			II		<b>-</b>	<b></b>

Damping. 1/sec	-6.187	<b>-0.183</b>	<b>.</b> 188	<b>184</b>	- <del>185</del>	-6.196	. 183 183	<b>Ja. 175</b>	<b>6</b> .184	<b>-9.186</b>	-0.203	<b>-0</b> .202	<b>Ja.</b> 193	<b>-6</b> . 192	<b>-0</b> .203	9.211	<b>9</b> . 200	9.200	<b>-9</b> .222	-0.237	<b>6</b> .219	<b>-6.228</b>	<b>-6</b> .325	-0.327	<b>-6</b> .375	6.347	- 6.398 - 398	-6.413	<b>-6.363</b>	285.6	0.4.9 0.4.0	9.44.0	464.0		9	217	-6.204	-6. 196	284	200	2000	9.50	20.0	6. 200 10. 400	9	
Frequency, Hz	6.424	6.422	6.434	6.434	6.637	6.639	6.424	6.430	6.422	6.455	6.639	6.639	6.416	6.424	6.428	6.422	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.639	6.639	8.686	6.695	6.691	6.689	6.701	6.695	6.71	17/.0	0.740 8.45		6.653	6.429	6.424	777	451	- CF- W		240.0	6.4	0.4.2 8.43	0.150
Shaft angle, deg	-1.99	-1.99	-1.99	-1.99	<b>8</b> .	<b>8</b> . †	4.62	-4.63	79.4	7.63	<b>8</b> .9	-6.00	-5.98	-5.98	-5.98	-5.98	-8.00	<b>8</b> 0.8	-10.00	-10.00	-16.66	-16.00	-12.00	-12.00	-14.00	-14.00	-16.00	-16.00	-16.00	-10 -10 -10 -10 -10 -10 -10 -10 -10 -10	13.66	-18.00	99.92	99.97-	9		8 8					99.4	<b>8</b> 6.7-	•	B 0	<b>D</b>
Advance	9.350	6.351	0.350	6.349	6.351	9.349	0.352	0.349	6.348	0.347	6.349	0.351	6.349	0.351	6.349	9.351	6.351	9.350	0.351	0.352	6.349	6.348	9.348	6.350	9.320	0.349	6.351	9.350	6.356	6.336	9.330	6.356	9.540 4.40	9.340	900	400	207	950		00°	0.030	191.9	6.465	- 007	90.400	. 166
Rotor speed,	999.23	999.23	1666.27	1000.04	998.67	1666.31	999.34	999.69	999.11	1991.99	1666.43	999.84	998.65	999.68	89.68	998.99	1666.43	1666.28	1000.55	1000.08	1686.96	1661.25	1666.68	989.84	999.49	1666.66	1000.55	1888.43	1666.26	1888.98	988.80	1000.20	1000.43	1004.30	900.73	1000	200	000	000 P	100.00	2000	79.888	7 P P P P P P P P P P P P P P P P P P P		880.10	) ·
Collective pitch, deg	9.	0.0	<b>9</b> . <b>9</b>	9.0	<b>9</b> .	<b>9</b> . <b>9</b>	<b>9.</b>	<b>9.9</b>	<b>0</b> .0	<b>9</b> .	9.0	<b>0</b> .0	<b>9</b> . <b>9</b>	9.0	<b>9</b> .	<b>⊕</b> .	<b>.</b>	<b>9</b> . <b>9</b>	<b>.</b>	<b>.</b>	<b>0</b> .0	•.•	•	<b>0</b> .0	•.•	<b>.</b>	•.•	<b>.</b>	0.0	9.0	9.0	<b>9</b> (	9.0	P			• <b>•</b>		•		9.0		<b>P G</b>		D 6	0.0
Data point number	83229010	83229011	83229012	83229013	82264082	82264083	83229014	83229015	83229016	83229017	82264084	82264085	83229018	83229019	83229020	83229021	82264086	82264087	82264088	82264089	82265001	82265002	82265003	82265964	82265005	82265006	82265007	82265008	82265009	82265010	82265011	82265012	82285913	+19C9779	62263610	82266817	#100000	F400001	4000000	#2067FB	0204400	9196779	62265019	0707070	62528827	07067700
Rotor	11	=======================================	H	11		-	11	11	=======================================	=	-	-	11	11	=	=	-		<b>—</b>	-	-		-	~				-	-	<b>-</b>			<b>-</b> , .	<b></b>	<b></b> 1-		• =	:=	1:	::	7.	<b></b> •	<b>→ :</b>		<b>-</b>	7 7

Damping. 1/sec	-6.207	-0.208	9.108	9 9	207.9	3 5	2.2	41.214	2.218	-0.219	<b>6.313</b>	<b>-9.318</b>	-0.392	<b>-6</b> .374	<b>-6</b> .358	<b>-0</b> .462	4.47	<b>6.47</b>	<b>-6</b> .237	<b>-0.236</b>	-0.221	-0.243	-8.216 0.216	9.217	-6.214	- F. 262	777.	717.0	7 - O	2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	20.4	401	9.195	191	-6.199	<b>-9.288</b>	-0.208	-0.261	-0.272	-6.417	-0.463	<b>-9.4</b> 26	-0.488	-0.477
Frequency,	6.436	6.670	6.654	0.430	27.0		6.643	6.648	6.641	6.645	6.643	6.650	6.682	6.688	6.701	6.688	6.717	6.705	6.658	6.646	6.439	6.439	6.434	6.654	6.636 6.636	0.000	6.632	0.432	0.430	6.420 6.420	. S.	6.428	6.430	6.441	6.434	6.658	6.656	6.674	6.656	6.678	6.689	6.699	6.699	6.695
Shaft angle, deg	-1.99	<b>8</b> .	8.3 † †	7) 7) 1	DD: 7				86	98	-10.00	-10.00	-12.00	-12.00	-14.00	-14.00	-14.00	-16.00	<b>9</b> .00	<b>0</b> .00	6.61	<b>6</b> .90	90.	-2.00	-2.00	-2.ee	-2.66 	7.1	)			7	7	40.4	\$.7	98.99	98.9	<b>8</b> .89	8.8	-10.00	-10.00	-12.00	-12.00	-14.00
Advance	8.398	6.338	0.400	9.407 101	40.40	401.4	6.53 64.61	64.0	402	6.401	0.402	6.463	0.402	0.402	9.401	0.399	<b>6</b> .400	0.396	0.450	0.451	<b>6</b> .449	9.448	9.447	0.450	9.448	6.436	6.451	9. <del>1</del> 1	104.0	0 .449 6 453	454	A 451	6.453	9.448	6.448	6.456	0.449	0.453	9.451	0.447	9.448	0.450	6.456	0.451
Rotor speed,	1999.94	1991.72	1000.43	1888.13	1000.15	1000	17.000 81 000	1000 BR	000	20.000 20.000	998.55	998.91	1000.66	1666.96	1666.31	999.26	1661.37	999.73	1666.43	999.49	999.57	69.666	999.69	1666.68	000.00	1666.68	999.73	30.000 30.000 30.000	1666.64	2000 to 0000 t	000	10.000 17.000	75.000	1000.39	999.92	1000.55	1000.20	1666.78	899.49	1666.68	1666.55	1000.43	1000.43	998.44
Collective pitch, deg	9.0	9.9	<b>6.</b>	9.0	9 G	<b>9</b> 6	9 6	9 6	•		9.6	9.0	0.0	0.0	<b>9</b> .0	0.0	9.3	<b>0</b> .0	<b>9</b> .0	<b>0</b> .0	<b>9</b> .0	<b>0</b> .0	<b>.</b>	0.0	<b>9</b> .	<b>9</b> .0	9 ( 9 (	9.0	9 G	D 6	<b>P</b> 6	9 6		6	9.0	6	9.	0.0	9.0	0.0	9.6	9.6	0.0	0.0
Data point number	83229029	82265020	82265021	83229838	027770010	03223032	82265833	82265022	8226502	82265025	82265926	82265027	82265028	82265029	82265030	82265931	82265032	82265034	82265035	82265036	83229035	83229036	83229037	82265937	82265038	82265039	82265040	82228838	87778878	03228040 03268044	82263641 82365843	8100040	83229643	83229044	83229045	82265643	82265944	82265045	82265046	82265047	82265048	82265049	82265050	82265051
Rotor	11	1	۰;	<b>-</b>	7 -		<u>.</u>	<b></b>	• •	4	-		-	-		-		-	<b>—</b>	-	II	I	I	<b>-</b>	→•	⊸.			<b>1</b>			٠ <u>-</u>	:=	1	II	-		-	-	-	-	-	-	-

Rotor	Data point number	Collective pitch, deg	Rotor speed, rpm	Advance ratio	Shaft angle, deg	Frequency. Hz	Domping 1/80c
1		•			;	e e	809
⊷ ⊩	82265052	•	1999.78	6.406 406	8. 4 4. 4	6.725	-6.242
<b></b>	82265854		1888.88	9.588	9 6	6.664	-0.248
	82265955	0.0	889.49	0.502	-2.60	6.654	-0.217
<b>—</b>	82265056	0.0	1666.28	9.501	-2.00	6.662	9.54
_	82265857	<b>0</b> .0	988.14	6.505	<b>8</b> .	6.648	<b>6</b> .218
_	82265858	<b>9</b> .	999.14	6.563	<b>8</b> :	6.648	-6.199
-	82265059	0.0	98.86	9.500	<b>8</b> .9	6.654	<b>6</b> .233
<b>—</b>	82265969	<b>6</b> .0	1666.31	6.583	99. 19.	9.638 9.638	8+7·9
⊷.	82265961	9.0	1000 .65	9.00	8 8	0.0/0	79
٠.	79009779	D (	200.000 100.000	90.0		6.004 8.678	
٠.	222220	D (	- 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0	900.0	99.00	8.070 8.75	4
٠.	40000770	P	988.50 98.000 98.000	90.0	2.00	6.67 7.69.7	422
<b>-</b> •	0000770		1000.000		20.51	6 717	9
<b>-</b> -	82265000	9.4	1901.48		99.4	689	9.241
	ROOKS		1961	. S. S.	96	6.674	<b>9</b> .24
	82265969	9	988.61	0.552	-2.60	6.652	-0.220
	82265970	9.0	999.84	0.550	-2.60	6.658	<b>9</b> .23
	82265971	0.0	989.14	0.551	8.7	6.646	9
-	82265072	<b>0</b> .0	999.84	0.550	<b>8</b> :	6.654	9.20
_	82265073	<b>6</b> .	999.84	9.554	<b>8</b> 9	6.656	9.52
	52265974	9.0	79.286	6.33	8.0	70.0 0.0	
<b></b>	82265975	•	1991.37	- CC - C	<b>8</b> 8	6.088	
<b></b> .	52265976	B. (	1666.43	9.00 6.00	8.9	+ 0.0 9.0 9.0 9.0	
<b>.</b>	7/863228	9.0	24.000 4.000	6.335	8. 9. 4 4. 4	66.0 60.0	9
¬:	0/00779	D	000.70	9.33	90.0	6.00	\$
] :	0764400	<b>9.</b> •	C7.888	9.047 9.43	•	A. 4.	
7.1	A1245002	) e	1867.81	0.042	96	6.455	9
:=	83249004	6	1001.08	0.045	98.9	6.445	98.9
:=	83249005	3.0	998.76	0.047	8.9	6.418	\$ <b>9</b>
: I	83249006	9.0	1666.27	0.047	6.61	6.436	<b>9</b> .9
II	83250008	3.0	999.81	0.044	<b>9</b> .0	6.436	<b>ም</b>
II	83250009	<b>9</b> .0	1666.64	<b>9</b> .043	<b>3</b> .	6.438	8. <b>9</b>
II	83250010	a.e	998.88	0.043	<b>6</b> .6	6.424	8
II	83250011	a.e	1666.27	6.642	6.62	6.441	87. G
11	83244040	3. <b>0</b>	999.81	0.045	-2.06	6.436	9
=	83244041	a.e	1000.62	9.046	-2.06	6.443	8
<b>.</b>	83249007	ю. 6	1001.08	9.048	-5.83 -6.83	6.440	5.0
I	83249008	B. (	88.00	9.6	-2.63	9.4.0	9
I	83249669	B)	18.888	9.040	2.63	0.430	9
Ξ:	83249010	9. o	/8.000 8.000 8.000	9.0	29.7-	0.44.0	99
<b>.</b>	21995258	9.0		240.0	- 1 T		9
-							

Damping, 1/sec	9	•					-B. 304	- <b>6</b> .365	- <b>6</b> .308	-A.307	•	9.398	-6.387	9.388	-6.302	٠	-0.30¢	•	-6.307	_•	•	-6.302	٠	88. P	9.302	-9·300	<b>-0</b> .299	-0.293	-0.295	<b>-0.289</b>	-9.288	-8.295	-6.289	-6.297	-6.291	-6.295	-9.288	<b>-9</b> .288	<b>-0</b> .285	<b>-0</b> .294	-0.294	<b>-9</b> .302	-0.298	<b>-9</b> .293	-0.293	-0.291
Frequency. Hz	A 428	6.432	6.418	6.426	6.445	6.434	6.424	6.426	6.414	6.441	6.424	6.445	6.426	6.432	6.422	6.440	6.424	6.441	6.434	6.430	6.430	6.440	6.438	6.440	6.438	6.432	6.426	6.434	6.449	6.441	6.428	6.432	6.428	6.436	6.426	6.426	6.418	6.443	6.449	6.443	6.447	6.451	6.426	6.426	6.451	6.445
Shaft angle, deg	00 F		5	16.91	10.7	4.02	-4.02	90.9-	90.9-	-6.06	90.9-	90.9	-6.06		-6.93	-8.06	-7.98	-8.02	<b>-8.0</b> 2	-7.99	98.9	- B. 63	-10.04	-10.06	-10.01	-10.01	-9.95	-10.00	-10.00	-11.96	-11.96	-14.00	-14.00	-16.04	-16.04	-17.99	-17.99	-20.00	-20.00	99.0	0.05	-2.07	-2.07	-3.96	-3.96	-5.97
Advance ratio	970	9.0	9.0	940	6.048	9.046	6.045	0.045	9.046	9.046	9.048	0.047	0.047	0.045	<b>9</b> .044	<b>9</b> .046	6.045	<b>9</b> .048	6.047	0.047	6.043	0.045	6.643	<b>6</b> .044	9.04	0.042	9.046	9.046	6.045	9.044	9.943	0.042	0.0 14	9.043	<b>6</b> .044	9.04	6.043	<b>9.0</b>	0.045	6.697	960.0	<b>9</b> . <b>6</b> 38	660.0	6.698	760.0	0.038
Rotor speed, rpm	000	DO:000	900	000 AF	1991.98	999.81	998.99	999.11	998.07	1000.27	999.23	1001.08	999.34	999.57	998.76	1000.15	999.46	1000.85	999.92	89.666	999.34	1000.27	999.82	1000.15	1000.62	1000.15	69.666	999.81	1001.20	1666.62	999.34	899.68	999.34	1000.04	999.34	999.23	998.53	1666.73	1661.26	1000.04	1000.50	1666.73	998.76	998.53	1001	1666.56
Collective pitch, deg	•	<b>9</b> 6	9 6	9 6	9 6	6	3.0	9.0	<b>9</b> .0	3.0	3.0	3.0	9.°	J.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	Ø.0	3.0	9.0	3.0	3.0	3.0	3.0	G.0	3.0	0.0 0.0	3.0	3.0	3.0	3.0	3.0	9.0	3.0	3.0	9.n	3.0	9.0	3.0	9	6	3.0
Data point number	F1611CE	01044010	6104000	R3249012	83249013	83250014	83250015	83244844	83244045	83244046	83249014	83249016	83249017	83250016	83250017	83244047	83245004	83249018	83249626	83249021	83250019	83250020	83244049	83244050	83245005	83245006	83245007	83250022	83250023	83250024	83250025	83250026	83250027	83250028	83250029	83250030	83250031	83250032	83250033	83250034	83250035	83250036	83250037	83250038	83250039	83250040
Rotor	:	::	7 -	:-	:=	II	Ξ	11	1	11	II	11	11	11	11	11	I	11	=	Ξ	11	=	I	=	Ξ	II	I	11	=	11	II	11	II	11	I	II	Ξ	11	11	11	II	II	I	Ξ	-	:::

Domping. 1/sec	- <b>6</b> .289 - <b>6</b> .291	9.58¢	9.294		•	-6.288	•	-6.286 - 287	900	•	282	<b>-0</b> .282		-9.296	<b>-9</b> .296	-0.297	<b>-0</b> .292	<b>-0</b> .293	•	<b>-6</b> .288	9.286	200	787	280	<b>-9</b> .282	-6.281	<b>-0</b> .273	-0.271	•	-0.296	-6.289	-9.284	6.295	<b>-6</b> .286	807.9	-8.295	<b>-6</b> .293	<b>-0.278</b>	<b>-9.299</b>		<b>-9</b> .296	<b>-9</b> .286
Frequency.	6.434	6.438	6.441	6.436	6.434	6.438	6.443	6.441	474.0	A 428	8.416	6.438	6.434	6.422	6.434	6.436	6.422	6.424	6.438	6.443	6.436	424.0	0.4-0	6.426	6.416	6.424	6.430	6.426	6.420	6.440	6.424	6.432	6.455	6.438	6.430	6.436	6.432	6.440	6.436	6.434	6.428	6.416
Shaft angle, deg	-5.96 -7.96	-7.94 6.94	\$ 8 9	-12.08	-12.07	-14.04	-14.65	-16.94	10.04	08.77.	20.00	-20.00	8.7	28.7	-6.65	-6.05	-8.02	<b>-6</b> . <b>6</b> 2	66.6-	86. P	-12.06	-12.06		15.93	-16.03	-17.96	-17.96	-19.95	-19.95	-7.95	-7.95	80.0			₩./-	89.98 80.98	8.96	-10.01	-10.01	-10.01	-10.02	-10.62
Advance	6.699 699	0.097	6.697	6.698	689.	88.0	889.	888		700. <b>0</b>	*0 C	660.0	0.149	0.140	<b>6</b> .146	0.148	<b>6</b> .149	0.149	<b>6</b> .149	0.147	0.149	<b>6.14</b> /	)		9,148	9.148	<b>6</b> .149	6.149	<b>6</b> .148	0.200	9.189	9.280	6.201	6.199	98.0	69.189	6.199	0.202	<b>6</b> . 198	9.198	6.199	<b>6</b> . 199
Rotor speed, rpm	999.46 999.46	999.92	1686.39	999.82	999.57	1000.04	1666.56	1000.39	7 · · · · · · · · · · · · · · · · · · ·	888.11 000 K7	1 × × × × × ×	1000.39	999.82	998.88	1000.04	1000.27	999.11	989.34	1000.62	1001.20	900.20	1666.27	-1.888	1996.94	11.000	999.92	1966.50	1000.27	999.57	1000.50	999.11	989.46	1991.43	988.34	1666.59	999.81	999.92	1000.39	999.92	99.68	999.69	999.11
Collective pitch, deg		9.6	• •	3.0	a.b	<b>9</b> .0	<b>.</b>	o.	<b>D</b> (	• •		3.0	3.0	d.D	3.0	3.0	3.0	3.0	<b>9.0</b>	<b>9.0</b>	•	9.7	• •		. m	9.0	3.0	a.0	<b>0</b> .n	<b>9.</b> 0	<b>6</b> .9	<b>0</b> .0	9.0	<b>9</b> .6	D.01	<b>9</b>	<b>9</b> , 0	9. 9.	J. 0	<b>9</b> .0	<b>9</b>	D.0
Data point number	8325 <b>00</b> 41 8325 <b>00</b> 42	83250043	83250045	83250046	83250047	83250048	83258849	83250050	63526631	70000700	81250854	83250055	83251004	83251005	83251006	63251007	83251008	83251009	83251010	83251011	83251012	83251013	+101CZC9	A1251013	83251017	83251018	83251019	83251020	83251021	83251026	83251027	83251032	83251033	83251034	82222884	83252005	83252006	83251035	83251036	83251037	83252007	83252008
Rotor			1	=======================================	<b>:</b>	=	I	Ξ:	<b>→</b> ;	<b>]</b>	-	:=	11	Ξ	=======================================	=======================================	==	11	11	11	H	Ξ:	3:	] <del> </del>			=======================================	11	11	11	11	H	_	I.	<b>⊒</b> :	I	I	II	11			II

Domping. 1/sec	-0.283	-0.284	<b>-0</b> .274	<b>-9</b> .285	997.9	<b>-9</b> .268	6.2/5	<b>-0</b> .278	9/7.9	-0.272	-0.262	<b>6</b> .263	757.	<b>-0.228</b>	6.239	6.238	6.233	<b>-9</b> .228	<b>6</b> .234	-0.227	<b>-6</b> .284	<b>-6</b> .289	-0.297	-0.275	<b>-0</b> .279	<b>-0</b> .284	<b>-0</b> .272	<b>-0</b> .28 <b>0</b>	<b>6</b> .273	. <del>-0</del> .251	<b>-6</b> .245	<b>-6.249</b>	-8.218	<b>-6</b> .226	977.9	<b>6</b> .228	957.9	<b>-6.238</b>	6.229	<b>-6</b> .233	<b>6</b> .231	<b>-6</b> .26 <b>0</b>	<b>-0</b> .27 <b>0</b>	<b>9</b> .27 <b>0</b>	<b>9</b> .268	-6.239
Frequency.	6.424	6.426	6.443	6.443	6.424	6.426	0.456	6.441	0.441	6.441	6.438	6.447	6.450	6.440	6.432	6.434	6.436	6.438	6.440	6.440	6.434	6.443	6.434	6.416	6.426	•	6.432	6.426	6.430	6.440	6.434	6.424	6.434	6.449	6.458	6.434	9.4	•	6.441		6.434	6.418	6.420	6.422	6.424	6.436
Shaft angle, deg	-10.02	-11.99	-11.99	-11.99	-12.65	-12.03	N	ו מי	?	-13.96	ю.	80 1	ю.	0.0	-18.00	-18.01	-18.01	-20.00	-20.00	-20.00	-8.07	8.99	8.9	-10.03	-10.00	-10.00	-12.00	-12.00	-12.00	-14.00	-14.00	-14.00	-16.00	-16.00	-16.00	-18.96	-18.66	-18.98	-20.00	-20.00	-20.00	-10.00	-10.00	-10.00	-10.00	-12.00
Advance ratio	0.200	0.200	6.199	0.200	9.133	9.198	6.197	0.197	6.197	9.196	. 198	9.199	. 100 100	6.197	6.201	6.199	6.198	0.199	6.198	6.198	0.248	6.249	0.250	0.249	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	6.256	0.250	6.256	0.250	0.250	0.250	0.250	6.300	6.300	6.300	6.366	9.300
Rotor speed,	999, 57	999.57	1000.85	1666.73	999.57	1000.04	1969.27	1661.28	1001.32	1661.32	1000.27	1001.32	1961.88	1666.97	1666.15	1000.39	1000.39	1000.39	1000.73	1000.62	1000.04	1000.62	999, 92	998.78	1000.00	1999.99	1000.00	1606.66	1999.99	1666.66	1000.00	1666.66	1000.00	1999.99	1000.00	1000.00	1000.00	1000.00	1000.00	1666.66	1000.00	1666.66	1666.66	1000.00	•	1000.00
Collective pitch, deg	6.5	G.0	0.n	J. 0	0.0 0.0	3.0 0.0	<b>6</b> .0	<b>8.</b> 0	9.5	3.0	9.n	<b>9.</b> 0	0.0 0.0	0.0	0.N	9.0	a.0	9.	9.0	3.6	9.0	9	6	9 6	9.5	3.0	9.0	9.0	3.0	3.0	a.6	<b>9</b> .6	0.0 0.0	3.0	o.6	3.0	a.e	a.e	o.0	0.D	0.D	<b>0</b> .0	3.0	<b>9</b> .0	<b>0</b> .0	3.0
Data point number	83252669	83251038	83251039	83251040	83252010	83252011	83252012	83252013	83252014	83252015	83252016	83252017	83252018	83252019	83252020	83252021	83252022	83252023	83252024	83252025	83252026	83252027	83252028	83252029	83252030	83252031	83252032	83252033	83252034	83252035	83252036	83252037	83252038	83252039	83252040	83252041	83252042	83252043	83252044	83252045	83252046	83252047	83252048	83252049	83252056	83252050
Rotor	11	II	11	11	=	=	=		<b></b>	1	I	-	11	=	=	I	II	II	I	II	Π	11		: 1	II	Ξ	Ξ	II	11	<b></b>	Ξ	11	II	11	=	II	=	=	-	II	H	II	11	II	=	11

Damping. 1/sec	-0.235	-0.236	<b>6</b> .238	<b>6</b> .22 <b>6</b>	-0.214	6.276	6.213	12.9 12.9	777.	207.00	612.9	-6.285 6.585		\$ 7.5 P	75.6	9.240	<b>19.249</b>	-6.262	<b>-6</b> .212	<b>-6</b> .202	-B. 190	<b>-6</b> . 199	<b>-0.194</b>	<b>-6.172</b>	9.179	-6.173	<b>-9.69</b> 2	-8.663	988	<b>-6.692</b>	-9.688 	-6.717	4.7	9. 78.5 9. 85.4		20.0	790.9	9.676	9.667	<b>8</b> ?	9.686	-6.716 	-6.716	97.78	45.724	38. 8
Frequency, Hz	6.434	6.441	6.420	6.426	6.446	6.426	0.4.0	6.436	******	6.4.6 404	6.422	6.441	6.441	6.441	6.422	6.432	6.430	6.434	6.432	6.441	6.438	6.428	6.430	6.432	6.432	6.438	6.453	6.461	6.457	6.447	6.451	6.478	6.465	6.459	6.455	0.440	6.455	6.463	6.449	6.457	6.453	6.447	6.441	6.441	6.457	6.438
Shaft angle, deg	-12.00	-12.00	-12.00	-14.00	14.66	-14.98	-14.00	-14.68	-16.00	-16.99	-16.90	18.66	-18.66	-18.66	-16.66	16.66	-16.66	-12.00	-12.00	-12.00	-14.00	-14.00	-14.00	-16.90	-16.00	-16.99	-2.66	-5.8	7.62	7.62	-6.04	<b>4</b> .9	7.97	-7.96	99.01-	99.91-	-12.00	-13.97	-13.96	-16.00	-16.00	-18.05	-18.05	-20.00	-20.00	-16.94
Advance	9.300	9.300	9.300	9.300	. 200 	9.388	6. 50¢	9.786	9. See	9.386	986	98.3	90.0	. 386	9.350	6.356	9.358	0.350	0.350	9.350	9.358	9.358	0.350	0.350	9.350	6.330	9.046	0.041	9.044	6.046	9.047	6.041	9.046	6.643	0.042	6.64	6.645	0.045	0.045	0.044	6.645	6.646	6.64e	6.645	0.043	6.693
Rotor speed,	1000.00	1999.99	1000.00	1000.00	1999	1999.99	1866.86	1999.99	1000.00	1600.60	1606.66	1906.00	1606.66	1666.66	1666.66	1888.88	1999.99	1000.00	1606.66	1666.66	1000.00	1606.66	1666.66	1666.66	1000.00	1666.66	999.11	1666.64	999.57	98.88	999.57	1001.43	1666.15	999.69	40.000	4.000	688.01	1666.39	999.34	999.92	999.57	999.11	998.76	998.65	999.81	68.788
Collective pitch, deg	<b>9</b> .5	3.0	<b>⊕</b> .₽	<b>0</b> .0	9.0 9.0	Ø.0	9.7	<b>9</b> .0	<b>9</b> .0	9. 19.	9.	Ø.0	<b>9</b> .0	ان 6	9.0	9. 9.	d.0	9.n	9.n	0.D	Ø.50	9.0	Ø.8	9.°	<b>9</b> .0	<b>9</b> .	<b>9</b> .0	6.6	<b>9</b> .0	<b>.</b>	<b>9</b> .0	<b>9</b> .	9.	<b>.</b>	9 (c)	9 (d	9 (0	<b>0</b> .	<b>0</b> .0	<b>0</b> .0	<b>9</b> .9	<b>.</b>	<b>6</b> .0	<b>.</b>	<b>0</b> .0	<b>5</b> 0.
Data point number	83252851	83252052	83252057	83252053	83252058	83252058	82222828	83252060	83232861	83252062	83252963	83252064	83252965	83252066	83252967	83252968	83252070	83252071	83252072	83252073	83252074	83252075	83252076	83252077	83252078	83252079	83259051	83259052	83259053	83259054	83259055	83259056	83259057	83259058	83259859	83259060	83259861	83259063	83259064	83259065	83259066	83259067	83259068	83259069	83259070	83259071
Rotor	11	I	=	=	=	<b>→</b> 1	=		-	II			I	I	II	=	=	11	II	11	11	11	II	=	1	<b>:</b>	Ξ	II	II	I	11	=	11		II	II	II	11	II	II	=		11	II	I	II

Damping. 1/sec	-6.663	9.67	<b>-9</b> .668	<b>678</b>	4.674	<b>679</b>	-0.674	-6.689	-6.684
Frequency, Hz	6.445	6.440	6.459	6.445	6.438	6.463	6.461	6.453	6.453
Shaft angle, deg	-16.04	-18.07	-18.07	-20.00	-20.00	-17.98	-17.99	-20.00	-20.00
Advance	6.695	9.036	6.697	6.697	6.697	6.151	0.148	0.147	0.149
Rotor speed,	998.99	998.30	999.81	998.76	998.41	1666.39	1666.27	999.57	686
Collective pitch, deg	6.6	6.6	6.6	6.0	<b>6</b> .0	6.6	6.9	6.0	9.0
Data point number	83259072	83259073	83259074	83259075	83259076	83259077	83259078	83259079	83259080
Rotor	11	11	11	11	I	=	11	=	=

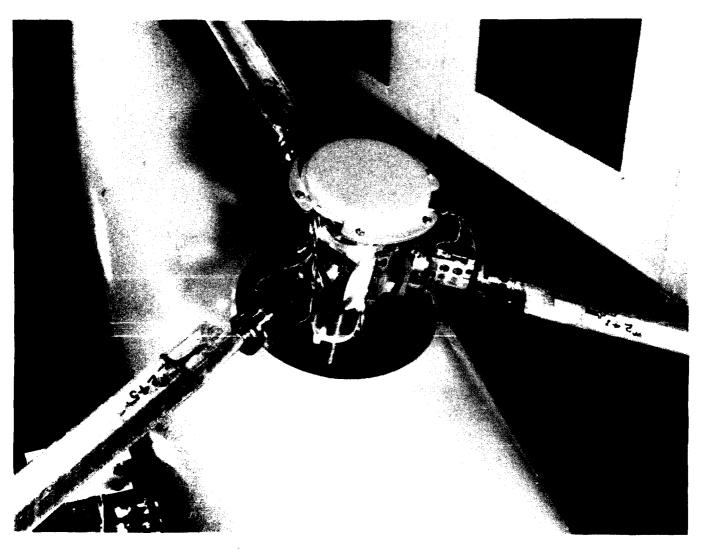


Figure 1.-Model hub and blades.

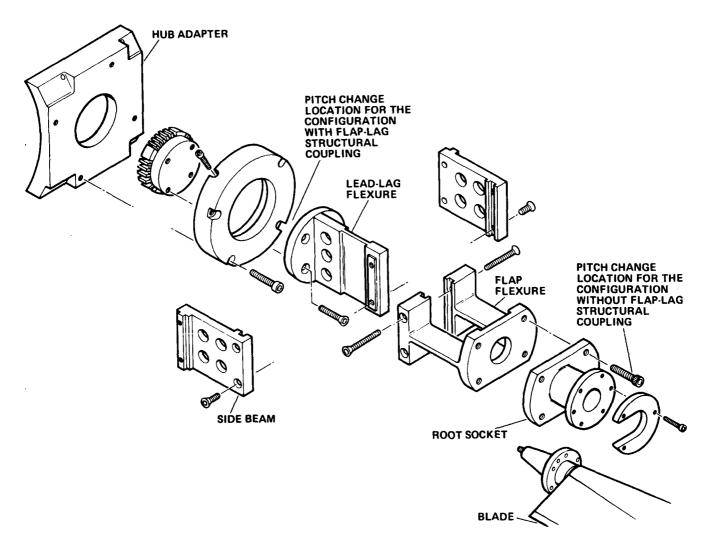


Figure 2.-Exploded view of blade and flexure assembly.

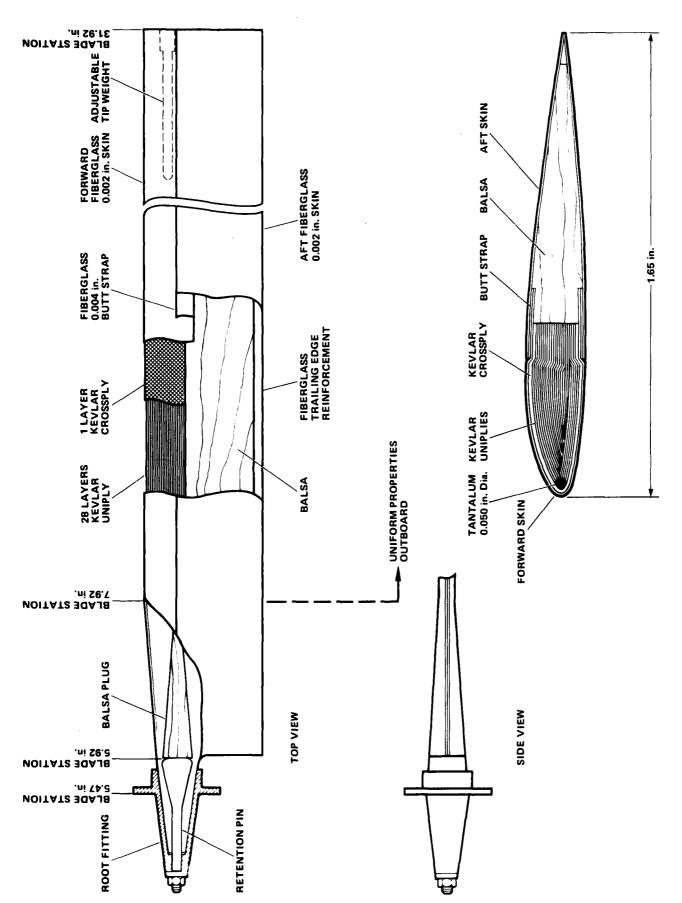


Figure 3.-Rotor blade planform and cross section.

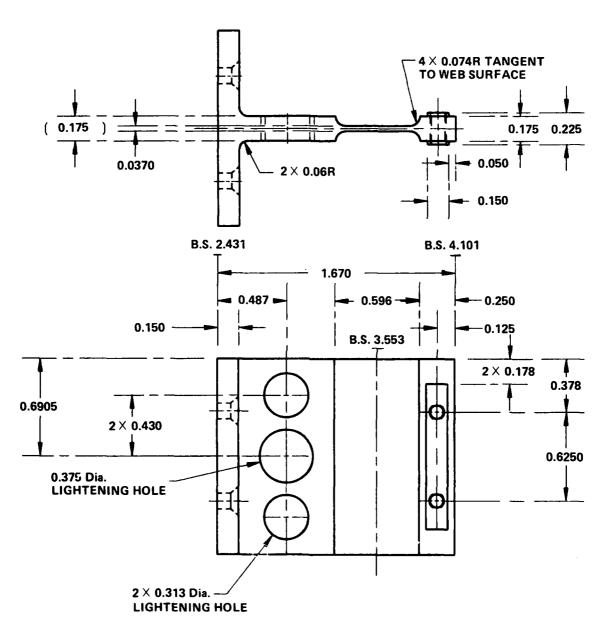


Figure 4.-Lead-lag flexure; 17-4PH H900 steel; dimensions in inches.

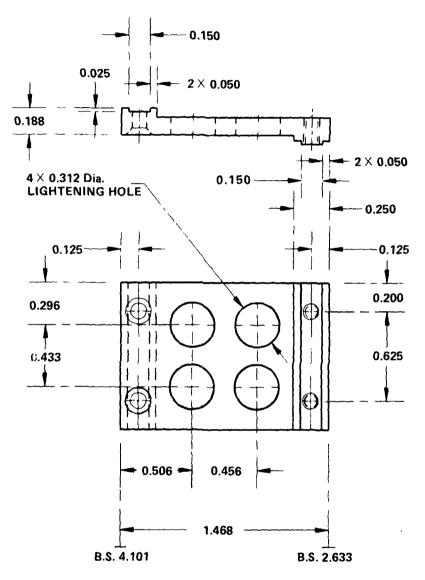


Figure 5.-Side beam; TI-6AL-4V titanium; dimensions in inches.

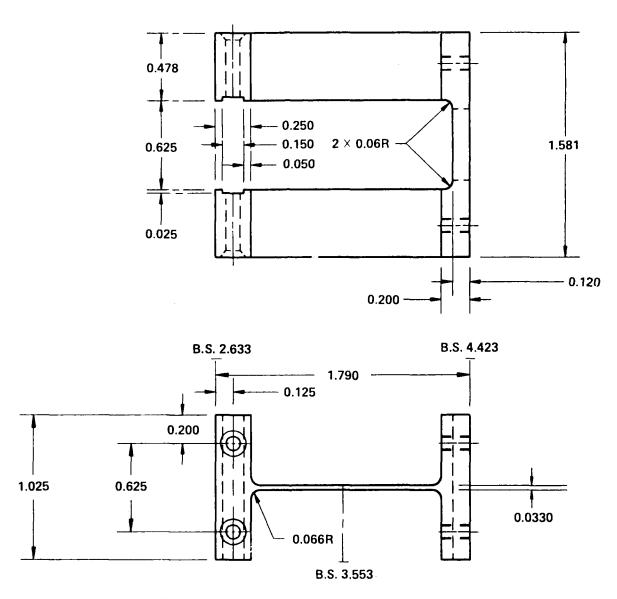


Figure 6.-Flap flexure; 17-4PH H900 steel; dimensions in inches.

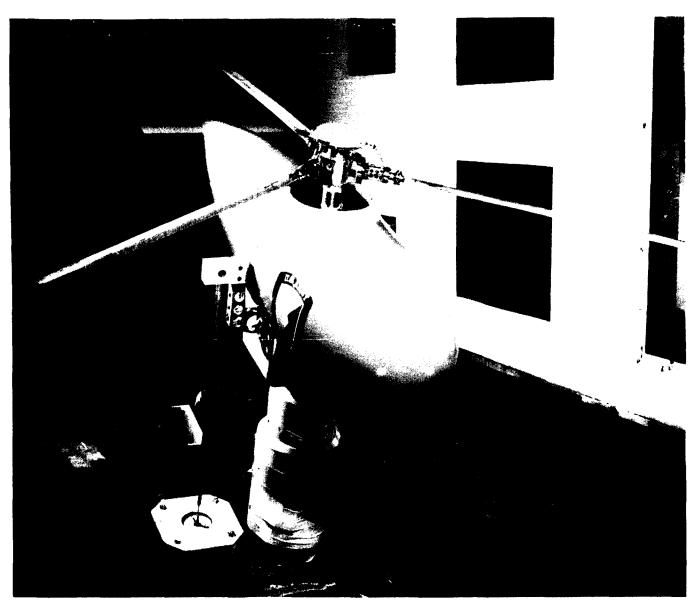
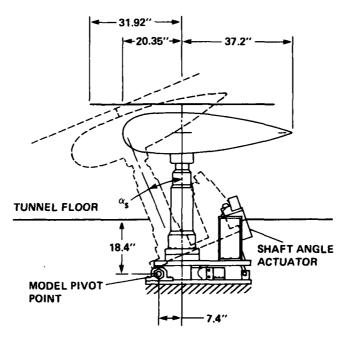
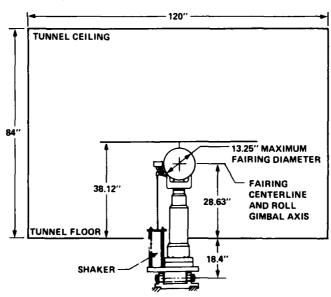


Figure 7.-Model installed in the Aeroflight dynamics Directorate's 7- by 10-foot wind tunnel test section.

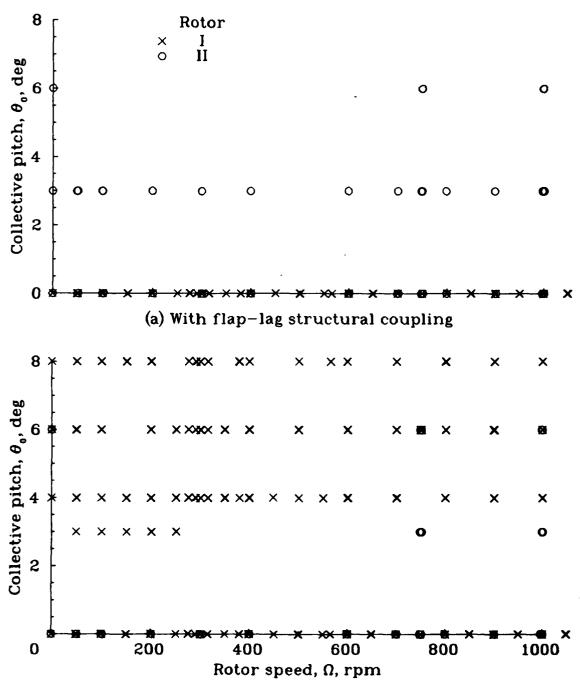


(a) Side view;  $\alpha_s = 0^{\circ}$  and  $-20^{\circ}$ .



(b) Front view;  $\alpha_s = 0^{\circ}$ .

Figure 8.-Installation diagram of the model in the Aeroflightdynamics Directorate's 7- by 10-foot wind tunnel test section.



(b) Without flap-lag structural coupling
Figure 9.-Hover test points.

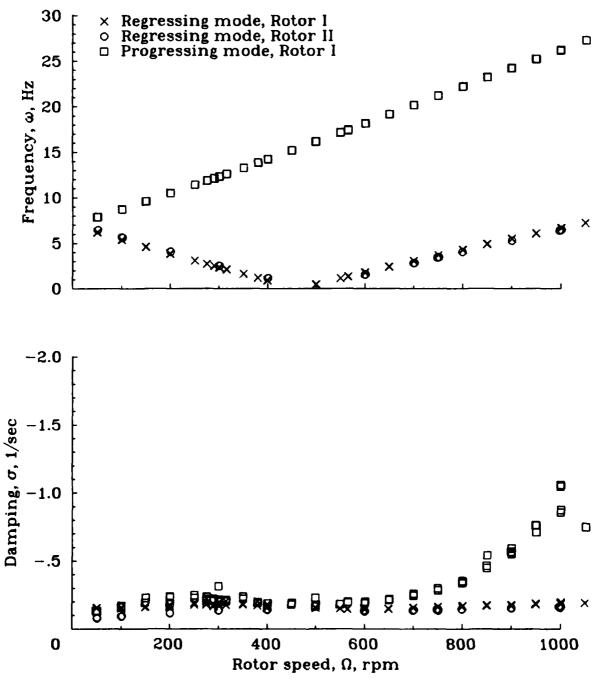


Figure 10.-Fixed system lead-lag frequencies and damping values versus rotor speed in hover;  $\theta_0 = 0^{\circ}$ .

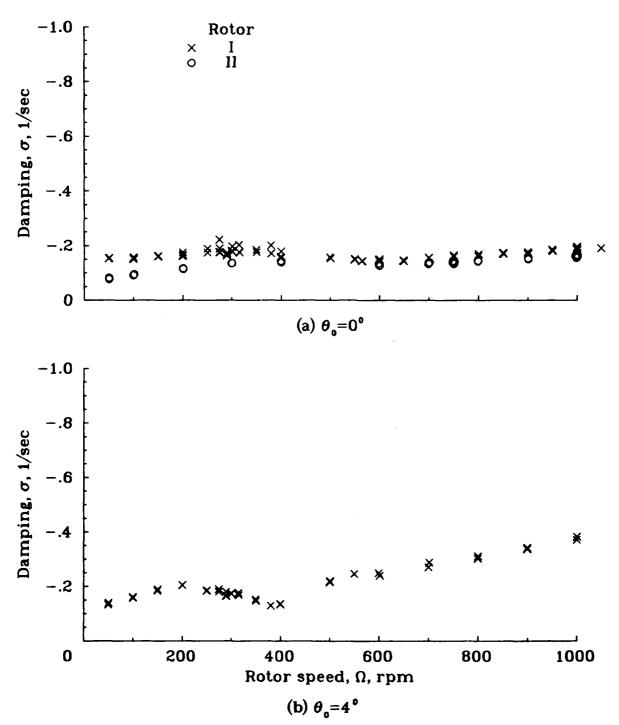


Figure 11.-Lead-lag regressing mode damping versus rotor speed in hover; configuration without flap-lag structural coupling.

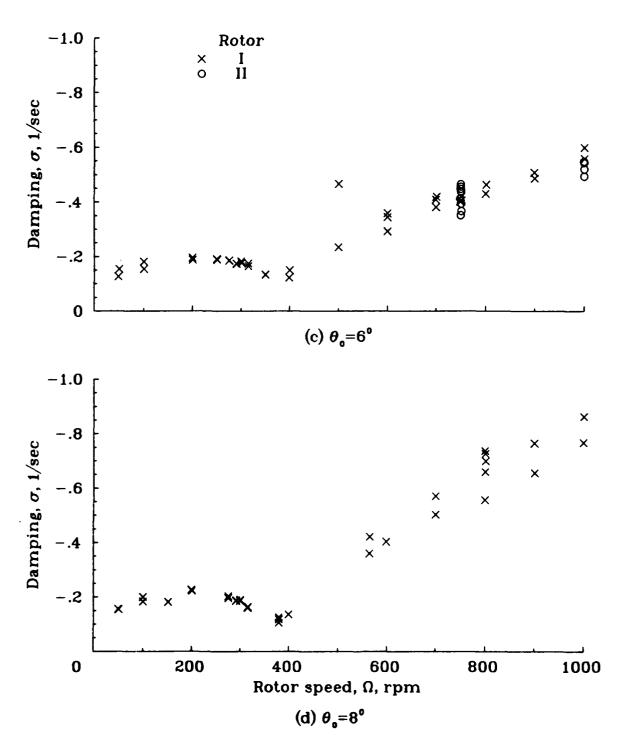


Figure 11.-Concluded.

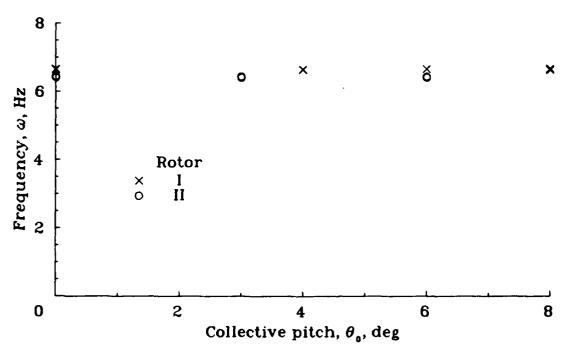
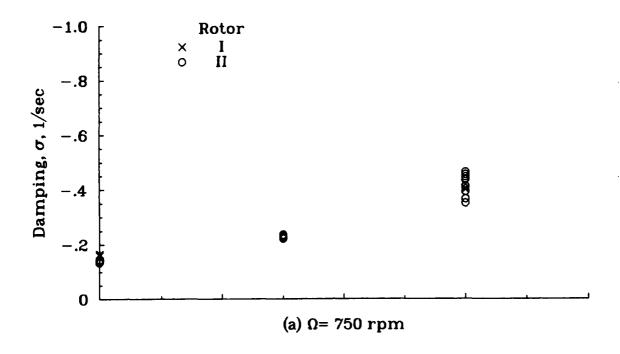


Figure 12.—Lead-lag regressing mode frequency versus collective pitch in hover; configuration without flap-lag structural coupling; 1000 rpm.



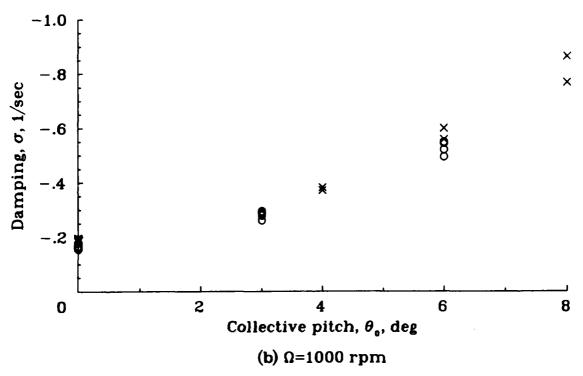
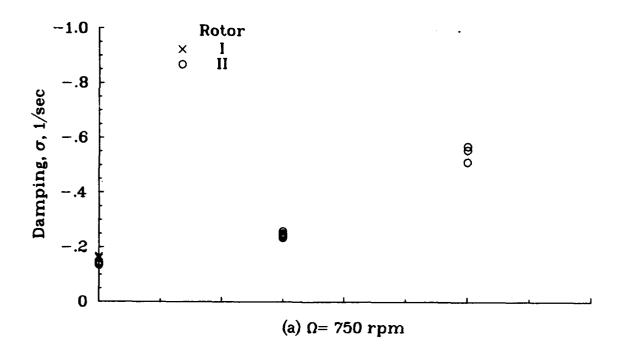


Figure 13.-Lead-lag regressing mode damping versus collective pitch in hover; configuration without flap-lag structural coupling.



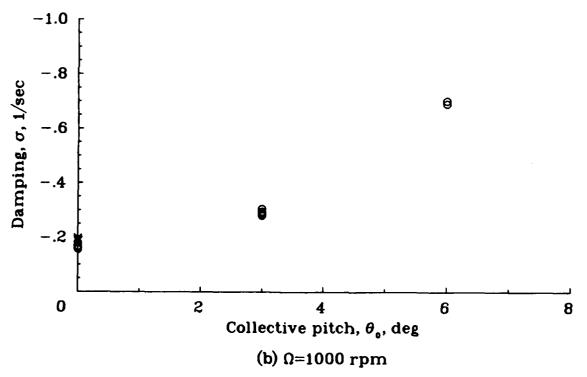


Figure 14.—Lead-lag regressing mode damping versus collective pitch in hover; configuration with flap-lag structural coupling.

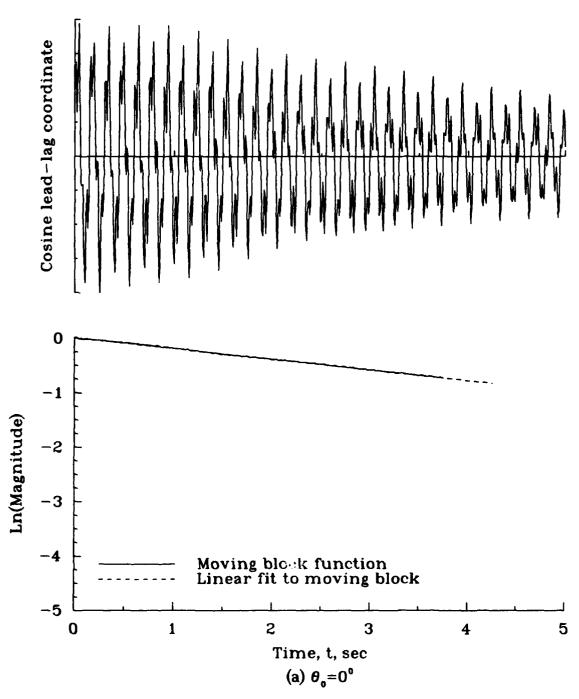


Figure 15.—Representative transient time histories in hover and their moving-block functions at the regressing lead-lag mode frequency; configuration without flap-lag structural coupling.

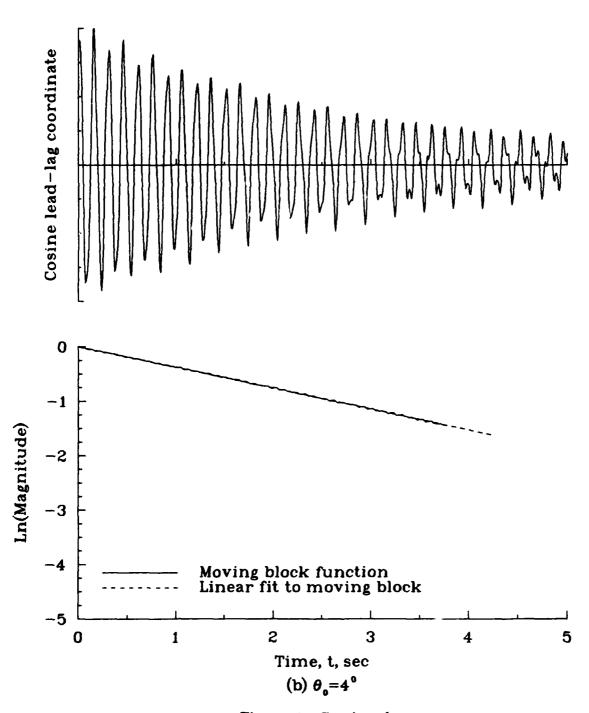


Figure 15.-Continued.

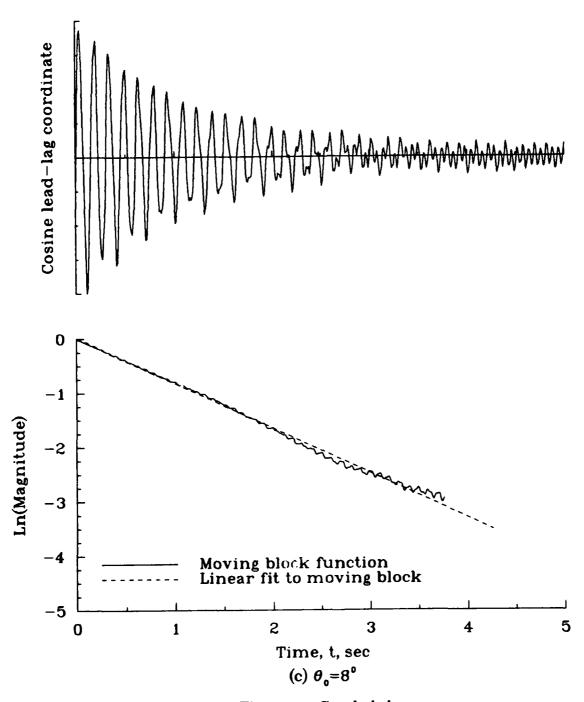
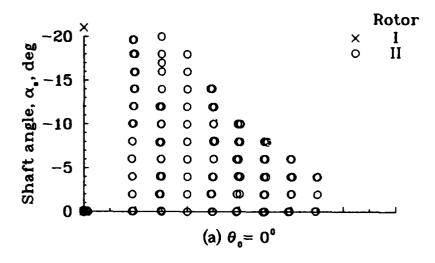
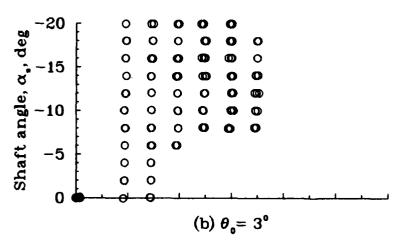


Figure 15.-Concluded.





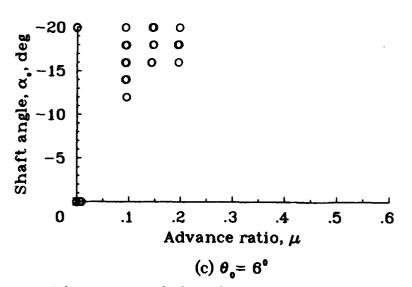


Figure 16.—Advance ratio, shaft angle, and collective pitch conditions tested at 750 rpm for the configuration without flap-lag structural coupling.

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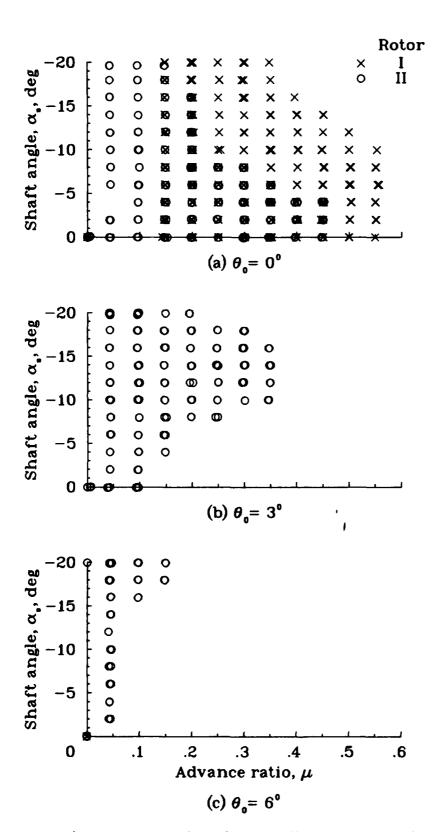


Figure 17.-Advance ratio, shaft angle, and collective pitch conditions tested at 1000 rpm for the configuration without flap-lag structural coupling.

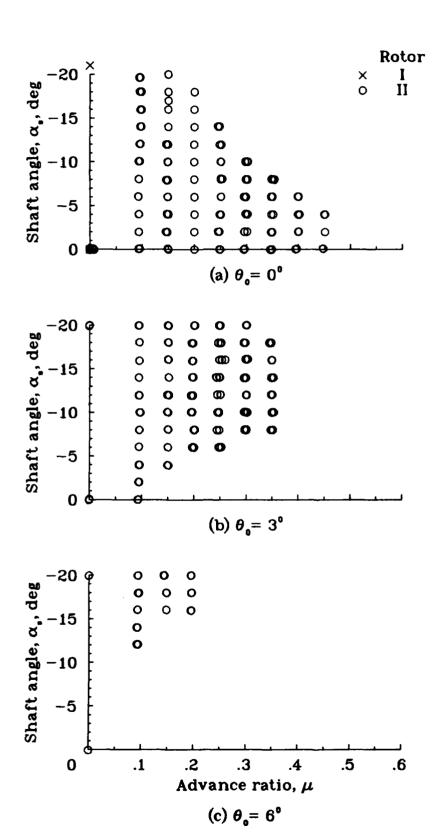


Figure 18.-Advance ratio, shaft angle, and collective pitch conditions tested at 750 rpm for the configuration with flap-lag structural coupling.

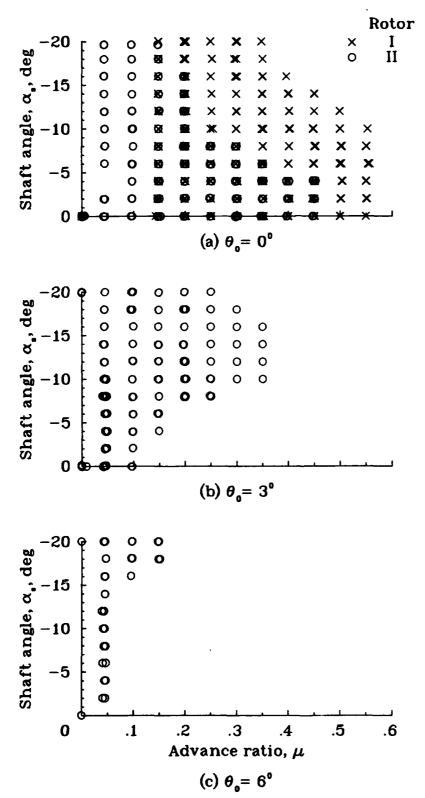


Figure 19.—Advance ratio, shaft angle, and collective pitch conditions tested at 1000 rpm for the configuration with flap-lag structural coupling.

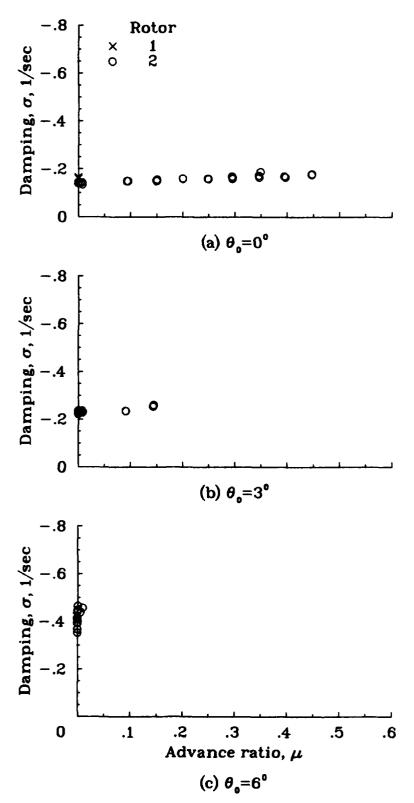


Figure 20.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm,  $\alpha_s = 0^{\circ}$ .

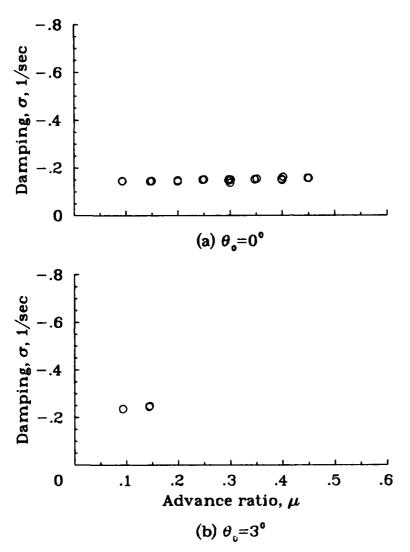


Figure 21.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm,  $\alpha_s = -4^{\circ}$ .

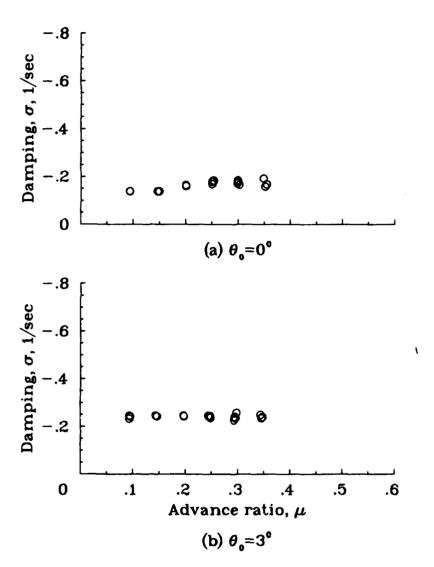


Figure 22.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm,  $\alpha_s = -8^{\circ}$ .

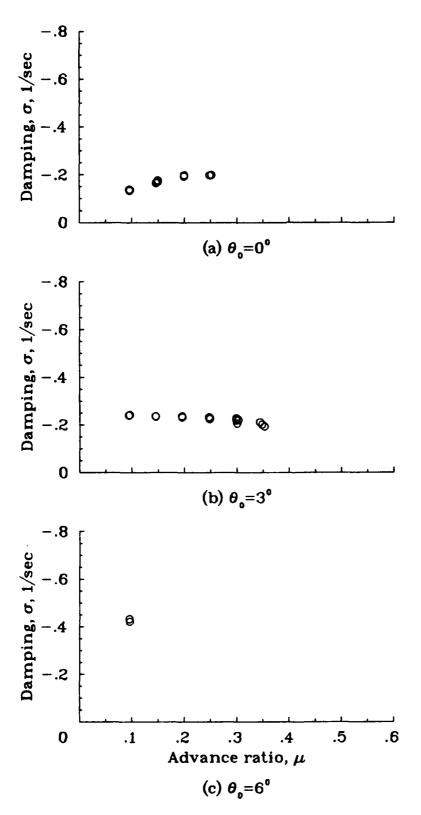


Figure 23.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm,  $\alpha_s = -12^{\circ}$ .

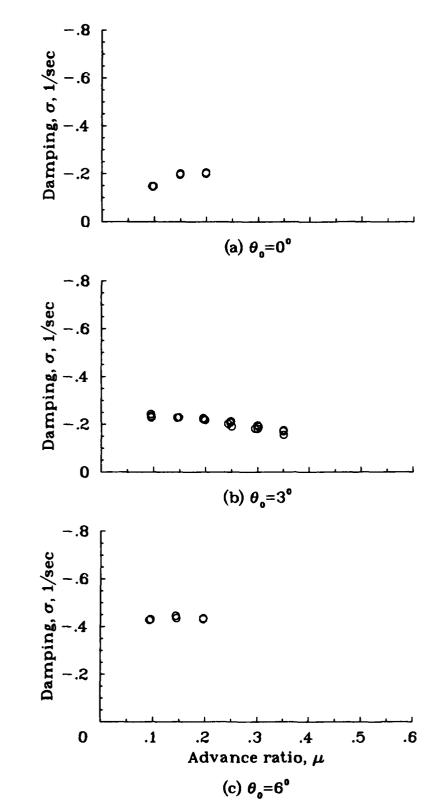


Figure 24.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm,  $\alpha_s = -16^{\circ}$ .

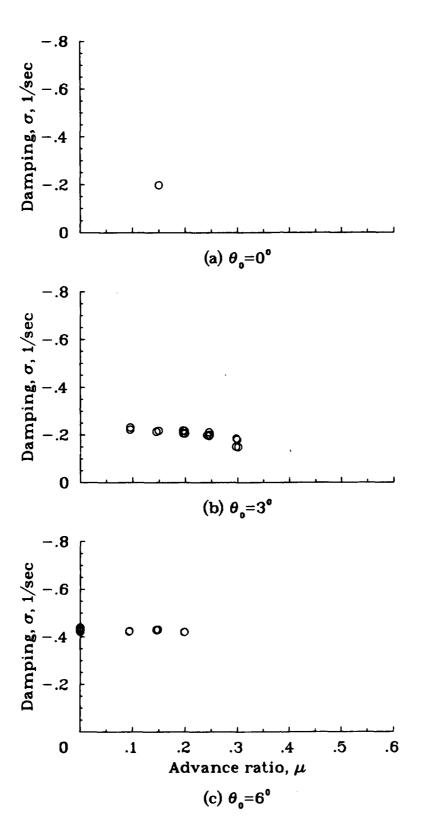


Figure 25.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 750 rpm,  $\alpha_s = -20^{\circ}$ .

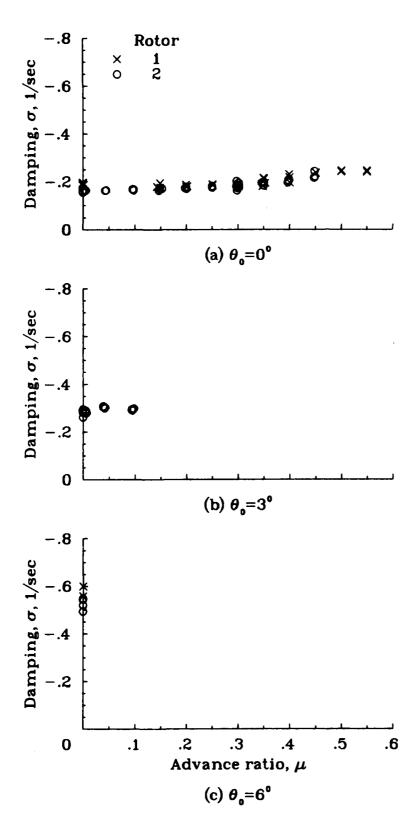


Figure 26.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm,  $\alpha_s=0^\circ$ .

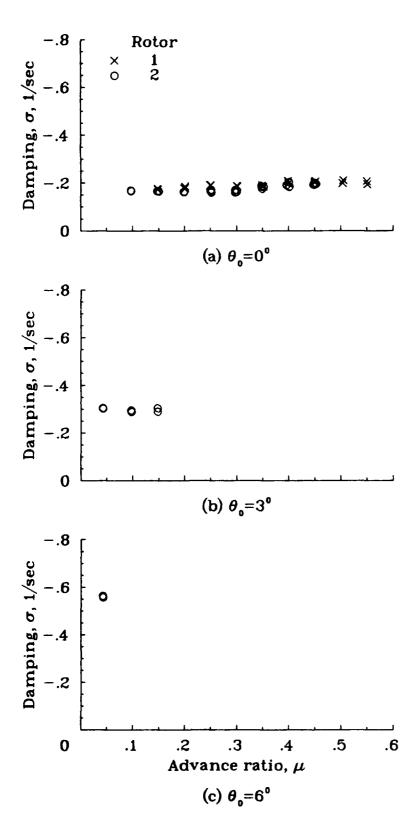


Figure 27.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm,  $\alpha_s = -4^{\circ}$ .

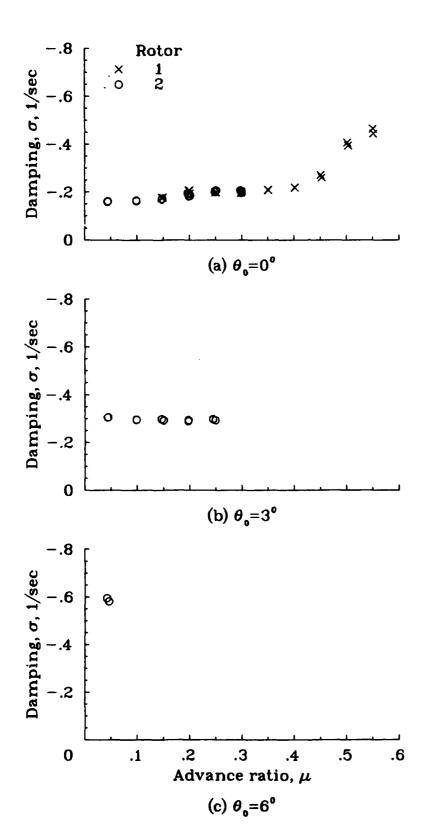


Figure 28.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm,  $\alpha_s = -8^{\circ}$ .

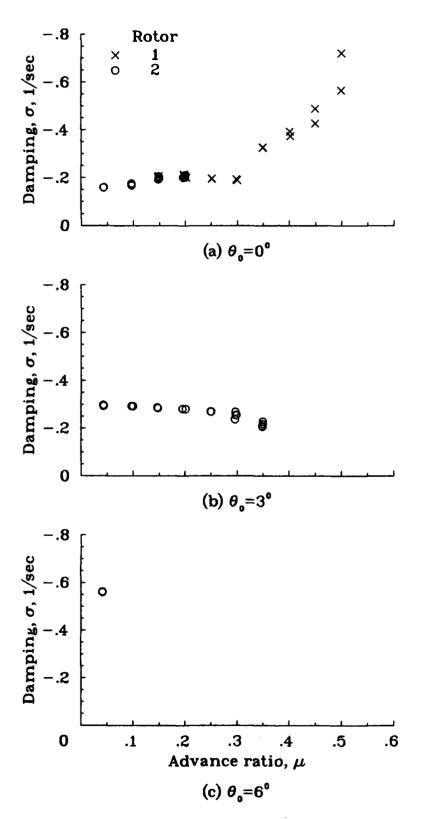


Figure 29.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm,  $\alpha_s=-12^\circ$ .

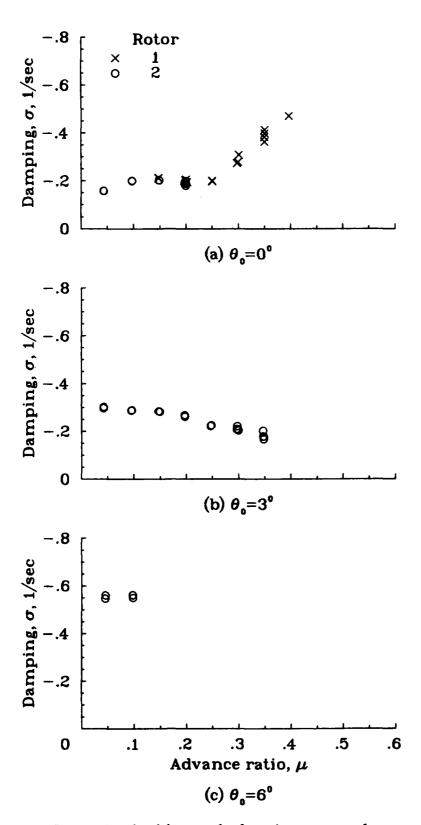


Figure 30.–Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm,  $\alpha_s = -16^\circ$ .

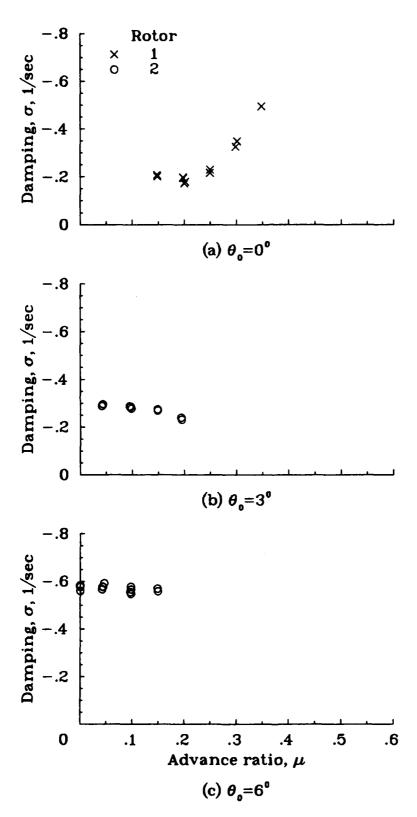


Figure 31.-Regressing lead-lag mode damping versus advance ratio; configuration without structural flap-lag coupling; 1000 rpm,  $\alpha_s = -20^{\circ}$ .

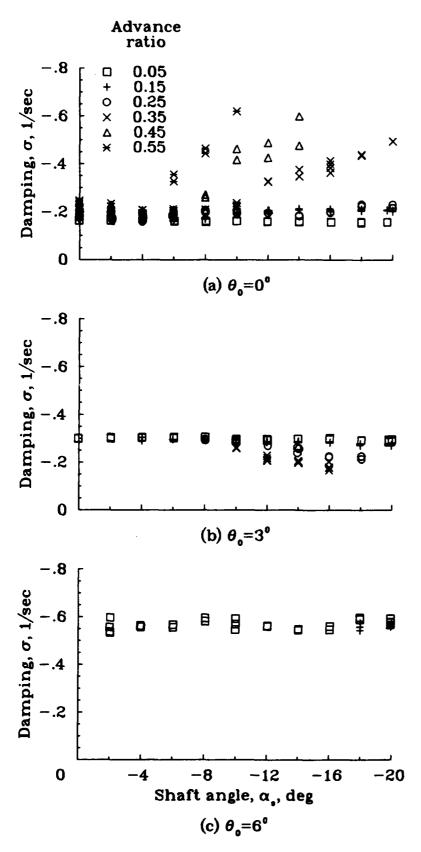


Figure 32.—Regressing lead-lag mode damping versus rotor shaft angle; configuration without structural flap-lag coupling; ; 1000 rpm; both Rotor I and Rotor II data are included without distinction.

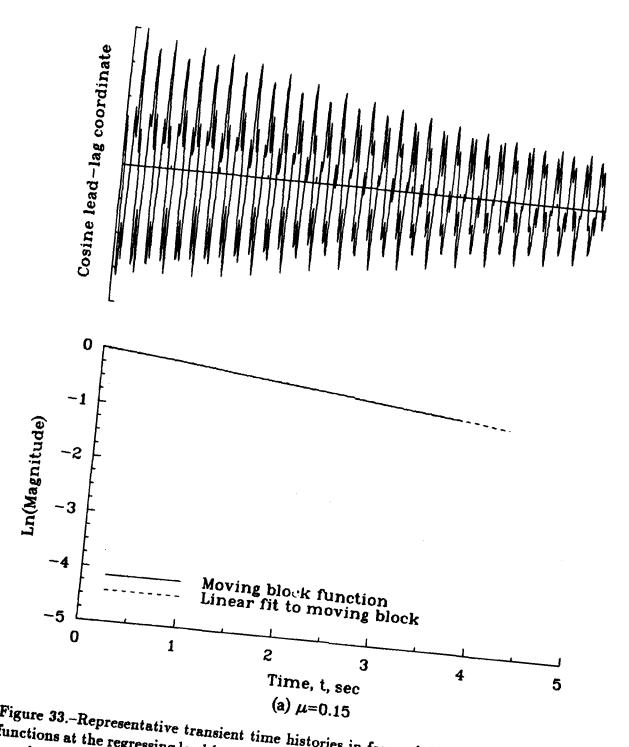
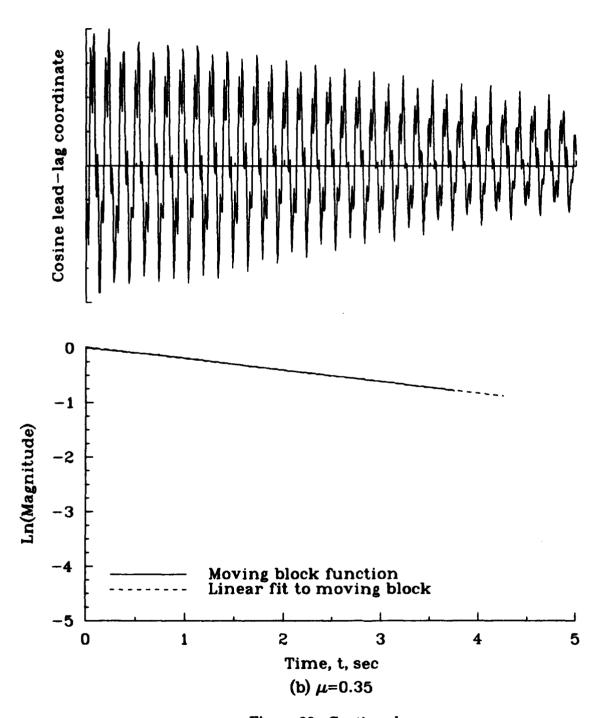


Figure 33.—Representative transient time histories in forward flight and their moving-block functions at the regressing lead-lag mode frequency; configuration without flap-lag structural coupling;  $\theta_0 = 0^{\circ}$ , 1000 rpm,  $\alpha_s = 0^{\circ}$ .



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Figure 33.-Continued.

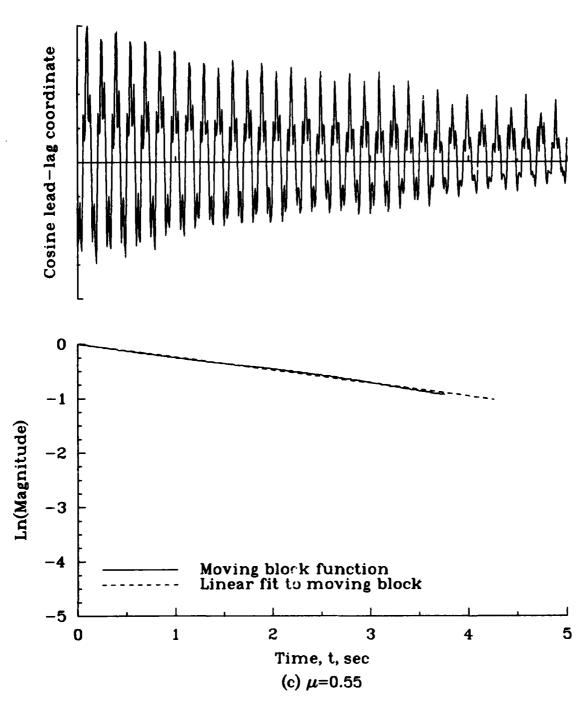


Figure 33.-Concluded.

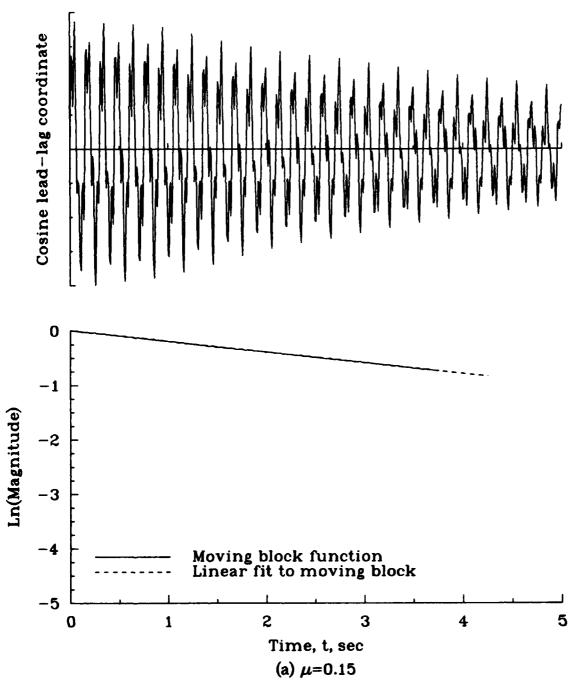


Figure 34.–Representative transient time histories in forward flight and their moving-block functions at the regressing lead-lag mode frequency; configuration without flap-lag structural coupling;  $\theta_0 = 0^{\circ}$ , 1000 rpm,  $\alpha_s = -10^{\circ}$ .

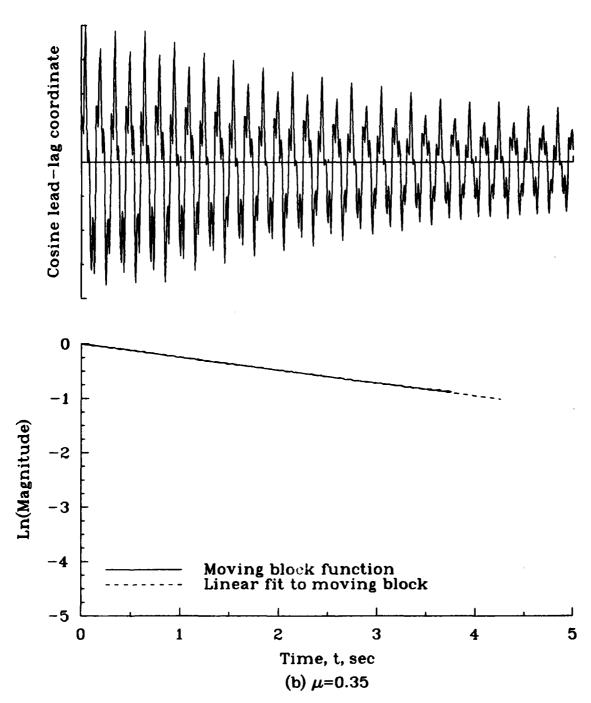


Figure 34.-Continued.

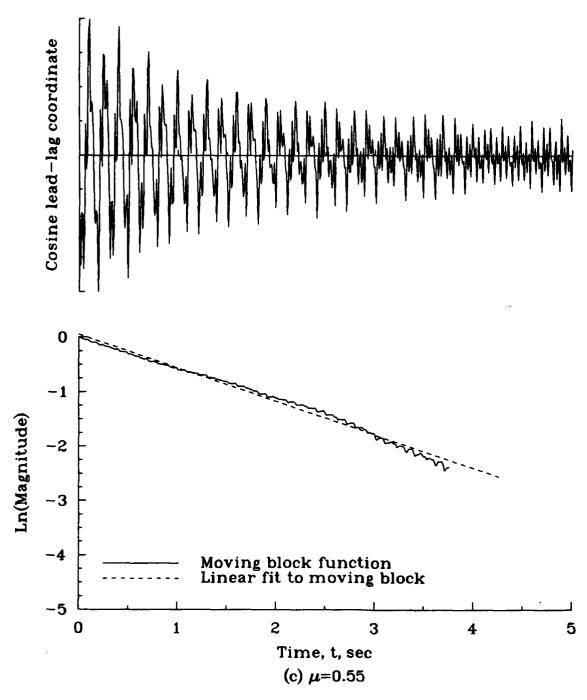


Figure 34.-Concluded.

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Point of Contact: Michael .  Moffett F	Field, CA 94035 (415) 6				
3. Abstract	Abstract				
was tested in the Aeroflighthe test was to determine ex ration in forward flight. The untrimmed at several collections as high as 0.55. Two inplaration both with and without was also conducted. Represhow general trends, and couse in detailed correlation abrupt increase in damping with high flapping loads. The results for hingeless rotors the data are expected to be analyses.	perimentally the lead-lag ne model tested had no crive pitch angles, at shaf ane natural frequencies, out structural flag lag coup resentative plots of the fomplete tabular data and exercises. The most pro- g with advance ratio at ce the hover data are consist without kinematic coupli	7- by 10-Foot Wi stability of a struct yelic pitch control of angles from 0° to 0.61/rev and 0.72/red oling. Concomitant frequency and dar model properties minent feature of extain high-speed, tent with previous ings. Overall, the o	and Tunnel. The sturally simple rot, and was therefore 2-20°, and at adver, were tested for the formation are in the forward flighth shaft-angle experimental and lata quality is ver	purpose of or configure operated ance ratios or configurate model resented to included for t data is an conditions, theoretical y good and	
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